## Greenhouse gas emission details and cost analysis of existing and alternative waste management systems (WMSs) in Kabul city

## Section 1. Collection and transportation

## (1) Greenhouse gas emissions

Greenhouse gas emissions from waste collection and transport (ton- $\mathrm{CO}_{2} /$ year) are calculated as

$$
\begin{equation*}
\text { Total GHG emissions }=\text { TFC } \times \mathrm{Q} \times \mathrm{GWP} \tag{1}
\end{equation*}
$$

where TFC represents the total fuel consumption (L/day) used for collection of mixed waste and recyclables, Q is the emission factor from diesel, and GWP is the equivalence factor based on carbon dioxide as 1 . To calculate TFC, we used

$$
\begin{equation*}
\mathrm{TFC}=\mathrm{TFC}_{\mathrm{M} \_} \mathrm{w}+\mathrm{TFC}_{R}, \tag{2}
\end{equation*}
$$

where $\mathrm{TFC}_{\mathrm{M}_{\mathbf{\prime}} \mathrm{w}}$ represents the amount of fuel consumption (L/day) used for collection of mixed waste; $T F C_{R}$ (L/day) represents the collection of recyclables. To calculate $\mathrm{TFC}_{\mathrm{M}_{-}} w$ and $\mathrm{TFC}_{R}$, the following equation was used.

$$
\begin{equation*}
\mathrm{TFC}_{M_{-} \mathrm{W}}=\mathrm{X}_{\mathrm{M}_{-} \mathrm{W}} \times \mathrm{FC}_{\mathrm{M}_{-} \mathrm{W}} \tag{3}
\end{equation*}
$$

Therein, $X_{M_{-}}$denotes the amount of mixed waste (ton/day) collected, and $\mathrm{FC}_{\mathrm{M}_{2}}$ stands for the unit value of fuel consumption with a loading factor of $100 \%$ (L/ton).

$$
\begin{equation*}
T F C_{R}=N_{i} \times D \times F C \tag{4}
\end{equation*}
$$

In the equation above, N stands for the number of trucks, irepresents the pattern of collection, D denotes the average travel distance of round trip (km), and FC expresses the unit value of fuel consumption with a loading factor of $100 \%(L / k m)$.

Note: To obtain the number of trucks for collection of recyclables in S-0, equation (5) was used. For S-3 and $\mathrm{S}-4$, equation (6) was applied.

$$
\begin{align*}
& N_{\text {RS-MRF }}=\operatorname{Roundup}\left(X_{R} / C / f\right)  \tag{5}\\
& N_{\text {D.C-MRF }}=\left(X_{R} / Y / f\right) \tag{6}
\end{align*}
$$

Therein, $X_{R}$ signifies the amount of recyclables (ton/day), $C$ denotes the capacity of truck (ton), $f$ stands for the frequency (1/day), RS-MRF expresses the number of trucks used for collection from recycling shops to MRF, $Y$ represents the amount of recyclables (ton/day) generated in different districts, and d.C-MRF denotes the collection of reyclabes from district centers to MRF. Following are the descriptions of the respective scenarios with their fuel consumption.

S-0: In the baseline scenario, the amount of mixed waste collected from collection points and transported to the landfill site is 1,314 ton/day, with an average fuel consumption of $8,048 \mathrm{~L}$ /day, meaning that the fuel consumption per ton of mixed waste in collection is $6.12 \mathrm{~L} /$ ton. Consequently, to calculate the amount of fuel consumption on mixed waste collection, equation (3) was considered.

Because waste collection of recyclables differs from mixed materials, from recycling shops to recycling facilities and then their residues to landfill site, equations (4) and (5) have been considered for calculation of the fuel consumption. Detailed calculations of equations (4) and (5) are presented with results in Tables S1 and S2 including the designed models, assumptions, and the values of variables.

Table A1. Diesel consumption for collection of recyclables in S-0
$\left.\begin{array}{|l|c|}\hline \text { Amount of waste (ton /day), } \mathrm{X}_{\mathrm{R}} & 22.7 \\ \hline \text { Capacity of truck (ton), C } & 12 \\ \hline \text { Frequency (1/day), f } & 1 \\ \hline \text { Number of trucks (number), } \mathrm{N}_{\mathrm{RS} \text {-MRF }} & 2 \\ \hline \begin{array}{l}\text { * Average travel distance of } \\ \text { round trip (km), D }\end{array} & 72 \\ \hline \text { * Fuel consumption of truck (L/km), FC } & 0.5 \\ \hline \text { Total fuel consumption (L/day), TFC } & \text { RS-MRF }\end{array}\right] 72$.
(2020) * DOS of Kabul city (2020)

S-1 and S-2: Total fuel consumption was estimated based on equation (3). $X_{M \_w}$ was found by calculation by multiplying the total population of Kabul, 4.67 million. The waste generation per capita per day was 0.54 kg .

S-3 and S-4: In this scenario, to calculate the amount of fuel consumption on mixed waste collection, equation (3) was considered, while regarding recyclables, for which the collection starts from the center of city districts to MRF / landfill site, equation (4) and (6) have been incorporated. Detailed calculations of equations (4) and (6) are presented with the results in Table A3 including the designed models, assumptions, and the variable values. In addition, the average travel distance $\mathrm{D}(\mathrm{km})$ has been modelled and calculated using GIS Network Analysis technique. Figure 2 depicts routing maps of waste collection on a source-separated system. Table A4 presents routing map details.

Table S3. Calculated fuel diesel consumption for collection and transport of source-separated waste recyclables from the center of city districts to recycling facilities in S-3

| Amount of waste (ton/day), $\mathrm{X}_{\mathrm{R}}$ | 227 |
| :--- | :---: |
| Loaded waste onto truck (ton/day) based on routes <br> (ton), Y | - |
| Frequency (1/day), f | 1 |
| Number of trucks (number), $\mathrm{N}_{\mathrm{R}-\mathrm{S} 3,54}$ | 20 |


| Average travel distance of round trip (km), D | 79 |
| :--- | :---: |
| Fuel consumption of truck (L/km), FC | 0.5 |
| Total fuel consumption (L/day), TFC.. .C-MRF | 774.2 |

Note: One truck has a 4-ton capacity. Its fuel consumption per km is $0.3 \mathrm{~L} / \mathrm{km}$ according to DoS. Other trucks have a 12 -ton capacity.


