



Article Research on Active Collision Avoidance and Hysteresis Reduction of Intelligent Vehicle Based on Multi-Agent Coordinated Control System

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Abstract: This paper provides a multi-agent coordinated control system to improve the real-time performance of intelligent vehicle active collision avoidance. At first, the functions and characteristics of longitudinal and lateral collision avoidance agents are analyzed, which are the main components of the multi-agent. Then, a coordinated solution mechanism of an intelligent vehicle collision avoidance system is established based on hierarchical control and blackboard model methods to provide a reasonable way to avoid collision in complex situations. The multi-agent coordinated control system can handle the conflict between the decisions of different agents according to the rules. Comparing with existing control strategies, the proposed system can realize multi decisions and planning at the same time; thus, it will reduce the operation time lag during active collision avoidance. Additionally, fuzzy sliding mode control theory is introduced to guarantee accurate path tracking in lateral collision avoidance. Finally, co-simulation of Carsim and Simulink are taken, and the results show that the real-time behavior of intelligent vehicle collision avoidance can be improved by 25% through the system proposed.

Keywords: multi-agent coordinated control system; active collision avoidance; blackboard model; real-time

1. Introduction

With the development of the intelligent vehicle, studies on the active collision avoidance system of intelligent vehicles have attracted more and more attention. Based on the perception of the driving environment, the intelligent vehicle can avoid collision risk by braking or steering.

To improve the performance of intelligent vehicles' active collision avoidance system, researchers have carried out effective research on longitudinal and lateral avoidance. In the aspect of longitudinal collision avoidance, Li Suhua et al. [1] proposed a longitudinal collision avoidance method for electric vehicles, establishing a safe distance model with consideration of road adhesion coefficient and driving intention. Li Shifu et al. [2] made a theoretical derivation of the critical distance of the warning and the critical distance based on the braking process and obtained a safe distance model considering the emergency of the preceding vehicle. Considering the characteristics of vehicle dynamics and synthesizing the influence of road environment and vehicle factors, an RV hierarchical safety distance model was established in the paper [3]. Hou Dezao et al. [4] designed the upper controller based on the optimal tracking theory and driver priority principle.



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). In the aspect of lateral collision avoidance, Boada et al. [5] designed an emergency steering path tracking controller with a fuzzy control logic method based on vehicle yaw rate. Soudbakhsh et al. [6] constructed the state equation with actual lateral acceleration, ideal lateral acceleration, yaw angle, and ideal yaw angle error. Li Wei et al. [7] proposed a lane change path planning method with an RBF neural network in which the boundary conditions of the path planning algorithm and path change based on polynomials are designed. This method has advantages in complex road conditions. Papers [8,9] studied the braking and steering modes based on the analysis of the vehicle braking process to design a longitudinal safety distance model under various working conditions and braking controllers [8]. In paper [9], the longitudinal and lateral safety distance models were also designed with different collision avoidance methods by analyzing the state of the preceding vehicle. Paper [10] introduced the advantages and shortcomings of the traditional APF method, solving the problem of excessive initial attractive force and the intelligent vehicle cannot reach the target by improving the potential field functions.

It can be seen from the above results that most active collision avoidance systems currently focus on a single collision avoidance method, and there is no reasonable integration of longitudinal and lateral collision avoidance. With the increasingly complex driving conditions of smart cars, the independent active collision avoidance method is difficult to meet the driving requirements of intelligent cars due to its poor flexibility. Therefore, under the premise of ensuring the timeliness of active safety control, it is of great significance to design a comprehensive coordinated control strategy for longitudinal collision avoidance and lateral collision avoidance. At present, most researchers believe that an agent is a computing entity with a life cycle that exists in a specific environment and has the characteristics of real-time perception of the surrounding environment and the ability to operate independently and affect the environment [11,12]. A single agent mainly has four basic characteristics: autonomy, sociality, responsiveness, and initiative. A Multi-Agent System (MAS, Multi-Agent System) is composed of multiple single agents. Through the coordinated control of each agent, its problem-solving ability is far beyond the ability of a single agent, so the multi-agent system is widely used in the coordinated control of complex systems [13,14]. A novel hybrid artificial intelligence-layered multi-agent architecture was presented in the paper [15] to help the digital transformation of energy and the smart grid.

