

Article

# Variable DC-Link Voltage Algorithm with a Wide Range of Maximum Power Point Tracking for a Two-String PV System

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**Abstract:** This paper proposes a variable DC-link reference voltage algorithm for wide range of maximum power point tracking (MPPT) for two-string photovoltaic (PV) systems. A multi-string system, which is a kind of PV system, is widely used due to its many merits (such as the ability to use low rating devices, high MPPT efficiency, and so forth). PV systems can choose their input voltages on the basis of their PV cell connection structure. The PV cell connection structure can be restricted because the input voltage and current affect the PV system design. This reduces the MPPT range under some weather conditions. In the restricted PV connection structure, this algorithm enlarges the MPPT range and minimizes the increment of the total harmonic distortion (THD) by selecting the appropriate DC-link voltage reference which is changed by comparing the sorted input voltage. To verify the proposed algorithm, simulation and experiments are conducted to show the results of the performance for the proposed algorithm.

**Keywords:** multi string; PV system; MPPT

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## 1. Introduction

Photovoltaic (PV) systems can be characterized by their input voltages, currents, and number of inputs. A number of studies have been conducted to evaluate the efficiency and characteristics of the cell connection structure in multi-input PV systems [1–6]. Many studies have shown that multi-input

systems have higher maximum power point tracking (MPPT) performance than single-input systems [7–9].

There are two types of grid-connected PV system structures: (1) those that contain only a DC/AC converter and (2) those that contain both a DC/AC converter and a DC/DC converter. Systems containing only a DC/AC converter generally require a 600 V (three-phase) input and 350 V (single-phase) input for the grid-connection. Furthermore, PV systems cannot be operated under high temperature and low solar radiation conditions. These conditions cannot guarantee the 600 V (three-phase) PV input voltage or 350 V (single-phase) PV input voltage.

These drawbacks are eliminated when the PV system contains both a DC/DC converter and a DC/AC converter. In this structure, the DC/DC converter can be selectively designed as the boost converter, the buck converter, or the buck-boost converter, depending on the PV cell connection. The buck-boost converter is the best design for obtaining the maximum MPPT range; however, it is less efficient than a simple boost or buck converter [10,11]. For PV power systems of 10 kW or less, the boost converter is the best choice due to the high efficiency and the usability of the connection. Under the usual weather conditions, the PV cell connections of 10 kW has the voltage range below 600 V.

In a multi-input PV system with both a DC/DC converter and a DC/AC converter, there are two types of MPPT control methods. These methods depend on where the control system is implemented [12]. In the first method, the boost converter controls the MPPT independently and the inverter implements DC-link voltage control for the grid-connection [13]. In the second method, the boost converter controls the DC-link voltage and the inverter performs MPPT control [14,15]. Both of these methods offer similar performance, but the first method has better scalability. However, if the MPP input voltage of PV systems is higher than the DC-link voltage, the MPPT cannot be implemented for both of these methods. In other words, the MPPT range is limited by the reference voltage. In this case, if the high DC-link reference voltage is set to extend the MPPT range, it will cause a large output current ripple in the inverter. To solve this problem, the filter must be designed with higher inductance. Another solution to this problem is by making the input voltage of PV cells smaller than the value of the DC-link reference voltage; however, this solution limits the number of input PV cell combinations. Moreover, if the PV cells are connected to a low input voltage, this will increase the boost converter's rated current. The switching device should be chosen on the basis of this information.

This paper presents an algorithm that varies the DC-link voltage based on the input voltage. The proposed algorithm is designed to have a wide MPPT estimation range while maintaining the DC-link voltage with minimal current ripple.

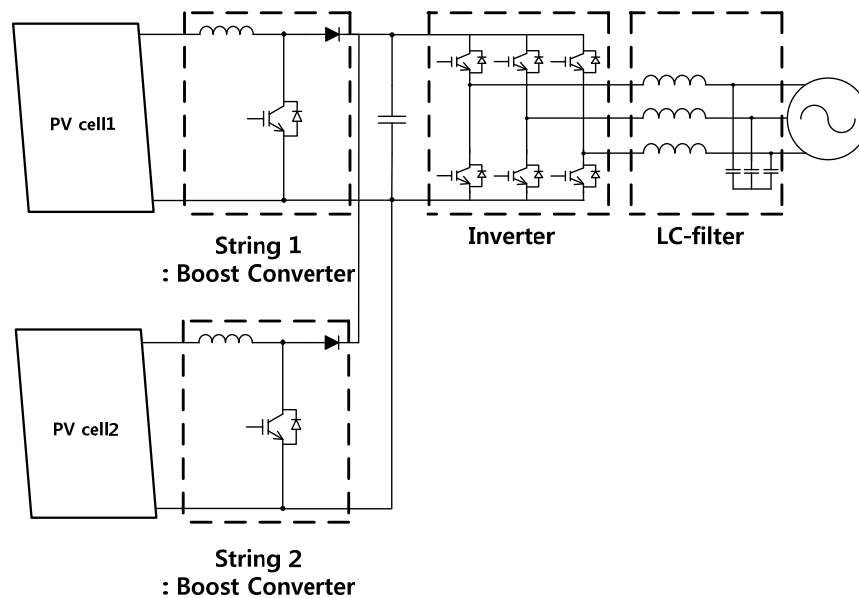
## 2. Configuration of a Two-String PV System

A PV system using two-string inputs consists of two boost converters, an inverter and an LC-filter and is depicted in Figure 1. The boost converters share the output, which is connected to the DC-link capacitor. The DC-link capacitor transfers power to the grid. The total power is divided across the two inputs. In this paper, the total power is divided as 7 kW on string 1 and 3 kW on string 2.

The current ripples to the DC-link capacitor cause a DC-link voltage ripple. This voltage ripple causes a corresponding ripple in the output currents from the inverter. Therefore, the boost converters

use the interleaved method to reduce the input current ripples [16,17]. The ON point of the switching device of string 1 is shifted from the ON point of the switching device of string 2 by half the switching period.

**Figure 1.** The configuration of a two-string PV system.



### 2.1. Boost Converter Control

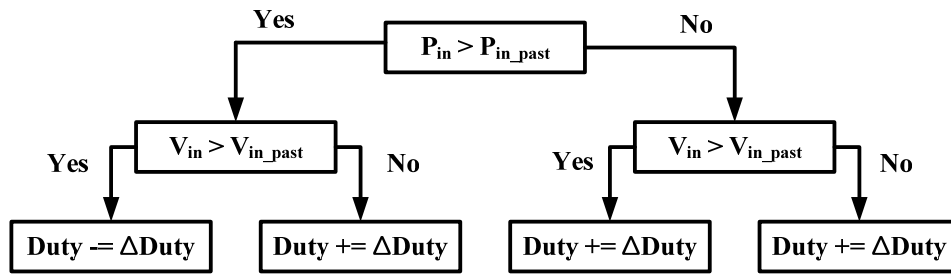
The MPPT algorithm is implemented in the boost converters. Each boost converter's operation is reflected in each MPPT algorithm. The MPPT algorithm for each string calculates the duty-cycle of the boost converter using its voltage and current. Therefore, each MPPT algorithm is implemented independently on the associated strings.

The MPPT algorithm is based on Perturb-and-Observe (P&O) algorithm. Many P&O algorithms have been studied [18–21], and most of them are simple. However, operation near the maximum power point (MPP) causes vibrations. The solution to this problem is to reduce the duty-cycle variation ( $\Delta$ duty) when operating near MPP [22] or to use a PI controller [23]. A drawback of the first approach is that the calculation for  $\Delta$ duty is sensitive to errors when the output power is low and the MPPT algorithm is initiated. If the sensing noise of the voltage and current is large, the calculation will not be accurate because  $\Delta$ power is small relative to  $\Delta$ duty. The second approach requires accurate modeling of Figure 1 and the steps of the controller's gain setting.

In this paper, the first approach is used to prevent vibration at MPP, as shown in Figure 2, and duty is increased or decreased according to the power and the voltage of the PV cells. An appropriate initial duty-cycle value is chosen to avoid the problem associated with low power. The power ( $P_{in}$ ) from the strings is calculated as shown in Equation (1):

$$P_{in} = V_{in} \times I_{in} \quad (1)$$

The input current ( $I_{in}$ ) contains the switching ripple of the boost converter. Therefore, the filtering value of the input current ( $I_{in}$ ) is used in the input power calculation.