Figure S1. Locations of current recycling facilities and landfill sites in Kabul city.


Figure S2. Routing map of collection and transport on source-separated waste from collection points/ center of a district to landfill site.

Table S4. Network analysis showing route distances generated from collection points / center of city districts of source-separated waste to landfill site

| S.no. | Start <br> point | Intermediat- <br> e point | End point | Route | Round <br> trip <br> $(k m)$ | ** Fuel <br> consumptio <br> n(L/km ) | Fuel <br> consumpti- <br> on (L) | Waste <br> amount <br> collected <br> (ton/day) |
| :---: | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 1 | ^Dis 3 | Dis 1 | Dumpsite | R1 | 99 | 0.5 | 49 | 11 |
| 2 | Dis 4 | - | Dumpsite | R2 | 70 | 0.5 | 35 | 12 |
| 3 | Dis 4 | - | Dumpsite | R2 | 70 | 0.5 | 35 | 12 |
| 4 | Dis 5 | - | Dumpsite | R3 | 80 | 0.5 | 40 | 12 |
| 5 | Dis 5 | Dis 4 | Dumpsite | R4 | 93 | 0.5 | 47 | 12 |
| 6 | Dis 7 | - | Dumpsite | R5 | 70 | 0.5 | 35 | 12 |
| 7 | Dis 9 | - | Dumpsite | R6 | 51 | 0.5 | 25 | 12 |
| 8 | Dis 10 | Dis 9 | Dumpsite | R7 | 69 | 0.5 | 34 | 10 |
| 9 | Dis 11 | - | Dumpsite | R8 | 77 | 0.5 | 38 | 12 |
| 10 | Dis 13 | - | Dumpsite | R9 | 90 | 0.5 | 45 | 12 |
| 11 | Dis 14 | Dis 11 | Dumpsite | R10 | 122 | 0.5 | 61 | 12 |
| 12 | Dis 15 | - | Dumpsite | R11 | 65 | 0.5 | 32 | 11 |
| 13 | Dis 15 | - | Dumpsite | R11 | 65 | 0.5 | 32 | 11 |
| 14 | Dis 7 | Dis 16 | Dumpsite | R12 | 79 | 0.5 | 39 | 12 |
| 15 | Dis 17 | Dis 2 | Dumpsite | R13 | 101 | 0.5 | 51 | 12 |
| 16 | Dis 18 | Dis 19 | Dumpsite | R14 | 69 | 0.3 | 34 | 4 |
| 17 | Dis 20 | Dis 6 | Dumpsite | R15 | 101 | 0.5 | 51 | 12 |
| 18 | Dis 20 | Dis 12 | Dumpsite | R16 | 89 | 0.5 | 45 | 12 |
| 19 | Dis 8 | Dis 22 | Dumpsite | R17 | 59 | 0.5 | 30 | 12 |
| 20 | Dis 10 | - | Dumpsite | R18 | 70 | 0.5 | 35 | 12 |
|  | Total |  |  |  | 1,588 |  | 793.8 | 227 |
|  | Average |  |  |  |  | 79 |  |  |

$\wedge$ Dis stands for district.

The following tables show total fuel consumption of waste collection for each scenario and the amounts of GHG emissions during this process on each scenario.

Table S5. Estimation of total fuel consumption for waste collection in existing and alternative scenarios

| Scenarios | Fuel consumption for <br> recyclables collection <br> (L/day) | Fuel consumption for mixed <br> waste collection(L/day) | Total (L/day) |
| :--- | :---: | :---: | :---: |
| Baseline scenarios | 83.4 | 8,048 | $8,131.4$ |
| Scenario 1 | - | 15,477 | 15,477 |
| Scenario 2 | - | 15,477 | 15,477 |
| Scenario 3 | 774.2 | $14,073.37$ | $14,847.57$ |
| Scenario 4 | 774.2 | $14,073.37$ | $14,847.57$ |

Table A6. Estimation the GHG emissions of waste collection for existing and alternative scenarios

| Scenarios | Impact category <br> $\left(\mathrm{CO}_{2}\right)$ | Unit | Total |
| :--- | :--- | :--- | :---: |
| Baseline scenario | Global Warming | ton $\mathrm{CO}_{2} /$ year | $7,899.89$ |
| Scenario 1 |  |  | $15,036.35$ |
| Scenario 2 |  |  | $15,036.35$ |
| Scenario 3 |  |  | $14,424.84$ |
| Scenario 4 |  |  | $14,424.84$ |

Note: Gaseous emissions from diesel fuel ( $2663 \mathrm{~g} / \mathrm{L}$ ) of $\mathrm{CO}_{2}$ were obtained from Kebin et al. (2010) and Babu et al. (2014). Characterization factors are based on IPCC model 2007 for a 100-year time horizon.