In this paper, an intelligent vehicle active collision avoidance method based on a multiagent coordinated control system is designed. The longitudinal and the lateral collision avoidance agents are designed based on the blackboard model, to provide reasonable collision avoidance way under different driving conditions. This proposed system can realize the multi-parallel operation of decision and planning at the same time. The lateral and the longitudinal collision avoidance agent can provide collision avoidance planning simultaneously, which can achieve the integration of collision avoidance decisions and planning. It will help reduce the time lag caused by the collision avoidance decisionplanning process and improve real-time performance.

The rest of this paper is organized as follows. In Section 2, the main agents of the intelligent vehicle are produced. In Section 3, the blackboard model is introduced to coordinated control of each agent, and the real-time performance of the multi-agent active collision avoidance system is evaluated through simulations in Section 4, followed by some concluding remarks in Section 5.

2. Main Agents

Decision-making agents with lateral collision avoidance and longitudinal collision avoidance are designed in this section to provide decisions for collision avoidance.

2.1. Longitudinal Collision Avoidance Agent

The safety distance model [16] of the longitudinal collision avoidance agent is designed as Equations (1) and (2):

$$S_l = \frac{V_r^2}{2a_{r-max}} + V_r(t_{detect1} + t_{decision1} + t_{excution1}) + d_0 \tag{1}$$

$$a_{r-max} = \begin{cases} \mu g cos\alpha - g sin\alpha & (downhill) \\ \mu g & (zero slope) \\ \mu g cos\alpha + g sin\alpha & (uphill) \end{cases}$$
(2)

where $t_{detect1}$ is the environment perception time, $t_{decision1}$ is the decision-planning time of the longitudinal collision avoidance agent, $t_{excution1}$ is the mechanical delay time, V_r is the vehicle speed, a_{r-max} is the maximum braking deceleration of the vehicle, d_0 is the minimum safety threshold between vehicles, μ is the coefficient of road adhesion, g is the acceleration of gravity and α is the vehicle slope angle.

A longitudinal collision avoidance agent is designed to get a safe distance from obstacles in front of the intelligent vehicle. Brake pressure will be calculated if a smaller distance between the obstacle and the intelligent vehicle than the safety distance is detected.

The analysis of vehicle forces during braking is made to get the brake pressure and the diagram is shown in Figure 1.



Figure 1. Diagram of vehicle force during braking.

The force balance equation of the vehicle is shown in Equation (3):

$$ma_{des} = F_t - F_{Xb} - \sum F(V_r) \tag{3}$$

 F_w is the air resistance force, T_s is the driving torque, T_{bf} and T_{br} are the braking torque of the front and rear wheels, F_f and F_r are the ground friction of the ground acting on the front and rear wheels, W_f and W_r are the vertical force of the front and rear wheels, F_t is the driving force, F_{Xb} is the braking force, and $\sum F(V_r)$ is the total resistance.

Air resistance and ground friction are shown in Equation (4):

$$\sum F(V_r) = \frac{1}{2} C_D A_a \rho v V_r^2 + mgf \tag{4}$$

Desired braking pressure can be calculated based on Equations (3) and (4), which is shown in Equation (5):

$$P_{des} = \frac{|ma_{des} + \frac{1}{2}C_D A_a \rho v V_r^2 + mgf|}{K_b}$$
(5)

 P_{des} is the desired braking pressure and K_b is the braking pressure ratio.

Most important of all, the braking force is represented approximately as a linear function of oil pressure in the brake system, as shown in Equation (6):

$$\frac{T_{bf} + T_{br}}{r_r} = K_b P_b \tag{6}$$

 r_r is the rolling radius of wheels, and P_b is the pressure of the brake pipe.

2.2. Lateral Collision Avoidance Agent

A fifth-order polynomial lane-changing model is used in this paper to present a lateral collision avoidance agent [17]:

$$y(x) = y_e \left[10(\frac{x}{x_e})^3 - 15(\frac{x}{x_e})^4 + 6(\frac{x}{x_e})^5\right]$$
(7)

 y_e is the lateral displacement for the vehicle to avoid a collision.