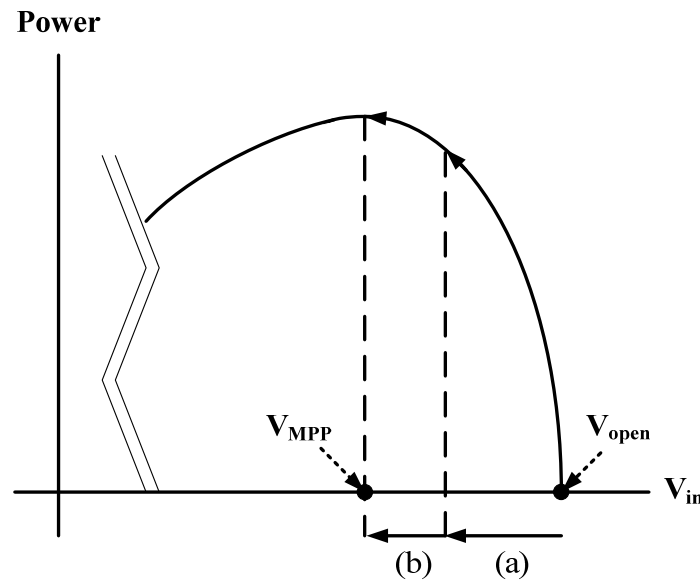
**Figure 2.** P&O algorithm for MPPT.

The power delivery is required when the boost converter generates a higher output voltage than the DC-link voltage. There must be sufficient duty-cycle to enable this increase in power delivery and to avoid the problems associated with low power. The initial duty-cycle value is calculated as shown in Equation (2):

$$D = \frac{V_{out}}{V_{in} + V_{out}} \quad (2)$$

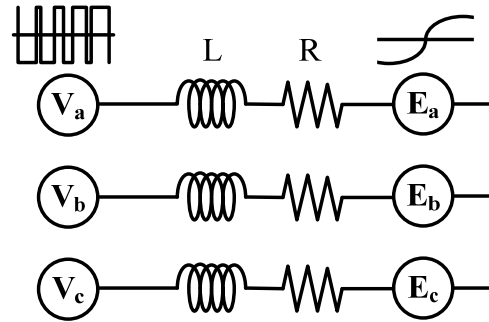
where  $V_{out}$  is the DC-link voltage.

Figure 3 illustrates the operation of the MPPT algorithm at the initial duty-cycle (a) and MPP after the duty-cycle is reached (b).

**Figure 3.** MPPT operation: the initial condition (a) and the later condition (b).

## 2.2. Inverter Control

The inverter handles the grid connection control. The modeling for the DC-link voltage control is based on Sannino's modeling method [24]. An inverter with a grid is modeled for the current control as shown in Figure 4.

**Figure 4.** The model of the inverter with the grid.

Equation (3) shows the inverter output voltage values for  $V_a$ ,  $V_b$ , and  $V_c$ :

$$\begin{aligned} V_a(t) &= Ri_a(t) + L \frac{di_a(t)}{dt} + E_a(t) \\ V_b(t) &= Ri_b(t) + L \frac{di_b(t)}{dt} + E_b(t) \end{aligned} \quad (3)$$

$$\begin{aligned} V_c(t) &= Ri_c(t) + L \frac{di_c(t)}{dt} + E_c(t) \\ V_{ds}(t) &= \frac{2V_a(t) - V_b(t) - V_c(t)}{3} \\ V_{qs}(t) &= \frac{V_b(t) - V_c(t)}{\sqrt{3}} \end{aligned} \quad (4)$$

Three-phase voltages ( $V_a$ ,  $V_b$ ,  $V_c$ ) are transformed to voltages ( $V_{ds}$ ,  $V_{qs}$ ) of stationary d-q axis by using Equation (4). The grid voltages ( $E_a$ ,  $E_b$ ,  $E_c$ ) and the grid currents ( $I_a$ ,  $I_b$ ,  $I_c$ ) are transformed to the stationary d-q axis.  $V_{ds}$  and  $V_{qs}$  are expressed as shown in Equation (5):

$$\begin{aligned} V_{ds}(t) &= Ri_{ds}(t) + L \frac{di_{ds}(t)}{dt} + E_{qs}(t) \\ V_{qs}(t) &= Ri_{qs}(t) + L \frac{di_{qs}(t)}{dt} + E_{qs}(t) \end{aligned} \quad (5)$$

The grid angle is used to change the value of the stationary d-q axis to the value of the rotating reference d-q axis. The calculated values to the rotating reference using the grid angle has only a DC-component and these are expressed as by Equation (6):

$$\begin{aligned} V_{de}(t) &= Ri_{de}(t) + L \frac{di_{de}(t)}{dt} + E_{de} \\ V_{qe}(t) &= Ri_{qe}(t) + L \frac{di_{qe}(t)}{dt} + E_{qe} \end{aligned} \quad (6)$$

where  $E_{qe}$  has a constant value that has the same magnitude of grid and  $E_{de}$  is zero.

Equation (6) is transformed into an s-domain function by the Laplace transformation. The input signal of controller is grid currents and the output signal of controller is output voltages of the inverter. The transferred function which is the system function is expressed as in Equation (7):

$$\frac{i_{qe,de}(s)}{V_{qe,de}(s) - E_{qe,de}} = \frac{1}{R + sL} \quad (7)$$

To apply the PI-controller, Equation (7) and the feed-forward components ( $V_{deff}$  and  $V_{qeff}$ ) are considered as shown in Figure 5. A proportional gain ( $K_p$ ) and a integration gain ( $K_i$ ) of the PI-controller should be selected by calculating the transfer function of Figure 5 by assuming that  $V_{deff}$  is same as  $E_{de}$  and  $V_{qeff}$  is same as  $E_{qe}$ . Then,  $E_{qe}$  and  $E_{de}$  are eliminated and the transfer function of Figure 5 can be simplified as shown in Equation (8):

$$I(s) = \frac{\frac{K_p}{L}s + \frac{K_i}{L}}{s^2 + \frac{K_p + R}{L}s + \frac{K_i}{L}} I^*(s) \quad (8)$$

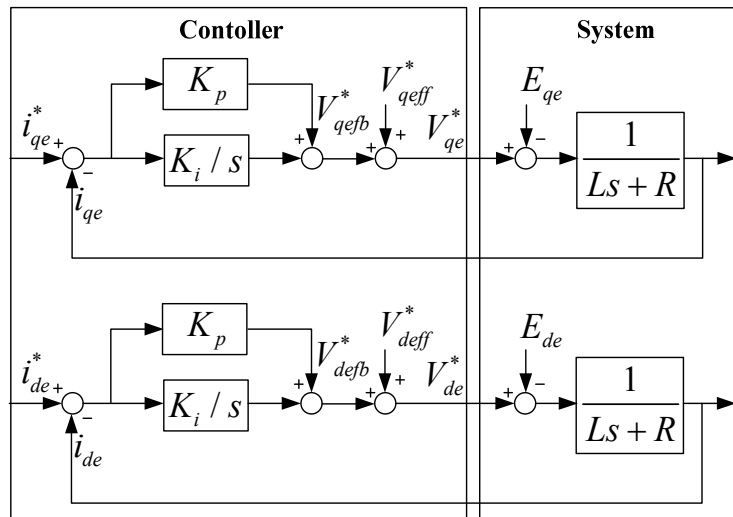
To simplify the transfer function,  $K_p$  and  $K_i$  gains are selected as shown in Equation (9).

$$\begin{aligned} K_p &= L \cdot \omega_{cc} \\ K_i &= R \cdot \omega_{cc} \end{aligned} \quad (9)$$

The transfer function can then be represented as a first-order function with a bandwidth of  $\omega_{cc}$ :

$$\frac{I(s)}{I^*(s)} = \frac{\omega_{cc}}{s + \omega_{cc}} \quad (10)$$

**Figure 5.** The current controller block diagram of the inverter.



The controller applies compensation control for the 5th and 7th harmonics. It uses a PI-controller and the fundamental angle from Rolim's PLL algorithm, which has outstanding performance owing to its use of disturbance injection [25]. This algorithm detects the grid angle ( $\theta_g$ ) by adding a low-pass filter to the basic PLL algorithm.