## (2) Cost analysis of collection

To calculate costs increased by the increased level of waste collection services to $100 \%$, we use

$$
\begin{equation*}
\text { TCoAWC }=A+B+C+D+E, \tag{7}
\end{equation*}
$$

where TCoAWC shows the total costs of alternative waste collection (S/year), A denotes the cost of collection trucks (\$/year), B stands for the cost of collection trucks maintenance (\$/year), C signifies the cost of diesel fuel for collection trucks (\$/year), D represents the salary cost (\$/year), and E expresses the cost for working tools, clothing, and training (\$/year). The respective calculations of these variables are presented hereinafter.
A. Cost of collection truck

The cost of collection trucks has been calculated using the following equation.

$$
\begin{equation*}
A=A 1+A 2 \tag{8}
\end{equation*}
$$

Therein, A1 represents the cost of collection trucks (\$/year) that collect mixed waste, wherease A2 (\$/year) is that for recyclables. To calculate A1 and A2, the equations are used.

$$
\begin{equation*}
A 1=\operatorname{Roundup}\left(X_{M \_w} /(C \times f)\right) \times(B / L) \tag{9}
\end{equation*}
$$

Therein, $X_{M \_w}$ represents the amount of uncollected mixed waste (ton/day), C denotes the truck capacity (ton), f is the frequency (trip) of truck (1/day), B stands for the cost per unit of truck ( $\$ /$ truck), and $L$ signifies the life time of vehicle trucks (year). Also,

$$
\begin{equation*}
A 2=N_{R-S 3, S 4} \times B / L \tag{10}
\end{equation*}
$$

where $\mathrm{N}_{\mathrm{R}-\mathrm{S3}, \mathrm{~s} 4}$ represents the number of trucks (number) as calculated using equation (6).
S-1 and S-2: In these scenarios, because all the waste has been assumed to be collected in mixed waste, there is only cost related to A1. Table A7 shows descriptions of the designed model, assumptions, and the variable values including the result in this regard.

Table S7. Cost calculations of added trucks for mixed waste collection in S-1 and S-2

| Items | Amount |
| :--- | :---: |
| Amount of waste (ton/day), $\mathrm{X}_{\mathrm{M} \_\mathrm{w}}$ | 1200.33 |
| Capacity of truck (ton/truck), C | 12 |
| Frequency ( 1/day ), f | 1 |
| * Cost per unit of truck (\$/truck), B | 25,000 |
| Lifetime of truck (year), L | 15 |
| Total (\$/year) | 168,333 |

* DoS of Kabul city (2020)

S-3 and S-4: In these scenarios, cost calculations of added trucks have been considered based on the total cost calculations of A1 and A2. Tables A8 and A9 show descriptions of the designed model, assumptions and the variable values including the results.

Table S8. Cost calculation of added trucks for mixed waste collection in S-3

| Items | Amount |
| :--- | :---: |
| Amount of waste (ton/day), $\mathrm{X}_{\mathrm{M} \_} \mathrm{w}$ | 973 |
| Capacity of truck (ton), C | 12 |
| Frequency (1/day ), f | 1 |
| Cost per unit of truck (\$), B | 25,000 |
| Lifetime of truck (year), L | 15 |
| Total (\$/year) | $136,666.7$ |

Table S9. Cost calculation of added trucks for recyclables collection in S-3

| Items | Amount |
| :--- | :---: |
| Number of trucks (ton), $\mathrm{N}_{\mathrm{R}-53,54}$ | 20 |
| Frequency ( 1/day ), f | 1 |
| Cost per unit of truck (\$), B | 25,000 |
| Lifetime of truck (year), L | 15 |
| Total (\$/year) | 33,333 |

B. Cost of collection trucks maintenance

Following is the formula for calculating the cost of collection truck maintenance (\$/year) in the scenarios.

$$
\begin{equation*}
\mathrm{B}=\mathrm{N} \times \mathrm{MC} \tag{11}
\end{equation*}
$$

In that equation, $N$ is number of trucks (number) and $M C$ ( $\$ /$ year) is the maintenance cost of trucks. Calculation of the number of trucks for the collection of mixed waste is based on Roundup ( $\mathrm{X}_{\mathrm{M} \_} \mathrm{w}$ / ( $\mathrm{C} \times$ f)). Their explanations including the values are presented in Tables A7 and A8. For recyclables the value of N is shown in Table A9.

## C. Cost of fuel for collection trucks

Following is the formula for the cost of fuel for collection trucks (C) (\$/year) of the scenarios.

$$
\begin{equation*}
C=T F C \times D P \tag{12}
\end{equation*}
$$

As shown there, TFC is the total fuel consumption (L/year), which is shown in Table A5 (L/day). Also, DP represents the diesel price, which is $0.49 \$ / L$, as obtained from a survey interview (2020).
D. Salary cost

Following is the formula to calculate the salary cost.

$$
\begin{equation*}
D=D 1+D 2 \tag{13}
\end{equation*}
$$

Therein, D1 stands for the salary cost for mixed waste collection ( $\$ /$ year), and D2 denotes that for recyclables (\$/year). To calculate D1 and D2, the following equations are used.

$$
\begin{equation*}
\text { D1 }=X \times N W \times S \tag{14}
\end{equation*}
$$

In that equation, X represents the amount of mixed waste (ton/day), and NW denotes the number of workers per ton of mixed waste (workers/ton/day). Also, S is the salary per worker ( $\$ /$ worker/year).

$$
\begin{equation*}
\mathrm{D} 2=\left(\mathrm{NW}_{\mathrm{S}-\mathrm{H}}+\mathrm{NW}_{\mathrm{Dis}_{-} \mathrm{MRF}}+\mathrm{OW}\right) \times \mathrm{S} \tag{15}
\end{equation*}
$$

As shown there, $\mathrm{NW}_{s-H}$ denotes the number of workers for collection of recyclables at the level of households, NW ${ }_{\text {Dis_MRF }}$ is the number of workers for collection of recyclables from districts to MRF, and OW is the number of office workers.

The total number of workers to be formalized in $\mathrm{NW}_{s-\mathrm{H}}$ has been formulated as

$$
\begin{equation*}
N W_{s-H}=T N H /(W D \times N F W \times F), \tag{16}
\end{equation*}
$$

where TNH denotes the total number that households in Kabul city are visited for their waste recyclables (number/year), WD represents the number of working days (days/year), NFW is the number of households covered per formalized worker (number of households /worker/day), and F stands for the frequency of collection (1/week). To obtain NFW, we started to find the number of households to have their recyclables collected per formalized worker. To do so, the following formula is used.
NFW = (WH-1) / T

Therein, WH represents the working hours ( $h /$ day), and $T(h)$ is the time spent to collect the recyclables per household, Which includes receiving waste from the household and walking to the next household. Also, (-1) represents the one hour break.