Longitudinal speed V_r is considered constant during the lane-changing and the relationship between trajectory and time can be shown as Equation (8):

$$y(t) = y_e [10(\frac{t}{t_e})^3 - 15(\frac{t}{t_e})^4 + 6(\frac{t}{t_e})^5]$$
(8)

 t_e is the lane-changing time, $x_e = V_r t_e$.

The equation of lateral acceleration in the course of vehicle lane change can be obtained based on Equation (8), which is shown in Equation (9):

$$\ddot{y(t)} = a_y(t) = \frac{60y_e}{t_e^5} [2t^3 - 3t_e t^2 + t_e^2 t]$$
(9)

The maximum lateral acceleration during the process can be calculated by Equation (10):

$$a_{ymax} = \frac{10\sqrt{3}y_e}{3t_e^2} \tag{10}$$

It can be seen from Equation (10) that the maximum lateral acceleration during the lane-changing process is related to the lane-changing time t_e and the lateral distance y_e . The minimum lane-changing time of the intelligent vehicle on dry asphalt pavement and wet asphalt pavement is set to 1.68 s and 2.1 s, and the maximum lateral accelerations are 7.67 m/s² and 4.91 m/s².

As shown in Figure 2, to avoid collision with the front obstacle, the lateral displacement of the right-corner vehicle should be greater than the width of the obstacle W_b [18].



Figure 2. Intelligent vehicle lateral collision avoidance route.

Assuming that there is no vehicle in adjacent lanes. The lateral displacement of point A should meet the requirement of Equation (11) based on the path provided in Equation (11):

$$W_b = y_e \left[10 \left(\frac{t_c}{t_e}\right)^3 - 15 \left(\frac{t_c}{t_e}\right)^4 + 6 \left(\frac{t_c}{t_e}\right)^5 \right] - \left(\frac{W_s}{2}\right)$$
(11)

where W_s is the vehicle width, t_c is the collision time, W_b is the lateral distance between the obstacle edge and the vehicle center.

The longitudinal displacement S_a of the vehicle can be calculated as Equation (12):

$$S_a = V_r(t_c + t_{detect2} + t_{decision2} + t_{excution2})$$
(12)

where $t_{detect2}$ is the perception delay, $t_{decision2}$ is the decision-planning time and $t_{excution2}$ is the steering mechanical delay.

The minimum longitudinal safety distance to accomplish horizontal change is shown in Equation (13):

$$S_{fmin} = S_a + L_{OA} - L + d_0$$
 (13)

The lateral collision avoidance agent is designed to calculate the desired steering wheel angle to follow the preset collision avoidance trajectory. A fuzzy sliding mode control, which has good robustness and real-time performance, is introduced to ensure the accuracy of the path tracking of the vehicle during the lateral collision avoidance process.

The yaw rate and derivative of the sideslip angle based on the vehicle two DOF model are shown in Equation (14) [19–21]:

$$\begin{cases} \dot{\omega} = \frac{a^2 C_f + b^2 C_r}{I_z v_r} \omega + \frac{a C_f - b C_r}{I_z} \beta - \frac{a C_f}{I_z} \delta\\ \dot{\beta} = \left(\frac{a C_f - b C_r}{M v_r^2} - 1\right) \omega + \frac{C_f + C_r}{M v_r} \beta - \frac{C_f}{M v_r} \delta \end{cases}$$
(14)

 β is the sideslip angle. v_y is the lateral speed. *M* is the vehicle mass. ω is the yaw rate. *a* and *b* are the front and rear wheelbase. I_z is the vehicle's moment of inertia. C_f and C_r represent the stiffness of the front and rear tires.

The vehicle yaw rate of the vehicle in this paper can be expressed as Equation (15):

$$\dot{\omega}_{r} = a_{11}\omega_{r} + a_{12}\beta + b_{11}u(t)$$

$$b_{11} = \frac{aC_{f}}{I_{z}}$$

$$a_{11} = \frac{a^{2}C_{f} + b^{2}C_{r}}{I_{z}v_{r}}$$

$$a_{21} = \frac{aC_{f} - bC_{r}}{Mv_{z}^{2}} - 1$$
(15)

The vehicle yaw rate is chosen as the controlled variable. The tracking error between the yaw rate and the ideal yaw rate can be shown in Equation (16):

$$e = \omega_r - \omega_d \tag{16}$$

The controller switching function is designed as Equation (17):

$$s = e + \gamma \int_{0}^{t} e(\tau) d\tau$$
(17)

where γ is the sliding surface gain.