The 5th harmonic of the inverter's output current is compensated by transferring the output current from the stationary reference frame to the rotating reference frame. Then the 5th harmonic component is represented as the DC value by five times fundamental angle. All the other components except the DC component are then eliminated using a low-pass filter:



$$I_{ripple}(h_{sw}) = \frac{V_{dc} M_i T_s}{2\sqrt{3}L} \sqrt{\frac{[h_1(M_i) + h_2(M_i) + h_3(M_i)]}{699840\pi M_i^4}} \quad (12)$$

where  $T_s$  is the switching period,  $M_i = \frac{\sqrt{2}E_n}{V_{dc}}$  and:

$$\begin{aligned} h_1(M_i) &= \sqrt{3M_i^2 - 4\sqrt{3}M_i} + 4 \cdot (3375M_i^5 - 4014\sqrt{3}M_i^4 + 1692M_i^3 + 1128\sqrt{3}M_i^2 + 96M_i + 64\sqrt{3}) \\ h_2(M_i) &= \sqrt{3M_i^2 - 2\sqrt{3}M_i} + 1 \cdot (-41040M_i^5 + 31248\sqrt{3}M_i^4 - 7632M_i^3 - 2544\sqrt{3}M_i^2 - 384M_i - 128\sqrt{3}) \\ h_3(M_i) &= (-114480M_i^4) \cdot (\sqrt{3}M_i^2 - \frac{163}{212}\pi M_i^2 + \frac{12}{53}\sqrt{3}M_i + \frac{459}{530}M_i + \frac{9}{53}\sqrt{3} - \frac{33}{106}\pi) \end{aligned} \quad (13)$$

From Equation (12), the high DC-link voltage can cause a THD increment. Furthermore, the results of the designed L-filter values according to the DC-link voltage are presented in [31]. These results show that in the high DC-link voltage, a large value inductance is needed to maintain the current ripple equal to that of the low DC-link voltage. Equation (12) and the results from [31] cover the inductance of the L-filter. In the LC-filter and LCL-filter design, the inductance calculation is based on the L-filter design method and the C-part or the CL-part is chosen for the additional ripple reduction.

If the inverter uses a higher DC-link voltage, a large filter will be needed for the same performance as the inverter with a DC-link voltage of 600 V. On the other hand, a higher DC-link voltage is necessary to achieve a wider MPPT range. The increase in THD for better performance is acceptable when the input voltage is greater than 600 V. However, it is unnecessary to increase THD when the input voltage is less than 600 V.

If the MPP voltage of PV cells is 655 V in the curve of Figure 7 and the DC-link reference voltage is 600 V, the boost converter does not operate and the voltage of the PV cells is maintained at 600 V. This result is shown in Figures 7 and 8. Although the PV cells maximum power is set to 9785 W, the power from the PV cells is 9512 W because the inverter controls the DC-link voltage to be 600 V. Also the duty-cycle of the boost converter is zero. It means that the boost converter is not operating. The power loss is 233 W (*i.e.*, 9785–9552 W) due to the tracking limitation. As the MPP voltage is increased, the power loss is larger.

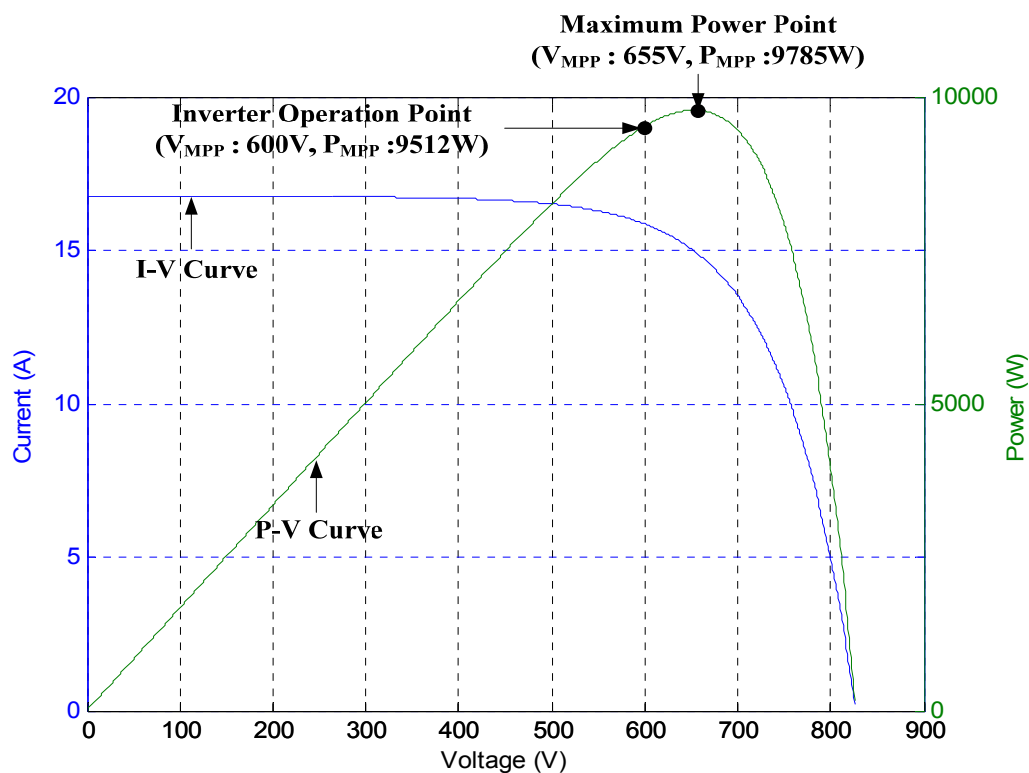
The maximum power is transferred by setting the DC-link reference voltage to be larger than the MPP voltage of PV cells. Figure 9 shows these results. The DC-link voltage is 750 V, and the PV cells voltage is 655 V like the MPP voltage. The duty of boost converter is not zero because the MPPT algorithm is performed by the boost converter. In contrast with the result of Figure 8, the power from the PV cells is increased to 9785 W which is the PV cells' maximum power. Therefore, we propose a DC-link voltage control method that is based on the input voltage.

Equation (14) expresses the optimal method for changing the DC-link voltage over 600 V:

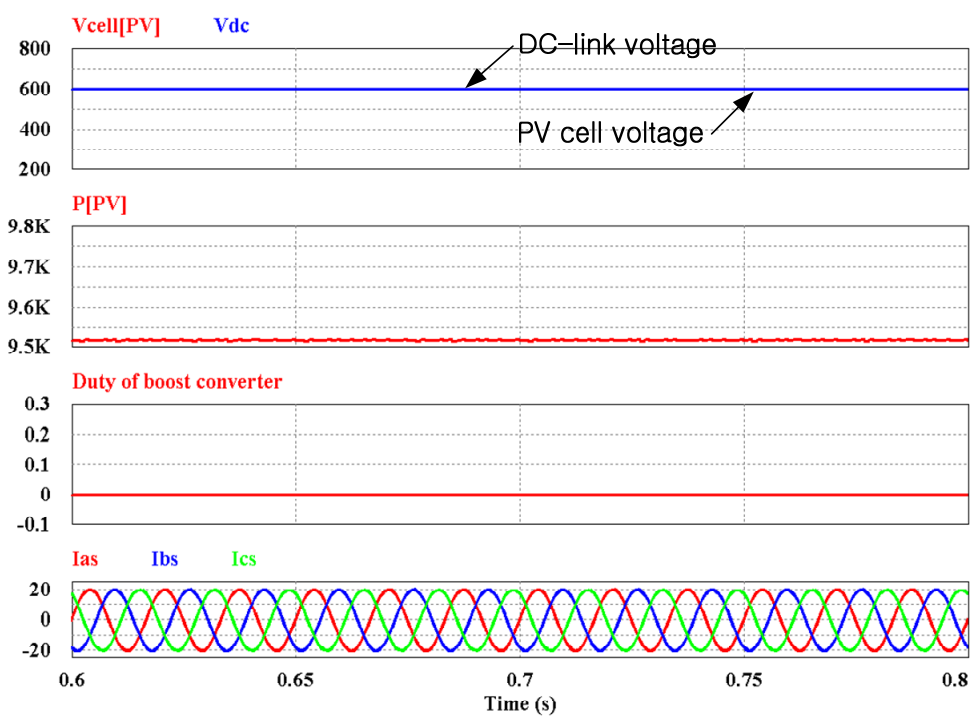
$$V_{DC-link} = V_{in} + \Delta V \quad (14)$$