For the calcuation of $\mathrm{NW}_{\mathrm{Dis}}$

$$
\begin{equation*}
\mathrm{NW}_{\text {Dis_Mrf }}=\sum \mathrm{NT} \times \mathrm{NW}_{\text {R_T }^{\prime}}, \tag{18}
\end{equation*}
$$

where NT stands for the number of trucks, and NW R_T $^{\text {d }}$ denotes the number of workers allocated to each truck. To ascertain the number of office workers (OW) integrated in this process, on average, four office workers might be necessary to manage the clerical and administrative tasks of 150 waste collection workers.

$$
\begin{equation*}
\mathrm{OW}=\left(\mathrm{NW}_{\text {S-H }}+\mathrm{NW}_{\text {Dis_ }} \mathrm{MRF}\right) / \mathrm{OW} \text { sub } \tag{19}
\end{equation*}
$$

In the baseline scenario, there are 2,415 workers - with a salary of $\$ 141$ per month, able to collect 1,314 ton of waste per day as mixed materials. In fact, for the collection of 1 ton of waste, 1.84 workers have been assigned. This number of workers has been examined from calculation of the salary cost related to mixed waste collection for alternative scenarios. However, this number ( 1.84 workers /ton) cannot be used to calculate the salary cost in source-separated system because there is house-to-house collection, with wastes then taken to the center of each district before being sent to MRF: something which differs from the process used for mixed waste collection.

Below are the cost calculations of labor for the respective scenarios.
S-1 and S-2: The following table shows descriptions of the designed model, assumptions, variable values, and results.

Table S10. Salary costs for integrating informal workers in mixed waste collection in S-1 and S-2

| Amount of waste (ton/day), X | 1200.33 |
| :--- | :---: |
| $*$ Number of workers per ton of mixed waste collected (worker/ ton/day), NW | 1.84 |
| Salary (\$/worker/year), S | $1,230.77$ |
| Total (\$/year) | $2,715,621$ |

* Salary is inferred as 102.56 \$ /month for integrated workers.

S-3 and S-4: Following are the descriptions of the designed model, assumptions, variable values, and results.

Table S11. Salary cost for the integration of informal workers in mixed waste collection in S3 and S4

| Amount of waste (ton/day), X | 973 |
| :--- | :---: |
| Number of workers per ton of mixed waste collected (worker/ ton/day), <br> NW | 1.84 |
| Salary (\$/worker/year), S | $1,230.77$ |
| Total (\$/year) | $2,203,472$ |

Table S12. Total number of households covered by a formalized workers for collection of source-separated waste

| Working hours (h), WH | 8 |
| :--- | :---: |
| Time spent for collection (h/household), T | 0.05 |


| Household number (number of households /worker/day), NFW | 140 |
| :--- | :--- |

Note: One-hour break was considered for serving and prayers.

Table S13 Total number informal workers to be integrated in collection of sources separated waste from house to house

| Parameter | amount | unit |
| :--- | :---: | :---: |
| Kabul city oopulation | $4,679,648$ | number |
| Household number | 7 | number /family |
| Number households in Kabul city | 668,521 | number |
| TNH = total number of households of Kabul city are visited | $244,010,217$ | number/year |
| Amount of waste recyclable generation | 455 | ton /day |
| Efficiency of source separation | 0.5 | 1 |
| F frequency of recyclables collection | 0.680 | visit/week |
| Production of recyclables per family | 140 | No. of households / <br> formalized worker/day |
| NFW = number of households covered per formalized <br> worker in collection of source-separated waste per day | 261 | day/year |
| WD = number of working days in a year | 954 | number |
| NW s-H = number of formalized workers for collection of <br> sources separated waste |  |  |

Table S14. Number of informal workers to be integrated in collection and transport of recyclabes from district centers to MRF/ landfill site

| Total number of workers for 12 ton type <br> truck |  | Total number of workers for 4 ton type <br> truck |  | Grand total <br> (number) |
| :---: | :---: | :---: | :---: | :---: |
| number of trucks, N | 19 | number of trucks, N | 1 |  |
| number of workers on <br> a truck, $\mathrm{NW}_{\mathrm{R}_{-} \mathrm{T}}$ | 6 | number of workers on <br> a truck, $\mathrm{NW}_{\mathrm{R}_{-} \mathrm{T}}$ | 1 |  |
| subtotal | 114 | subtotal | 4 | 118 |

* According to DoS and the World Bank report of 2016, 6 workers on large size trucks and 4 on a small one were assigned to load the waste to trucks. Based on that, we assumed 6 workers for a large truck ( 12 ton), and 4 for small size truck ( 4 ton).

Table S15. Total number of informal workers integrated as office workers in source-separated waste collection and transport

| Number of staff on collection of sources separated waste from house to <br> house, NW $_{\text {S-H }}$ | 954 |
| :--- | :---: |
| Number of workers for collection and transport from waste collection <br> points to MRF/landfill, NW <br> Dis_MRF | 118 |
| Number office workers for 150 waste collection workers, OWsub | 4 |
| Office workers, OW (number) | 29 |

## E. Costs for working tools, clothing, and training

Following is the formula used to calculate these costs in these scenarios.

$$
\begin{equation*}
\mathrm{E}=\mathrm{NW} \times \mathrm{C}_{\mathrm{TCT}} \tag{20}
\end{equation*}
$$

In that equation, NW stands for the number of workers to be integrated in the scenario as found from the salary cost, and $C_{\text {TCT }}$ denotes the cost for working tools, clothing and training ( $\$ /$ formalized worker/year). The value of the $\mathrm{C}_{\text {TCT }}$ variable is $\$ 68.6$, which was obtained from DoS.

## F. Total costs of alternative waste collection (TCoAWC )

Following are tables showing the total costs of waste collection for alterative scenarios.