The sliding mode control law is designed based on Equations (15)–(17), which is shown in Equations (18) and (19):

$$u = \frac{1}{b_{11}} \left[-f(\omega_r) + \gamma(\omega_r - \omega_d) + K(t) sgn(s) \right]$$
(18)

$$K(t) = -ksgn(s) \quad k > 0 \tag{19}$$

Control of front wheel angle can be expressed as Equation (20):

$$\delta = \frac{I_z}{aC_f} \left[\frac{aC_f - bC_r}{I_z} \beta + \frac{a^2 C_f + b^2 C_r}{I_z V_r} \omega_r - \omega_d + \gamma(\dot{\omega_r} - \omega_d) \right]$$
(20)

The steering wheel angle can be obtained as Equation (21):

$$\theta_s = \delta * i_{SW} \tag{21}$$

 i_{sw} is the steering system ratio.

3. Multi-Agent Coordinated Control System Based on Blackboard Mode

Longitudinal and lateral collision avoidance agents are taken into consideration to ensure the multi-agent coordinated control system deals with the traffic accident risk. Additionally, global path planning agents, path tracking agents, and actuator control agents are taken as fundamental agents in the system.

Each agent of a multi-agent coordinated control system can be carried out in its default mode. Thus, the conflict problem in the driving process is generally classified into three categories according to the cause: resource conflicts, target conflicts, and result conflicts [22].

As can be seen from Figure 3, conflicts between longitudinal and lateral collision avoidance agents are easily issued. When front obstacles are detected by vehicle sensors, safe distance will be calculated by the longitudinal collision avoidance agent and braking force will be transmitted to the active braking agent. Correspondingly, steering control signals will be transmitted to the active steering agent by the lateral collision avoidance agent. Different solutions for front-distance avoidance may lead to the result of conflicts in multi-agent systems.



Figure 3. Topology of multi-agent coordinated control system.

The blackboard model is used to solve result conflicts in this section [23], in which each agent exchanges data and writes its solution on the blackboard. The model is composed

of three basic components: blackboard, knowledge source, and control mechanism. The internal coordination module manages the data on the blackboard in a unified manner. When there is a collision avoidance decision conflict between the agents, the coordination module can choose a reasonable collision avoidance method according to the internal rule base. A multi-agent coordinated control system based on a blackboard model is shown in Figure 4. As shown in Figure 4, the multi-agent active collision avoidance decisionmaking system based on the blackboard model is divided into three layers: a planning layer, decision and coordination layer, and execution control layer. Longitudinal and lateral collision avoidance agents constitute the planning layer of the system, which also includes the basic global path planning agent, path tracking agent, and actuator control agents. They can be regarded as different knowledge sources, and each agent can interact with the blackboard model to obtain information and complete a relatively independent and complete problem-solving. In the decision and coordination layer, the blackboard module is used to store the environmental information obtained by the environment perception system of the intelligent vehicle and the solution results of each agent, and the internal coordination module is used to manage the data on the blackboard in a unified way. When encountering collision avoidance decision conflicts between agents, the coordination module needs to choose a reasonable collision avoidance method according to the internal rule base. The executive control layer includes the active braking control agent and the active steering agent, which interacts with the blackboard model and finally, executes the decision of the multi-agent collision avoidance control system.



Figure 4. Multi-agent coordinated control system based on blackboard model.

During the driving process, the information acquired by the environment perception layer is uploaded to the blackboard in real time, and each agent obtains information by interacting with the blackboard. When an obstacle appears on the default path, longitudinal and lateral collision avoidance agents are activated. The brake pressure and steering wheel angle are uploaded to the blackboard separately. If the two agents are activated at the same time, a choice must be made by the coordinated control module according to the actual situation.

Figure 5 shows the choice of active collision avoidance during an emergency in different environments.



Figure 5. The choice of active collision avoidance during an emergency in different environments: (a) Dry asphalt pavement ($\mu = 0.8$); (b) Wet asphalt pavement ($\mu = 0.5$).