**Figure 7.** The inverter operation point and the maximum power operation point in the PV cells characteristic curve.



**Figure 8.** Simulation results: MPP is 655 V and the DC-link reference voltage is 600 V.



**Figure 9.** Simulation results: MPP is 655 V and the DC-link reference voltage is 750 V.

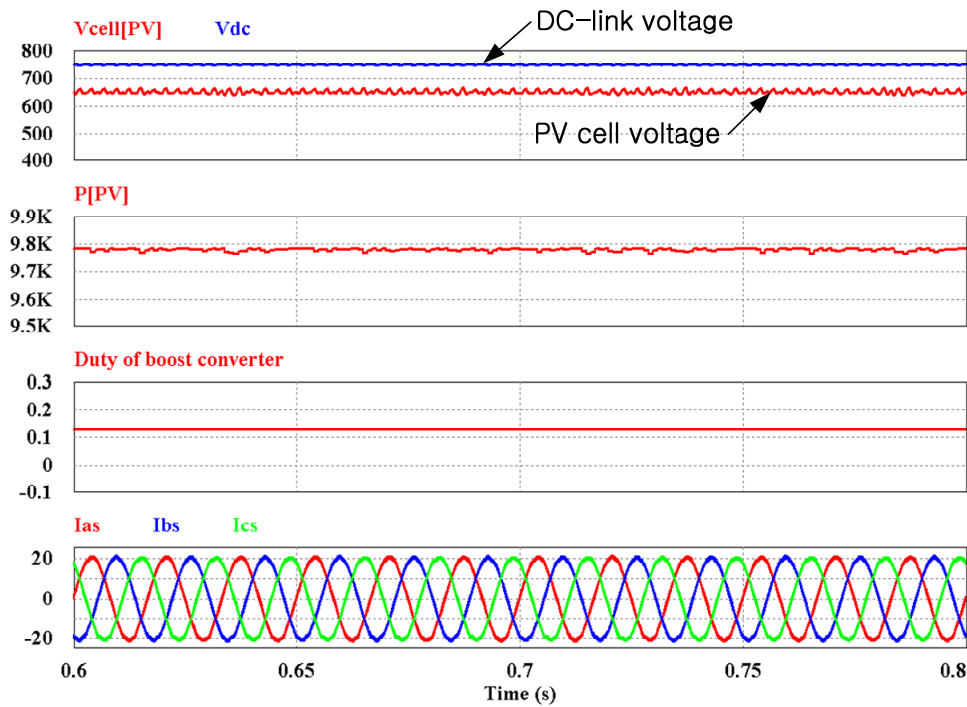
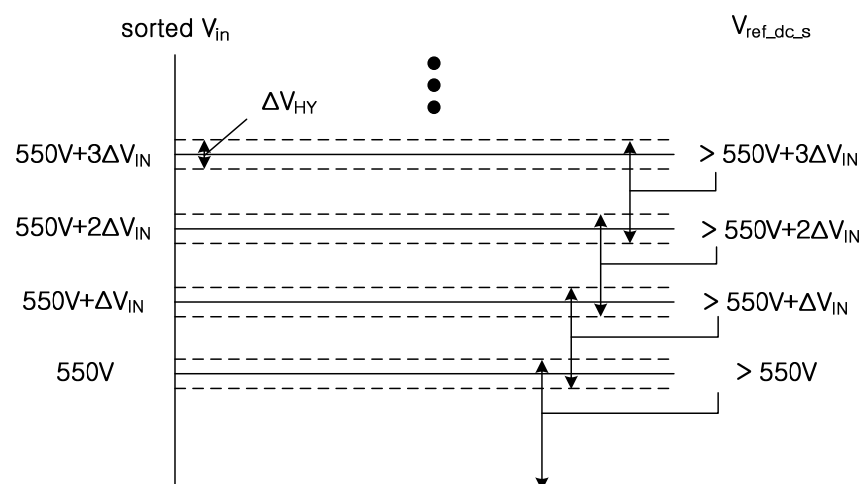


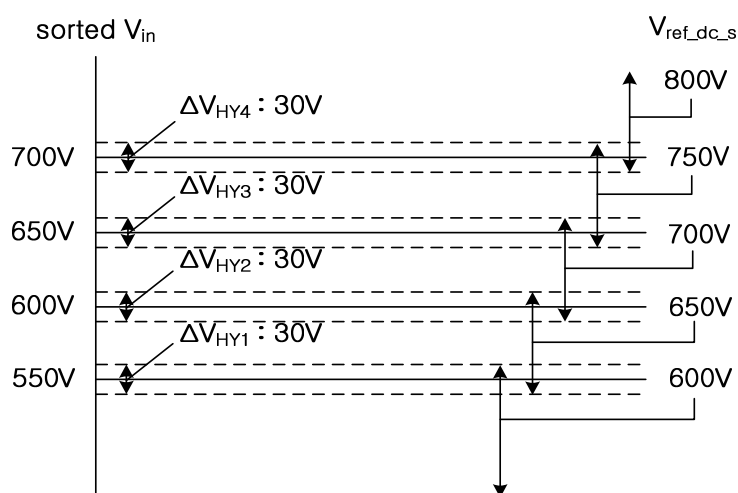
Figure 10 shows a basic concept of the proposed algorithm. The performance characteristics and THD of the output current are determined by the selection of  $\Delta V_{IN}$  and  $\Delta V_{HY}$ . THD will be unnecessarily increased if  $\Delta V_{IN}$  is too large; therefore, a relatively small value has to be chosen for  $\Delta V_{IN}$  by considering the sensing noise. This noise causes frequent changes in the DC-link voltage reference. Moreover,  $\Delta V_{IN}$  should be larger than the variation of the DC-link voltage.

**Figure 10.** Range setting of the variable DC-link algorithm.



If the variation is larger than  $\Delta V_{IN}$ , the DC-link reference is changed continuously. This also causes the stability problem.  $\Delta V_{HY}$  must be chosen to prevent the change in the DC-link reference voltage at the boundary between input voltages and is not applied at the system initialization. The DC-link controller should not generate any overshoot because the overshoot halted the power delivery from the PV cells to the DC-link capacitor which leads to that the PV cells voltage increases to change the DC-link reference voltage. Therefore, the actual DC-link reference voltage ( $V_{ref\_dc\_a}$ ) is designed to produce a ramp response after the DC-link voltage is selected ( $V_{ref\_dc\_s}$ ) according to the sorted input voltage. The ramp response is calculated on the basis of the cut-off frequency of the DC-link voltage controller and should be slower than the response of the DC-link voltage controller. Finally, this algorithm is related to the MPPT operation of the boost converter. The boost converter should quickly increase and decrease the duty of the boost converter to maintain the current output power during the DC-link reference change. There are two cases of the DC-link reference change. One is when the DC-link reference is increased and another is when the DC-link reference is decreased. In the first case, the boost converter with the slow response speed cannot deliver the power of the PV cells due to the sudden DC-link voltage increase and the small duty it previously had. This means that the current of the PV cells is decreased and the input voltage of the PV cells is increased simultaneously and then the DC-link reference voltage is increased once more. Consequently, the DC-link voltage is increased until the input voltage of the PV cells becomes the same as the open voltage of the PV cells. In the second case, the boost converter cannot deliver the power due to the previous large duty. This previous large duty causes the large current and the PV (input) voltage to be decreased. Consequently, the DC-link reference voltage is decreased to the initial voltage of DC-link reference. The proposed algorithm has been simulated and demonstrated experimentally with the settings as shown in Figure 11.