Table S16. Cost calculation of waste collection of S-1 and S-2 in WMS (\$/year)

| Items | Integrated cost <br> (\$/year) | Existing waste <br> collection (\$/year) | Total annual cost <br> (\$/year) |
| :--- | :---: | :---: | :---: |
| Salary (\$/person/year) | $2,715,621$ | $4,086,923.08$ | $6,802,544$ |
| Working tools, clothing and <br> training (\$/ formalized worker) | 151,362 | 165,669 | 317,031 |
| Cost of trucks (\$/truck) | 168,333 | - | 168,333 |
| Vehicle maintenance (\$/year) | 305,828 | $1,132,429$ | $1,438,257$ |
| Diesel fuel consumption (\$/L) | $1,328,677$ | $1,045,033$ | $2,373,710$ |
| Total |  |  | $11,099,875$ |

Source: ${ }^{1}$ Cost of a second-hand truck is $\$ 25,000$, according to DoS officials (2020) with the assumption of a 15-year lifetime.

Table S17. Cost calculation of waste collection of S-3 and S-4 WMS (\$/year)

| Items | Integrated cost <br> (\$/year) | Existing waste <br> collection (\$/year) | Total annual cost <br> (\$/year) |
| :--- | :---: | :---: | :---: |
| Salary (\$/person/year ) | $3,592,183$ | $6,134,615.38$ | $7,679,106$ |
| Working tools, clothing and <br> training (\$/ formalized worker) | 200,219 | $258,203.68$ | 365,888 |
| Cost of trucks (\$/truck) | 170,000 | - | 170000 |
| Maintenance of the vehicles <br> (\$/year) | 308,856 | $1,132,428.62$ | $1,441,285$ |
| Diesel fuel consumption (\$/L) | $1,219,578$ | $1,045,032.80$ | $2,264,611$ |
| Total |  |  | $11,920,890$ |

## Section 2. MRF/recycling

(1) Greenhouse gas emissions

For the calculation of GHG emissions (ton $\mathrm{CO}_{2} \mathrm{eq} / \mathrm{year}$ ) of MRF at different scenarios, following are the related equations.

$$
\begin{equation*}
\text { Total GHG emissions }=\Sigma \mathrm{T}_{\text {Electricity }} \times \mathrm{Q}_{\mathrm{i}} \times \mathrm{GWPi}+\Sigma \mathrm{TFC} \times \mathrm{Mi} \times \mathrm{GWPi} \tag{21}
\end{equation*}
$$

Therein, $\mathrm{T}_{\text {Electricity }}$ signifies the total amount of electric energy using on the recycling treatment(kWh/day), $\mathrm{Q}_{\mathrm{i}}$ stands for the mass of GHG emissions from electricity ( $\mathrm{kg} \mathrm{CO}_{2} /$ day) where i is assigned for a category, GWP expresses the equivalence factor based on carbon dioxide as 1, TFC represents the total amount of diesel consuming on recycling treatment (L/day), and Mi denotes gaseous emissions from diesel fuel ( $\mathrm{kg} \mathrm{CO}_{2} /$ day). The total amount of electricity and diesel fuel are calculated as

$$
\begin{align*}
& \mathrm{T}_{\text {Electricity }}=\mathrm{X} \times \mathrm{A} \text { and }  \tag{22}\\
& \mathrm{TFC}=\mathrm{X} \times \mathrm{B}, \tag{23}
\end{align*}
$$

where X represents the amount of waste (ton/day) taken at MRF, A represents the electricity consumption per ton of waste ( $\mathrm{kWh} / \mathrm{ton}$ ), and B denotes the diesel use per ton of waste (L/ton). Furthermore, to calculate the avoided GHG emissions from equivalent amount of materials production from virgin processes, the following equation was applied. It incorporates the IDEA database of MILCA software.

$$
\begin{equation*}
\text { Total GHG emissions }=\Sigma \mathrm{TA}_{R} \times \mathrm{PC}_{\mathrm{i}} \times \mathrm{GHG} \tag{24}
\end{equation*}
$$

In that equation, $\mathrm{TA}_{R}$ is the amount of recyclable materials recovered from recycling process(ton/day), $\mathrm{PC}_{\mathrm{i}}$ represents the parentage compositions of waste recyclables within the total amount ( $100 \%$ ) of recyclables (see Table A18), and i is the type of material. Residues were considered as inert materials. Characterization factors are based on IPCC moldel 2007 for a 100-year time horizon.

Equation 22 has shown Net GHG emissions from recycling treatment as shown below.
Net GHG emissions (kg CO2eq) = Equation (21) - Equation (24)

Table S18. Percentage compositions of waste recyclables among the total amount (\%) of recyclables

| component | composition (\%) |
| :--- | :---: |
| glass | 11 |
| plastic | 39 |
| metal | 22 |
| paper | 28 |

$\square$

The following tables show descriptions of the designed model, assumptions, variable values, and calculations related to recycling treatments in different scenarios.