Longitudinal lateral collision avoidance agents are plotted in Figure 5a,b. The minimum safety distance required for emergency longitudinal collision avoidance is related to the square of the vehicle speed, and the minimum longitudinal safety distance required for emergency lateral collision avoidance is related to the square of the vehicle speed. When the vehicle speed is in the lower range, the collision avoidance distance required for longitudinal collision avoidance is small. With the increase in speed, the collision avoidance distance required for longitudinal collision avoidance increases rapidly, and the longitudinal collision avoidance distance required for lateral collision avoidance begins to be smaller than that for longitudinal collision avoidance. It can be seen that D_b in area (1) is greater than the longitudinal and lateral collision limit distance. In this case, the vehicle faces no risk and the auxiliary braking mode is adopted. At this time, more attention should be paid to the traffic efficiency and occupant comfort of the vehicle. The absolute value of the vehicle deceleration is limited to 4 m/s² or less.

When located in areas (2) and (4), the maximum braking deceleration should be adopted in this emergency condition to reduce the risk of traffic accidents.

When D_b is located in area ③, the speed of the vehicle is higher and the longitudinal distance required for collision avoidance is large. So, a lane-changing strategy will be taken to avoid a collision.

According to the analysis above, the decision and judgment process of the coordinated module is shown as follows, which is designed to make sure the vehicle drives along the planned path. When an obstacle ahead is detected by an intelligent vehicle, the distance between the intelligent vehicle and the obstacle must be compared with the safe distance of the limit collision distance of the longitudinal collision avoidance agent and the lateral collision avoidance agent, firstly. If the distance D_b is longer than the braking limit distance, then it is according to the braking acceleration to judge whether to use auxiliary braking mode or emergency braking mode. However, if the distance is shorter than the braking distance and longer than the steering limit distance, which will use the steering collision avoidance mode.

The active collision avoidance control strategy in this paper is shown in Figure 6a and the collision avoidance control strategy is shown in Figure 6b. T_1 is the planning time of longitudinal collision avoidance, T_2 is the decision time of collision avoidance way, T_3 is the planning time of lateral collision avoidance, T_4 is the execution control time.



Figure 6. Active collision avoidance system control method: (**a**) Distributed coordinated control system; (**b**) Sequential control system.

As shown in Figure 6a, time consumption $T_{D-Braking}$ and $T_{S-Braking}$ used during the entire collision avoidance can be calculated as Equations (22) and (23):

$$T_{D-Braking} = max\{T_1, T_2\} + T_4 \text{ or } T_{D-Steering} = max\{T_2, T_3\} + T_4$$
(22)

$$T_{S-Braking} = T_2 + T_1 + T_4 \text{ or } T_{S-Steering} = T_2 + T_3 + T_4$$
 (23)

As can be seen from Equations (22) and (23), the separation of the collision avoidance decision and the collision avoidance planning will take more time.

The distributed multi-agent coordinated system based on the blackboard model performs parallel operations. The lateral and longitudinal collision avoidance agents, respectively, solve the steering wheel angle and brake pressure required for collision avoidance. At the same time, the blackboard coordinated module selects the optimal collision avoidance way according to the environmental information and can directly output the control instruction to agents of the execution control layer. By rationally unifying the decision and planning, the running time lag of the active collision avoidance system is reduced, and the real-time behavior of the vehicle collision avoidance is effectively improved.

4. Simulation Analysis

To verify the real-time performance of the distributed coordinated multi-agent system of the active collision avoidance proposed, the longitudinal collision avoidance agent, the lateral collision avoidance agent, and the blackboard model were built in CarSim and Simulink.

Some of the important vehicle parameters are given in Table 1. Most of them are directly measured from a B-class vehicle.

Co-simulation results are compared with the Sequential control system collision avoidance and the co-simulation model is shown in Figure 7.