**Figure 11.** The used range in the simulations and the experiments.



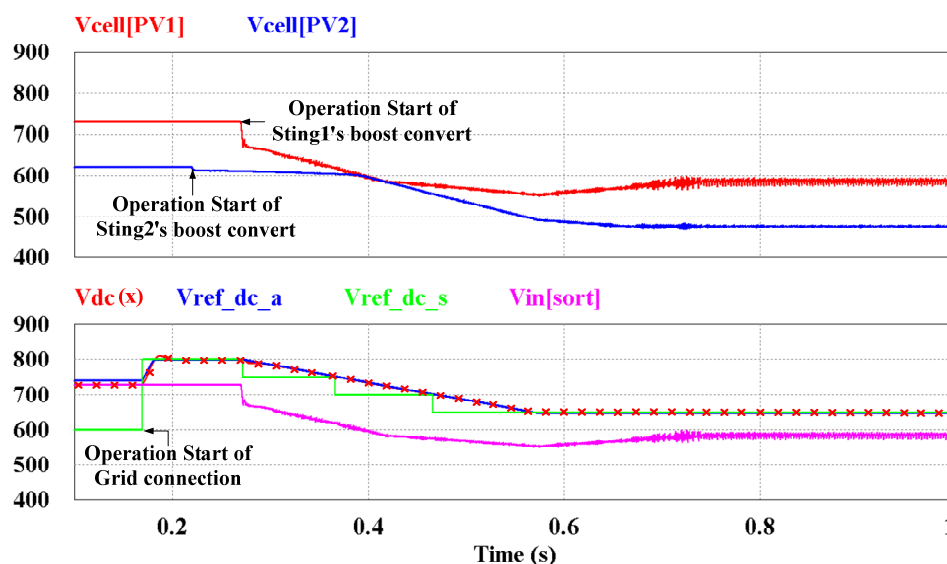
The maximum voltage of the PV cells is assumed to be lower than 800 V. By considering the noise component of the experimental set, the value of  $\Delta V_{IN}$  has been chosen through experiments as 50 V to minimize the increment of THD; the value of  $\Delta V_{HY}$  is 30 V.

#### 4. Simulation

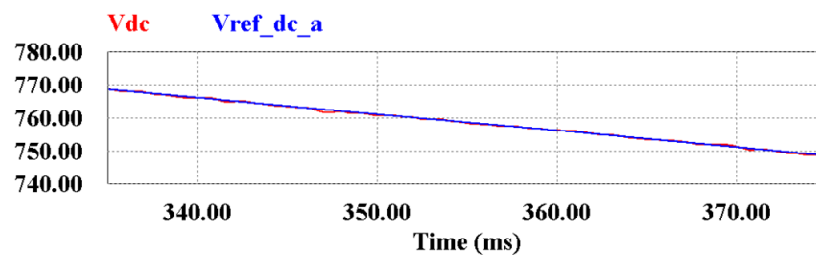
The proposed algorithm has been simulated using PSIM. The simulation circuit is as shown in Figure 1. The circuit parameters are chosen for a 10 kW system. The input inductances of the boost converters are 1.5 mH, the capacitance of DC-link capacitor is 1100  $\mu$ F, and the inductance and capacitance of LC-filter parameters are 2 mH and 4.7  $\mu$ F. The switching frequency for both the boost converter and the inverter is 20 kHz. The three-phase grid uses a 380 V line-to-line voltage. The  $\omega_n$  value for the DC-link voltage controller is 300 rad/s, and 500 V/s is used as the ramp response of the DC-link reference voltage. The period of the MPPT algorithm calculation is 0.05 s and  $\Delta$ duty-cycle is 0.005. The temperature of the PV cells is increased or decreased in order to characterize the performance of the algorithm.

Figure 12 illustrates the performance of the proposed algorithm when the PV system is initiated. The temperature of PV1 is set as the lower value than that of PV2. The initial DC-link reference voltage is 600 V, but is then set to 800 V in accordance with Figure 11 because the sorted voltage is 730 V (the input voltage of PV1 is 730 V). The input voltage decreases when the boost convert starts operating. The decrease in the input voltage changes the DC-link reference. The selected DC-link voltage and the actual DC-link reference voltage with the 500 V/s ramp response is changed according to Figure 11.

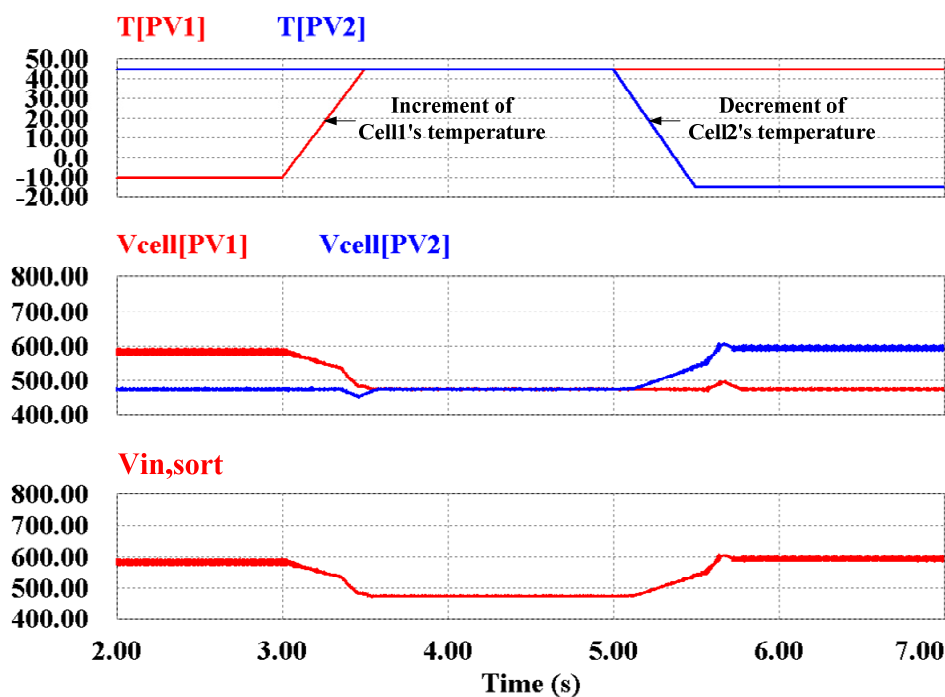
**Figure 12.** Simulation results for the PV cells voltages, the DC-link voltage,  $V_{ref\_dc\_a}$ ,  $V_{ref\_dc\_s}$ , and  $V_{in,sort}$  from Figure 11 when the PV system is initiated.



During the operation, the DC-link voltage is maintained over the sorted input voltage. This approach yields the minimum THD. By choosing the slower ramp response than the response of the DC-link voltage controller, the DC-link voltage follows the DC-link reference voltage as shown in Figure 13.

**Figure 13.** Simulation results for the DC-link voltage and  $V_{ref\_dc\_a}$ .

Figures 14 and 15 show the system's performance when the temperature of PV1 is increased from  $-10\text{ }^{\circ}\text{C}$  to  $45\text{ }^{\circ}\text{C}$  for 0.5 s and the temperature of PV2 is decreased from  $45\text{ }^{\circ}\text{C}$  to  $-15\text{ }^{\circ}\text{C}$  for 0.5 s. The input voltage of PV1 decreases owing to the increase in the temperature, and the sorted voltage is chosen as the voltage of PV1. At this point, the MPPT algorithm of the string 1's boost converter increases the duty-cycle to find MPP. In addition, the DC-link reference voltage decreases to 600 V when the sorted voltage decreases below the minimum of  $\Delta V_{HY3}$ . Therefore the magnitude of the grid current is decreased because the PV's temperature increase reduces its maximum power. Similarly, the input voltage of PV2 increases owing to the decrease in temperature, and the sorted voltage becomes the input voltage of PV2. Thus the DC-link reference voltage is selected according to the voltage of PV2. The DC-link reference voltage changes to 650 V when the sorted voltage increases above the maximum of  $\Delta V_{HY3}$ . In addition, the duty-cycle of the MPPT algorithm for string 2's boost converter is decreased to determine MPP and the grid current is increased.

**Figure 14.** Simulation results for the temperatures of the PVs, two PV cells voltages, and the sorted voltage ( $V_{in,sort}$ ) when the temperatures of the PV cells are changed.

**Figure 15.** Simulation results for the DC-link voltage,  $V_{ref\_dc\_a}$ ,  $V_{ref\_dc\_s}$ ,  $V_{in,sort}$ , grid currents and duty-cycles of the boost converters when the temperatures are changed.