Table S19. Model designed for calculating parameters of recycling of waste in SO

| Parameters | Amount | Unit | Source |
| :---: | :---: | :---: | :---: |
| Total percentage of recyclable materials in household waste | 18 | \% | Azimi and Matsumoto, 2017 |
| Sorting efficiency at MRF | 95 | \% | - |
| Recycling rate | 80 | \% | - |
| * Consumption of diesel for operations, B | 3.21 | L/ton | Rajaeifar et al., 2015 |
| * Consumption of electricity for operations, A | 3.2 | kWh/ton | Rajaeifar et al., 2015 |
| Waste amount of dry recyclables to be sorted at MRF, X | $=0.009 \times 2527$ | t | calculation |
| Waste amount of dry recyclables to be sorted at MRF, X | 22.74 | t | calculation |
| Waste amount of dry recyclables recovered by sorting process | $\begin{gathered} =22.743 \times 0.95 \times \\ 10^{\wedge}-3 \end{gathered}$ | Gg | calculation |
| Waste amount of dry recyclables recovered by sorting process | 0.02160585 | Gg | calculation |
| Amount of dry recyclable materials recovered from recycling process (avoided material), $T A_{R}$ | $=0.02160585 \times 0.8$ | Gg | calculation |
| ** Amount of dry recyclable materials recovered from recycling process (avoided material), $T A_{R}$ | 0.01728468 | Gg | calculation |
| Avoided glass materials | 1,920.52 | kg | calculation |
| Avoided plastic materials | 6,721.82 | kg | calculation |
| Avoided metal materials | 3,841.04 | kg | calculation |
| Avoided paper materials | 4,801.3 | kg | calculation |
| Consumption of diesel for operations, TFC | 73 | L | calculation |
| *** Consumption of diesel for operations, | 2,694 | MJ | calculation |
| Consumption of electricity for operations, T Electricity | 73 | kWh | calculation |
| Total amount of recycling materials | 17,285 | kg | calculation |
| Total amount of recycling materials, $\mathrm{TA}_{R}$ | 17 | ton | calculation |
| *** Residues | 5.5 | ton | calculation |

Source: Rajaeifar, M.A.; Tabatabaei, M.; Ghanavati, H.; Khoshnevisan, B.; Rafiee, S. Comparative life cycle assessment of different municipal solid waste management scenarios in Iran. Renew. Sust. Energ. Rev. 2015, 51, 886-898.
** For the calculation of each avoided material, we multiplied the total amount of recyclable materials recovered from recycling process by their percentage compositions in household waste, as Table A19 has shown the compositions of recyclable materials.
*** For changing the amount of fuel into energy, we multiplied that by 36.9 MJ , which is the energy value of diesel fuel in L.
**** Residues are considered as inert materials when being landfilled. For that reason, only emissions related with fuel consumption were considered during landfilling.
We considered higher efficiency because two separations were conducted before going to MRF. In addition, the reference was given in Table A17

Note: In Table A19, we linked the variables in this table with the variables included in the formula above. Therefore, please follow this when you want to link the variables of other tables with the formula ones.

Table S20. Model designed for calcuating the paramaters for recycling of waste in S2

| Parameter | amount | unit | * source |
| :--- | :---: | :---: | :---: |
| Total percentage of recyclable materials in HSW | 18 | $\%$ | - |
| Sorting efficiency at MRF | 70 | $\%$ | - |
| Recycling rate | 70 | $\%$ | - |
| Consumption of diesel for operations | 3.21 | $\mathrm{~L} / \mathrm{ton}$ | - |
| Consumption of electricity for operations | 3.2 | $\mathrm{kWh} / \mathrm{ton}$ | - |
| Waste amount of mixed waste to be sorted at <br> MRF | $=2527 \times 10^{\wedge}-3$ | Gg | calculation |
| Waste amount of mixed waste to be sorted at <br> MRF | 2.527 | Gg | calculation |
| Waste amount of dry recyclables recovered by <br> sorting process | $=2527 \times 0.18 \times 0.7 \times$ | Gg | calculation |
| Waste amount of dry recyclables recovered by <br> sorting process | 0.318402 | Gg | calculation |
| Amount of dry recyclable materials recovered <br> from recycling process (avoided material) | $=0.318402 \times 0.7$ | Gg | calculation |
| Amount of dry recyclable materials recovered <br> from recycling process (avoided material) | 0.2228814 | Gg | calculation |
| Avoided glass materials | $2,4764.6$ | kg | calculation |
| Avoided plastic materials | $8,6676.1$ | kg | calculation |
| Avoided metal materials | $49,529.2$ | kg | calculation |
| Avoided paper materials | $61,911.5$ | kg | calculation |
| Consumption of diesel for operations per day | $8,111.67$ | L | calculation |
| Consumption of diesel for operations per day | $299,320.62$ | MJ | calculation |
| Total consumption of electricity for operations | $8,086.4$ | kWh | calculation |
| Total amount of recycling materials | 222.88 | ton | calculation |
| Total amount of residuals | 95.5 | ton | calculation |

* Some parameters have no written references because they are described above.

Table A21. Model designed for calcuating the paramaters in recycling of wastes in S3 and S4

| Parameter | amount | unit | source |
| :--- | :---: | :---: | :---: |
| Total percentage of recyclable materials in HSW | 18 | $\%$ | - |
| Efficiency of source-separation of recyclables | 50 | $\%$ | - |
| * Sorting efficiency at MRF from mixed recyclables | 84 | $\%$ | - |
| recycling rate | 92 | $\%$ | - |
| Consumption of diesel for operations | 3.21 | $\mathrm{~L} / \mathrm{ton}$ | - |
| Consumption of electricity for operations | 3.2 | $\mathrm{kWh} /$ ton | - |
| Waste amount of dry recyclables to be sorted at <br> MRF | $=2527 \times 0.18 \times 0.5 \times$ <br> $10 \wedge-3$ | Gg | calculation |
| Waste amount of dry recyclables to be sorted at <br> MRF | 0.22743 | Gg | calculation |
| Waste amount of dry recyclables recovered by <br> sorting process | $0.22743 \times 0.84$ | Gg | calculation |
| Waste amount of dry recyclables recovered by <br> sorting process | 0.1910412 | Gg | calculation |
| Amount of dry recyclable materials recovered from <br> recycling processes (avoided material) | $0.1910412 \times 0.92$ | calculation |  |
| Amount of dry recyclable materials recovered from <br> recycling processes (avoided material) | 0.175757904 | Gg | calculation |
| Avoided glass materials | 19528.66 | kg | calculation |
| Avoided plastic materials | 68350.296 | kg | calculation |
| Avoided metal materials | 39057.31 | kg | calculation |
| Avoided paper materials | 48821.64 | kg | calculation |
| Total consumption of diesel for operations | 730.05 | L | calculation |
| Total consumption of diesel for operations | 26938.86 | MJ | calculation |
| Total consumption of electricity for operations | 727.78 | kWh | calculation |
| Total amount of recycling materials | 175.76 | ton | calculation |
| Total amount of residuals | 51.67 | ton | calculation |

* For how it was selected this percent, please consult Table A22. We considered the average rate of efficiencies between minimum and maximum.