Two different conditions are adopted to characterize the effectiveness of a multi-agent coordinated control system and superiority in improving the real-time performance of active collision avoidance. The vehicle that used the distributed coordinated multi-agent control system of active collision avoidance based on the blackboard proposed in this paper is recorded as vehicle A and the vehicle that used the sequential control system of active collision avoidance is recorded as vehicle B.

| Parameter | Value | Unit |
|---|--------|-------------------|
| Mass (m) | 1274 | kg |
| Distance from c.g.to front axle (a) | 1.8 | m |
| Distance from c.g.to rear axle (b) | 1.31 | m |
| Atmospheric density (ρ) | 1.206 | kg/m ³ |
| Frontal area (A_a) | 1.6 | m ² |
| The rolling radius of wheels (r_r) | 0.31 | m |
| Intelligent vehicle width (W_s) | 1.695 | m |
| Stiffness of the front tire (C_f) | 976.24 | N/rad |
| Stiffness of the rear tire (C_r) | 980.18 | N/rad |
| Coefficient of air resistance (C_D) | 0.3 | 1 |
| Inertia around the vertical shaft (I_z) | 1523 | kg∙m ² |

Table 1. Basic parameters of the vehicle.



Figure 7. Distributed multi-agent collision avoidance system simulation.

4.1. Simulation of the Longitudinal Collision Avoidance Agent

The vehicle speed is set as 36 km/h, and suddenly, there is an obstacle that falls 10 m in front of the vehicle. The green dotted line in the figure is the moment when the obstacle appears. At this time, D_b is located in the area ④. Simulation results are shown in Figure 8.

Results show that after detecting the obstacle, the vehicle selects braking to avoid a collision. As can be seen from Figure 8c, the brake pressure output time of vehicle A is 0.13 s ahead of vehicle B. What is more, from Figure 8a,b, we can see that vehicle A is 3.12 m away from the obstacle at 3.1 s when it stops, and vehicle B is 1.4 m away from the obstacle at 3.18 s when it stops. In the face of sudden emergency conditions, the coordinated control system adopted by vehicle A can make decisions and simultaneously conduct collision avoidance planning to realize the integration of collision avoidance decision-making and planning, so that vehicle A will provide safer control. So, the data from the simulation experiments show that a multi-agent coordinated control system improves the real-time performance of active collision avoidance, which has a shorter braking distance than the sequential control system.



Figure 8. Simulation of longitudinal collision avoidance: (**a**) Vehicle speed; (**b**) Distance between vehicle and obstacle; (**c**) Brake pressure of the vehicles.

4.2. Simulation of the Lateral Collision Avoidance Agent

This simulation will be used to verify the performance of the multi-agent coordinated control system at higher vehicle speeds. The vehicle runs at a constant speed along the road at 80 km/h, and suddenly, there is an obstacle falling 30 m from the front as shown in Figure 9a. The green dotted line in Figure 9a,b is the location and moment when the obstacle appears. The relative distance between the lateral width of the obstacle and the vehicle center of mass is 2 m. At this time, D_b is in the area (3). Simulation results are shown in Figure 9.

Results show that when the obstacle appears, the vehicle selects steering to avoid collision in this situation. The steering wheel angle output time of vehicle A is 0.14 s ahead of vehicle B as shown in Figure 9b. The critical collision time is calculated to be 1.09 s, the longitudinal displacement of vehicle A is 28.43 m, and the longitudinal displacement of vehicle B is 31.54 m. At this time, vehicle B collided with the obstacle, and vehicle A still has a certain distance from the obstacle. Figure 9a shows a close-up view of the collision with vehicle B. The timeliness and effectiveness of vehicle A's lane-changing collision avoidance control have been verified, but its trajectory tracking performance has room for improvement. Therefore, as shown in Figure 9c,d, the fuzzy sliding control is adopted to ensure the good tracking performance of the vehicle on the lane-changing trajectory and the lateral acceleration curve of the vehicle is also more gradual, which meets the stability requirements of the vehicle. The fuzzy sliding control mainly acts on the turn-back stage of the vehicle's emergency steering. As can be seen from Figure 9, the lateral acceleration



of the vehicle decreases significantly after the vehicle quickly escapes from the danger of collision, which can ensure the stability of the vehicle and the comfort of the occupants.

Figure 9. Simulation of lateral collision avoidance: (**a**) Lane-changing track; (**b**) Steering wheel angle; (**c**) Lane-changing track; (**d**) Lateral acceleration.