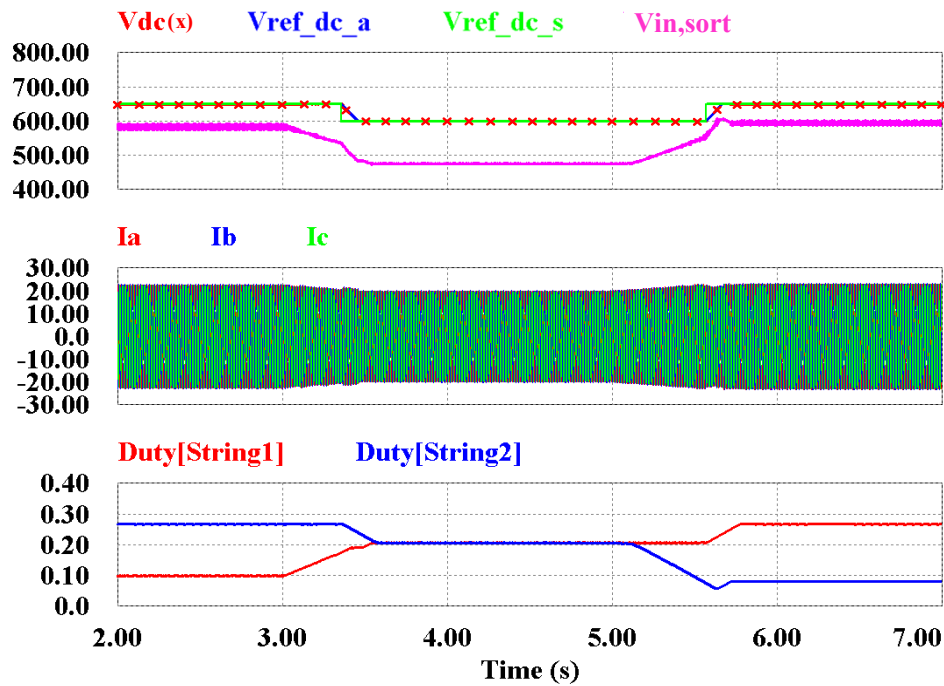
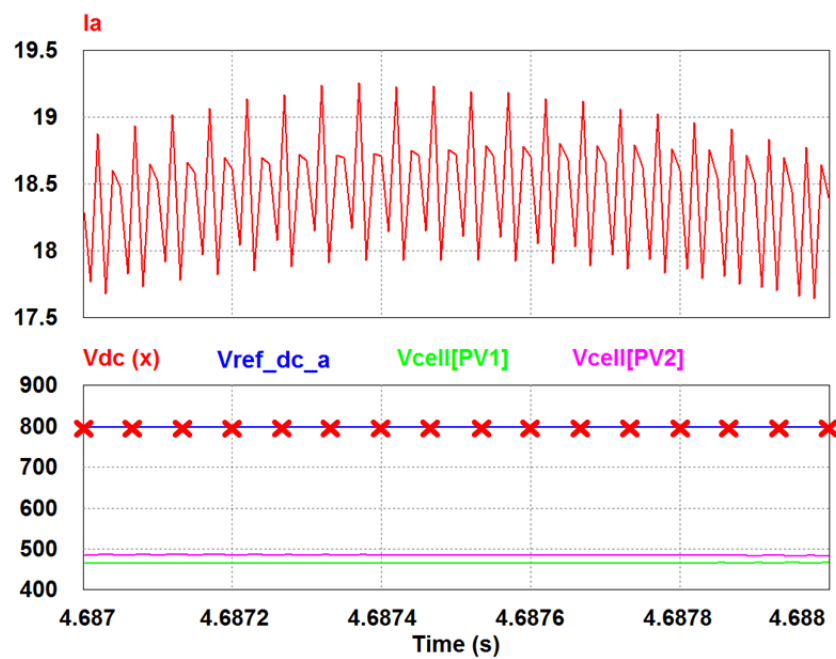


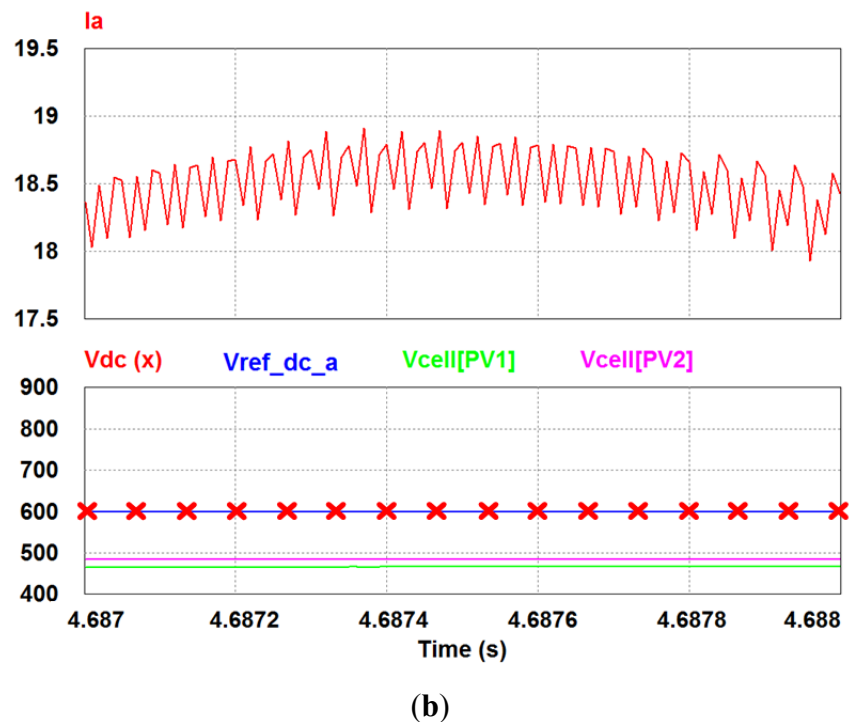
Figure 16a shows the results of the simulation using the DC-link reference voltage to 800 V at the same conditions and Figure 16b is enlarged from Figure 15.

**Figure 16.** Simulation results for the a-phase current, the DC-link voltage,  $V_{ref\_dc\_a}$  and two PV cells voltages according to the DC-link reference voltage 800 V (a) and 600 V (b).



(a)

Figure 16. Cont.

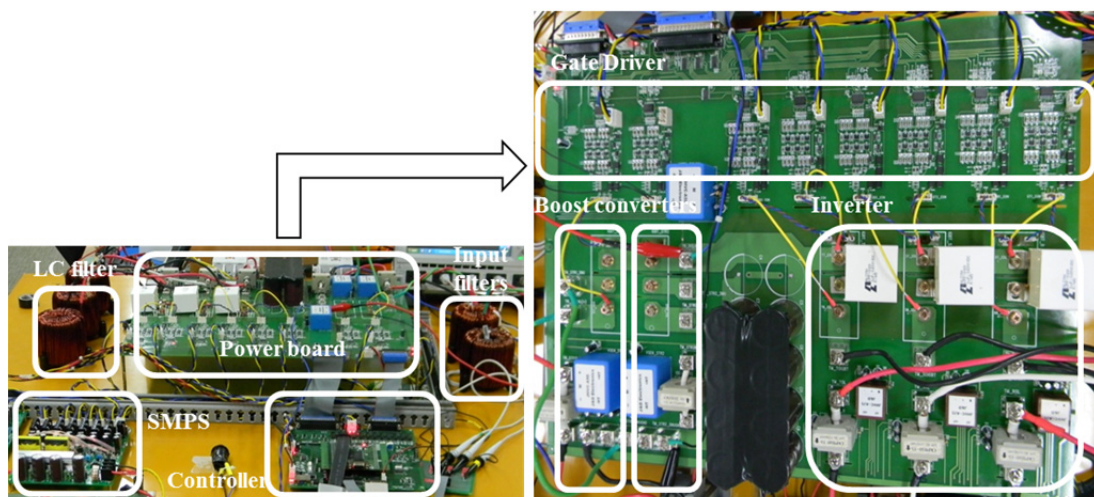


These shows that the a-phase current ripples are different according to the DC-link reference voltage. In Figure 16a, the peak-to-peak value of the a-phase current ripple is 1 A when the DC-link reference voltage is set to 800 V. However, when the DC-link reference voltage is set to 600 V, the peak-to-peak value of the a-phase current ripple is 0.6 A in Figure 16b. From the results, it is identified that changing the DC-link reference voltage according to the sorted voltage reduces THD increase.

#### 4. Experimental Section

The algorithm has been tested using a 10 kW experimental setup. The experimental set consists of an inverter and two boost converters as shown Figure 1; a photograph of the electronics is shown in Figure 17.

Figure 17. Experimental setup of the 10kW two-string PV system.