Table S22. Averaging manual sorting efficiency at MRF for source-separated waste

| material | minimum recovery <br> efficiency (\%) | maximum recovery <br> efficiency (\%) | average (\%) |
| :---: | :---: | :---: | :---: |
| paper | 60 | 95 | 78 |
| glass | 70 | 95 | 83 |
| plastic | 80 | 95 | 88 |
| metal | 80 | 95 | 88 |
| Average rate of <br> efficiency of MRF (\%) | - | - | 83.75 |

Source: Design of a Materials Recovery Facility (MRF) For Processing the Recyclable Materials of New York City's Municipal Solid Waste (2000).

Table S23. Estimation the GHG emissions of recycling waste treatment of different scenarios

| Scenarios | Impact category <br> $\left(\mathrm{CO}_{2}\right.$ eq) | Unit | Recycling | Avoided <br> emissions | Net <br> emission |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Baseline scenario | Global Warming | ton CO2 <br> eq/year | 85.03 | $13,302.92$ | $-13,217.89$ |
| Scenario 1 |  |  | - | - | 0.00 |
| Scenario 2 |  |  | $9,947.82$ | $171,537.64$ | $-161,589.82$ |
| Scenario 3 |  |  | 895.30 | $135,269.68$ | $-134,374.37$ |
| Scenario 4 |  |  | 895.30 | $135,269.68$ | $-134,374.37$ |

## (2) Cost

For calculating costs borne because of recycling treatment including the integration of informal workers, the following equation has been applied.
TCoWR = A + B+ C

In that equation, TCoWR represents the total cost of waste recycling (\$/year), A denotes the cost of electricity and diesel fuel (\$/year), B stands for the salary cost (\$/year), and C is the total cost for working tools, clothing, and training (\$/year)

## A. Cost of electricity and diesel fuel for recycling treatment

Following is the formula for the cost of electricity and diesel fuel for waste recycling.

$$
\begin{equation*}
\mathrm{A}=\mathrm{C}_{\text {Electricity }}+\mathrm{C}_{\mathrm{D}} \tag{27}
\end{equation*}
$$

Therein, $\mathrm{C}_{\text {Electricity }}$ signifies the total cost of electricity ( $\mathrm{kWh} /$ year) and $\mathrm{C}_{\mathrm{D}}$ ( $\$ /$ year) expresses the total cost of diesel consumption. These were found using the equations below as

$$
\begin{align*}
& C_{\text {Electricity }}=X \times E L \times E P \text { and }  \tag{28}\\
& C_{D}=X \times D \times D P, \tag{29}
\end{align*}
$$

where X stands for the amount of waste (ton/day), EL denotes the unit value of electricity use ( $\mathrm{kWh} / \mathrm{ton}$ ), EP represents the electricity price ( $\$ / \mathrm{kWh}$ ), 365 signifies the conversion factor into year, D denotes the unit value of diesel consumption (L)/day), and DP stands for the diesel price ( $\$ / \mathrm{L}$ ). Values of EP ( 0.16 ) and DP (0.49) were obtained through an interview survey.

## B. Salary cost

Following is the formula which has been applied for calcuating the salary cost for integration of informal workers into the formalized system at MRF for waste reycling.

$$
\begin{equation*}
B=(X / y) \times S \tag{30}
\end{equation*}
$$

Here, B represents the salary cost of integeared workers (\$/year), X denotes the amount of waste taken to MRF (ton/day), y stands for the average rate of sorting (tones/person/day), and S expresses the salary cost per formalized worker (\$/person/year).

Below are the cost calculations of labor for each scenario:
S-2: Following table shows the descriptions of the designed model, assumptions, variable values and results.

Table S24. Salary cost for the integration of informal workers for recycling process at MRF in S-2

| Item | Amount |
| :--- | :---: |
| Amount of waste collected to MRF (ton/day), X | 2,527 |
| * Average rate of sorting at MRF (tones/person/day),  <br> y 5.12 <br> Salary (\$/year), S $1,230.77$ <br> Total (\$/year), B $607,451.92$ $\mathbf{l}$ (1) |  |

Source: "Integrated Solid Waste management - A Life Cycle Inventory". White et al. (1995), Chapman \& Hall, London; and Ministry of Urban Development Government of India (2000).

S-3 and S-4: In the case of source-separated waste materials at MRF, first we found the average sorting rate amount per person per day (tons/day/person) (Table A25) as

$$
\begin{equation*}
y=S R_{i} \times(W H-1), \tag{31}
\end{equation*}
$$

where SR denotes the average range of sorting rate of each recyclable material at MRF; i is their category. Also, WH represents the working hours, which are $8 \mathrm{~h} / \mathrm{day}$, with ( -1 ) one hour break time for serving and prayers.