5. Conclusions

A multi-agent coordinated control system based on a blackboard model is proposed for improving the real-time performance of an active collision avoidance system in this paper. To do this, some agents, including a longitudinal collision avoidance agent and lateral collision avoidance agent, are established, and all of them can support and cooperate under the unified goal to produce reasonable control rules in coordination with the blackboard model, which can select a reasonable collision avoidance method under different driving conditions. In the process of active collision avoidance, the decision and planning are simultaneously operated. At the same time as the decision and planning are completed, underlying control instructions can be executed immediately, and the decision and planning integration of the collision avoidance system is realized, which effectively reduces the time lag during the process of active collision avoidance. The simulation results also indicate that the proposed multi-agent active collision avoidance system can reduce the decision and planning time, improving the real-time behavior of the intelligent vehicle.

The next step will further consider the state of the preceding vehicle. In terms of emergency steering and collision avoidance, the next step will be to consider vehicles in adjacent lanes to ensure that vehicles in adjacent lanes are not affected during the process of changing lanes to avoid collisions. At the same time, a real vehicle test is arranged. **Author Contributions:** Conceptualization, C.Y.; methodology, J.S.; software, S.W. and Q.Y.; validation, Y.H., Y.C. and L.C.; formal analysis, C.Y.; investigation, S.W.; resources, Y.G.; data curation, Y.Y.; writing—original draft preparation, Y.L. and X.W.; writing—review and editing, S.W.; supervision, S.W.; project administration, L.C.; funding acquisition, C.Y. All authors have read and agreed to the published version of the manuscript.

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Nomenclature

Symbol

| $t_{detect1}$ (s) | the environment perception time |
|---------------------------|--|
| $t_{decision1}$ (s) | the decision-planning time of longitudinal collision avoidance agent |
| $t_{excution1}$ (s) | the mechanical delay time |
| V_r (km/h) | the vehicle speed |
| $a_{r-max} (m/s^2)$ | the maximum braking deceleration of the vehicle |
| <i>d</i> ₀ (m) | the minimum safety threshold |
| μ | the coefficient of road adhesion |
| $g (m/s^2)$ | the acceleration of gravity |
| α (rad) | the vehicle slope angle. |
| F_w (N) | the air resistance force |
| T_s (N·m) | the driving torque |
| T_{bf} (N·m) | the braking torque of the front wheels |
| T_{br} (N·m) | the braking torque of the rear wheels |
| F_f (N) | the ground friction of the ground acting on the front wheels |
| $\vec{F_r}$ (N) | the ground friction of the ground acting on the rear wheels |
| W_f (N) | the vertical force of the front wheels |
| W_r (N) | the vertical force of the rear wheels |
| F_t (N) | the driving force |
| F_{Xb} (N) | the braking force |
| $\sum F(V_r)$ (N) | the total resistance. |
| \overline{P}_{des} (Pa) | the desired braking pressure |
| K _b | the braking pressure ratio |
| r_r (m) | the rolling radius of wheels |
| P_b (Pa) | the pressure of the brake pipe |
| y_e (m) | the lateral displacement for the vehicle to avoid collision |
| t_e (s) | the lane-changing time |
| $W_{s}(m)$ | the vehicle width |
| $t_{c}(s)$ | the collision time |
| $W_{b}(m)$ | the lateral distance |
| S_a (m) | the longitudinal displacement |
| $t_{detect2}$ (s) | the perception delay |
| $t_{decision2}$ (s) | The decision-planning time |
| $t_{excution2}$ (s) | the steering mechanical delay |
| β (rad) | sideslip angle |
| v_{y} (km/h) | the lateral speed |
| M (kg) | the vehicle mass |
| ω (rad/s) | the yaw rate |
| a and b (m) | the front and rear wheel base |

| I _z (kg·m²) | the vehicle's moment of inertia |
|-----------------------------|---|
| C_f and C_r (N/rad) | the stiffness of the front and rear tire |
| γ | the sliding surface gain |
| i _{SW} | the steering system ratio |
| θ_s (rad) | the steering wheel angle |
| T_{1} (s) | the planning time of longitudinal collision avoidance |
| T_{2} (s) | the decision time of collision avoidance way |
| <i>T</i> ₃ (s) | the planning time of lateral collision avoidance |
| T_4 (s) | the execution control time |
| T _{D-Breaking} (s) | time consumption using distributed coordinated control system |
| $T_{S-Breaking}$ (s) | time consumption using a sequential control system |
| ~ | |

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