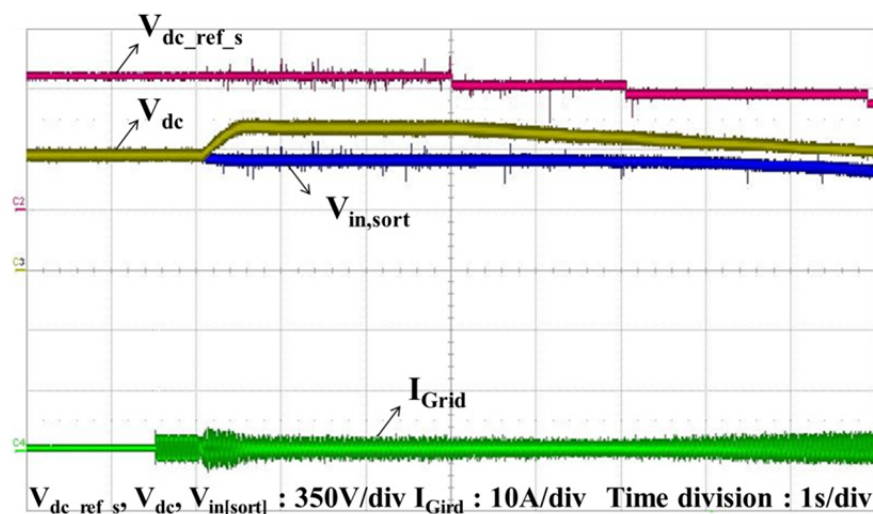




The rated powers of the string 1 and string 2 boost converters are 7 kW and 3 kW. The rated power of the inverter is 10 kW. Most of the system parameters are the same as those used in the simulations: two input inductances of the boost converters are 1.5 mH, the capacitance of the DC-link capacitor is 1100  $\mu$ F, and the inductance and capacitance of LC-filter parameters are 2 mH and 4.7  $\mu$ F. The switching frequency for both the boost converter and the inverter is 20 kHz, and the three-phase grid uses a 380 V line-to-line voltage. However,  $\omega_n$  for the DC-link voltage controller is chosen to be 30 rad/s for system stability, and the ramp response of the DC-link reference voltage is 50 V/s. The calculation period for the MPPT algorithm is 0.5 s and  $\Delta$ duty-cycle is 0.005.

The inputs are connected to PV simulators. The temperature and solar radiation of the PV cells are increased or decreased to characterize the performance of the algorithm by using simulator software. A temperature change is applied to the simulator of string 1. Figure 18 shows the experimental results when the PV system is initiated.

**Figure 18.** Experimental results for the DC-link voltage,  $V_{in,sort}$  and  $V_{ref\_dc\_s}$  from Figure 11 when the PV system is initiated.

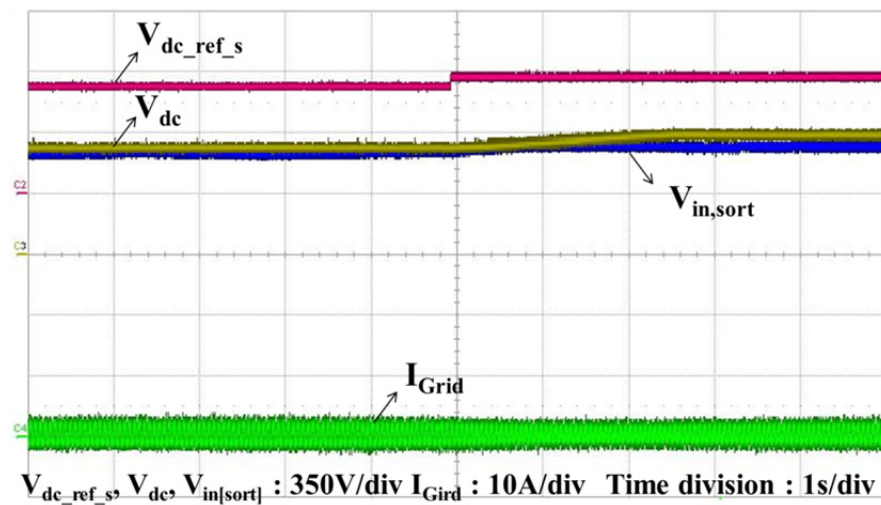


The DC-link reference voltage is chosen to be 800 V because the sorted voltage is higher than 700 V. The system operation is the same as that in simulations. The MPPT algorithm causes the sorted voltage to decrease and the grid current to increase; the DC-link reference voltage is decreased according to the sorted voltage.

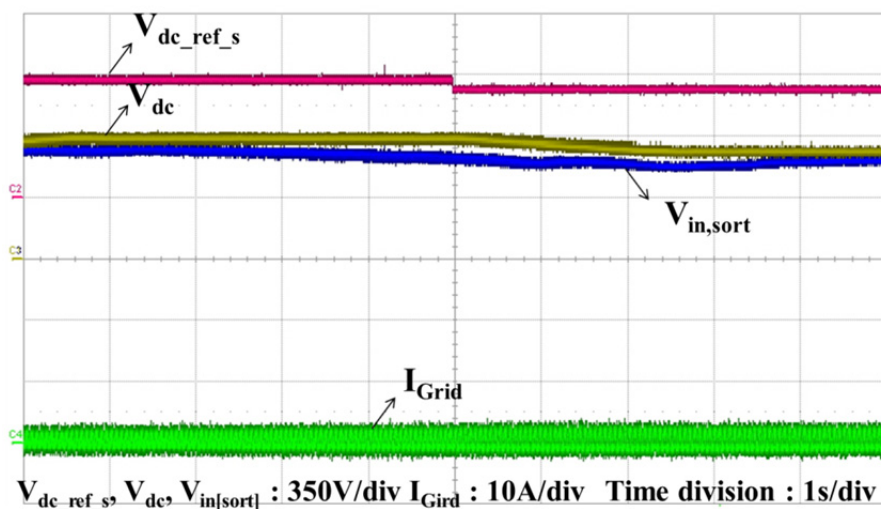
Figures 19 and 20 show the change in the DC-link reference voltage that occurs owing to the sorted voltage. The temperature of PV1 is changed from 30  $^{\circ}$ C to 10  $^{\circ}$ C, as shown in Figure 19, and the effects are shown in Figure 21. The points of Figure 21 present the operation point of the PV system. The DC-link voltage increases with the increase in the sorted voltage from 650 V to 700 V. The MPPT algorithm is appropriately carried out during  $\Delta$ temperature. Figure 20 plots the waveforms when the temperature of PV1 changes from 10  $^{\circ}$ C to 30  $^{\circ}$ C. In contrast with Figure 19, the sorted voltage is decreased and the DC-link reference voltage is decreased, as well.



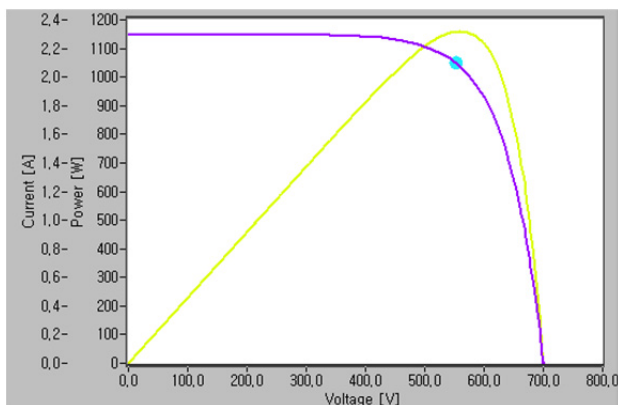
**Figure 19.** Experimental results for the DC-link voltage,  $V_{in,sort}$  and  $V_{ref\_dc\_s}$  from Figure 11 when the temperatures of PV1 is decreased.



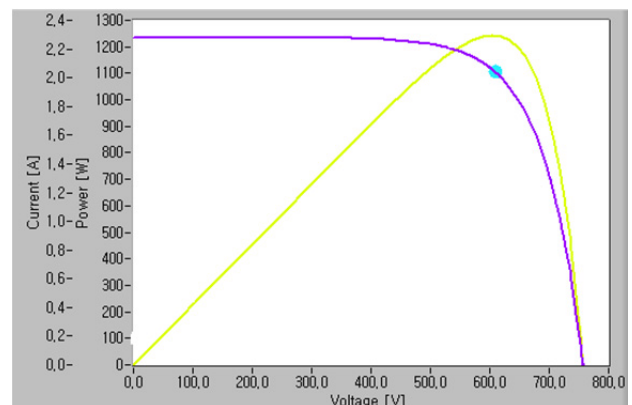
**Figure 20.** Experimental results for the DC-link voltage,  $V_{in,sort}$  and  $V_{ref\_dc\_s}$  from Figure 11 when the temperatures of PV1 is increased.



**Figure 21.** PV-curves of a PV simulator according to the temperature: (a) 30 °C and (b) 10 °C.



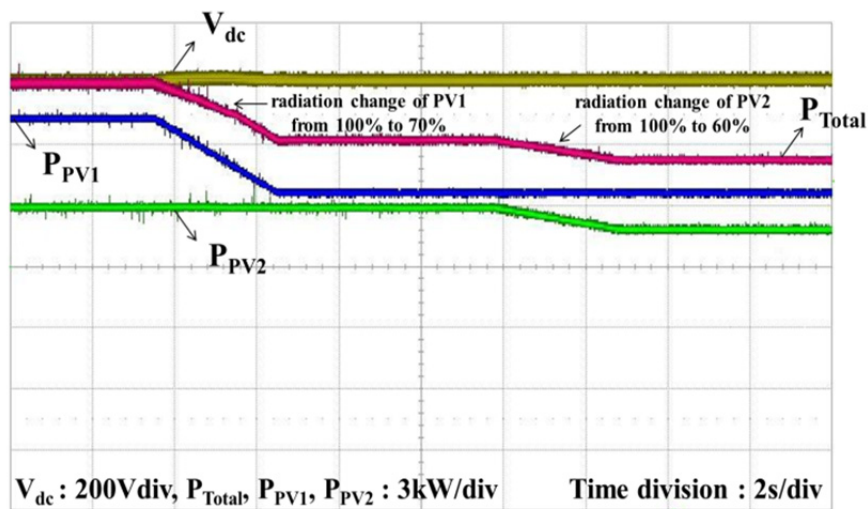
(a)



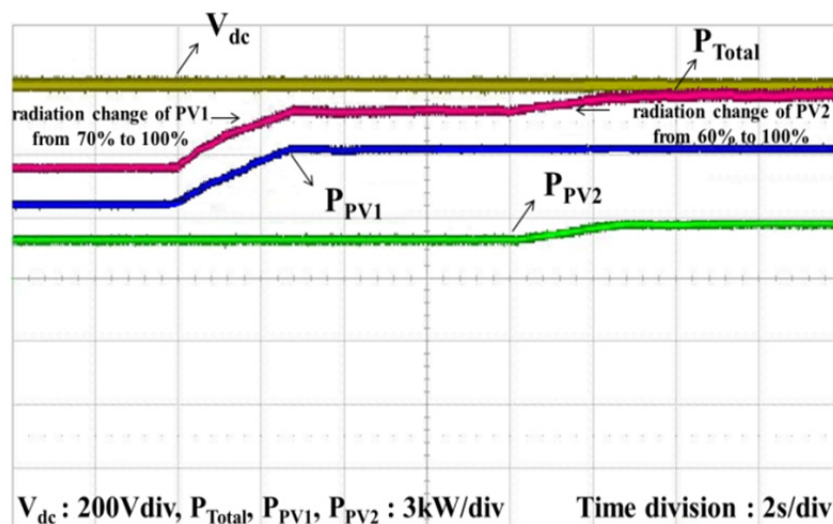
(b)

Figures 22 and 23 show the powers waveforms when the radiation is altered. In Figure 22, the radiation of PV1 is changed from 100% to 70%, and the radiation of PV2 is changed from 100% to 60%. The radiation of PV1 is changed from 70% to 100% and the radiation of PV2 is changed from 60% to 100% in Figure 23. The change in radiation does not cause the voltage of the PV cells to increase. Therefore, the DC-link voltage also remains unchanged. The total power changes, however, because the PV powers are increased or decreased. In this case, the maximum power point tracking is well conducted by the MPPT algorithm and is shown in Figure 24.

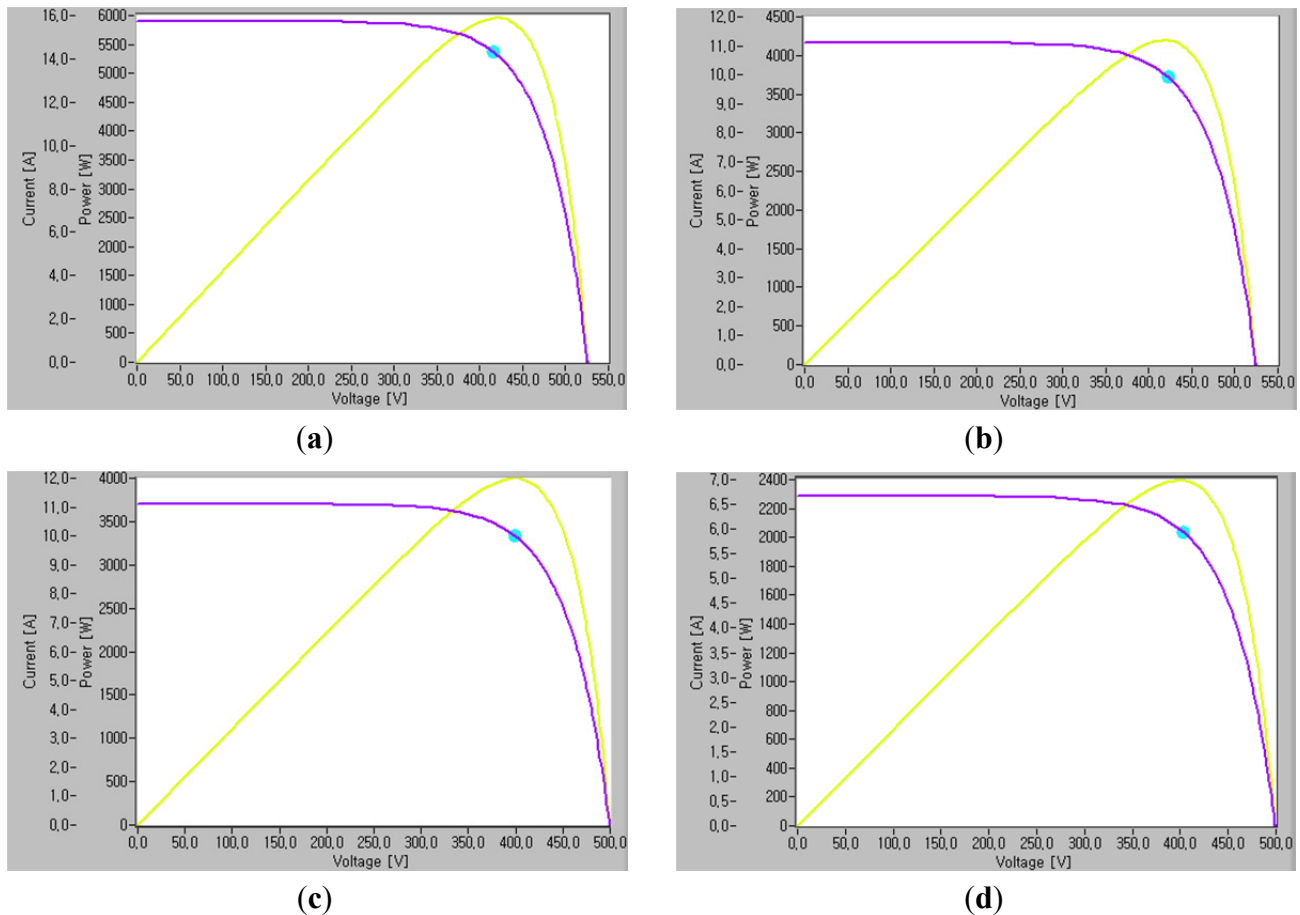
**Figure 22.** Experimental results for powers of inputs and output when the radiation of PVs is decreased.



**Figure 23.** Experimental results for powers of inputs and output when the radiation of PV is increased.



**Figure 24.** PV-curves of PV1 and PV2 according to radiation. (a) PV-curve of PV1 at radiation of 100%; (b) PV-curve of PV1 at radiation of 70%; (c) PV-curve of PV2 at radiation of 100%; (d) PV-curve of PV2 at radiation of 60%.



## 5. Conclusions

In this paper, we have proposed a variable DC-link control method that provides minimization of the THD increase and a wide MPPT range in a two-string PV system. We have also described the configuration of the two-string PV system, the inverter control for the grid connection, and the boost converter control for MPPT. The variable DC-link reference voltage algorithm has been applied to the PV system. This algorithm changes the DC-link reference voltage according to the sorted input voltage and a table that sets the range and the hysteresis. Finally, we have presented simulations and experimental results that verify the performance of the proposed algorithm and demonstrated its wide range of MPPT.

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