Table S25. Average amounts of sorting of source-separated materials at MRF (ton/day/person)

| Material | Range of sorting rate <br> (tons/hours/person) |  | Average sorting |
| :--- | :---: | :---: | :---: |
| Paper (tons/hours/person) | 0.75 | 5.00 | 2.88 |
| Glass, tons/hours/person) | 0.45 | 0.90 | 0.68 |
| Plastics, tons/hours/person) | 0.15 | 0.30 | 0.23 |
| Aluminum <br> (tons/hours/person) | 0.05 | 0.06 | 0.06 |
| Overall average of sorting at <br> MRF per person per day <br> (tons/day/person) |  | $\mathrm{y}=6.70$ |  |

Table S26. Total number of workers to be integrated for processes on source-separated waste at MRF

| Item | Amount |
| :--- | :---: |
| Waste amount (ton/ year), X | 82964.5 |
| average rate of sorting (ton/day/person), y | 6.7 |
| Salary (\$/year), S | $1,230.77$ |
| Total, B (\$/year) | $58,370.26$ |

Note: We regarded 261 days/year as working days after excluding weekends.
C. Costs for working tools, clothing and training

Following is the formula to calculate this cost in the scenarios.

$$
\begin{equation*}
\mathrm{C}=\mathrm{NW} \times \mathrm{C}_{\mathrm{TCT}} \tag{32}
\end{equation*}
$$

In that equation, NW stands for the total number of workers to be integrated at MRF, and $\mathrm{C}_{\text {TCT }}$ denotes the cost for working tools, clothing and training (\$/ formalized worker/year). NW is calculable by X/y , which is defined at section $B$ (salary cost). The value of $C_{T C T}$ variable is $68.6 \$ / y e a r$, as obtained from DoS.
D. Total cost of waste recycling (TCoWR)

The following tables are cost calculations for waste recycling / MRF and revenues from the sale of recyclables of the scenarios.

Table S27. Cost calculation of waste recycling treatment in S-2 of WMS (\$/year)

| Parameter | Total annual cost (\$/year) |
| :--- | :---: |
| Salary (\$/person/year) | $607,451.92$ |
| Working tools, clothing and training (\$/ formalized <br> worker) | $33,857.85$ |
| Electricity cost for recycling process (\$/year) | $473,002.56$ |
| Diesel cost for recycling process (\$/year) | $1,450,772.18$ |
| Total | $2,565,084.52$ |

Table S28. Cost calculation of waste recycling treatment in S-3 and S-4 of WMS (\$/year)

| Parameter | Total annual cost (\$/year) |
| :--- | :---: |
| Salary (\$/person/year) | $58,370.26$ |
| Working tools, clothing and training (\$/ formalized <br> worker) | $3,253.41$ |
| Electricity cost for recycling process (\$/year) | $42,570.23$ |
| Diesel cost for recycling process (\$/year) | $130,569.50$ |
| Total | $234,763.40$ |

E. Cost revenues from sales of recycled materials Following is the formula for calculating revenues from sales of recycled products.

$$
\begin{equation*}
\mathrm{CR}=\Sigma(\mathrm{Mi} \times \mathrm{Pj}) \tag{33}
\end{equation*}
$$

In that equation, CR represents the total cost of revenues (\$/year); Mi dentos the recycled materials at MRF (ton/day), i is assigned for the type of material, P stands for the market price of materials per ton (\$/ton), with j representing the category.

Table S29. Annual revenue from the sale of recyclables in S-2

| Material | Amount <br> recycled <br> (ton/day), M | $*$ Market price <br> (\$/ton) | Total revenue (\$/year) |
| :--- | :---: | :---: | :---: |
| Glass | 24.76 | 256.41 | $2,317,712.56$ |
| Plastic | 86.68 | 128.21 | $4,055,996.99$ |
| Metal | 49.53 | 256.41 | $4,635,425.13$ |
| Paper | 61.91 | 51.28 | $1,158,856.28$ |
| Total |  |  | $12,167,990.96$ |

* Source survey interview (2020)

Table S30. Annual revenue from the sale of recyclables in S-3 and S-4

| Material | Amount <br> recycled <br> (ton/day ) | Market price <br> $(\$ /$ ton $)$ | Total revenue (\$/year) |
| :--- | :---: | :---: | :---: |
| Glass | 19.53 | 256.41 | $1,827,681.91$ |
| Plastic | 68.35 | 128.21 | $3,198,443.34$ |
| Metal | 39.06 | 256.41 | $3,655,363.82$ |
| Paper | 48.82 | 51.28 | $913,840.95$ |
| Total |  |  | $9,595,330.02$ |

## Section 3. Landfilling

## (1) Greenhouse gas emissions

Because landfill gas emissions mainly consist of $\mathrm{CO}_{2}$ and $\mathrm{CH}_{4}$, but because $\mathrm{CO}_{2}$ has biogenic origin and we did not consider that in the system boundary of the study. Therefore, we only calculated the emissions associated with $\mathrm{CH}_{4}$ gas. Calculation of $\mathrm{CH}_{4}$ emissions was conducted based on the IPCC default method as

$$
\begin{equation*}
\mathrm{CH}_{4}=\left(\mathrm{HWDS} \times \mathrm{DOC} \times \mathrm{MCF} \times \mathrm{DOC}_{\mathrm{F}} \times \mathrm{F} \times 16 / 12-\mathrm{R}\right)(1-\mathrm{OX}), \tag{34}
\end{equation*}
$$

where HWDS represents fraction of HW interred at disposal sites, MCF stands for the methane correction factor, DOC denotes is the degradable organic carbon fraction, $D O C_{F}$ expresses the fraction of degradable organic carbon that ultimately is degraded and released, F is the fraction of $\mathrm{CH}_{4}$ in Landfill gas by volume, R expresses the recovered $\mathrm{CH}_{4}$, and $16 / 12$ is the molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$. Also, OX is the oxidation factor. The default values for calculating the $\mathrm{CH}_{4}$ release from open dumps are followed by $0.4,0.77,0$ and $50 \%$, respectively, for MCF, $\mathrm{DOC}_{\mathrm{F}}, \mathrm{OX}$ and F . For $\mathrm{CH}_{4}$ estimation for unsanitary landfilling, the default value of MCF was selected 0.6 because the current landfill activities are similar to the uncategorized management approach, which is neither to managed or unmanaged disposal sites, based on IPCC report
standards. However, in sanitary landfill, this value is 1 because it is a managed site. The amount of diesel use at landfilling has been calculated using the following equation.

$$
\begin{equation*}
\mathrm{TFC}=\mathrm{X} \times \mathrm{A} \tag{35}
\end{equation*}
$$

Here, TFC is the total fuel use on landfilling the waste (L/day), X represents the amount of waste (ton/day), and A denotes the unit value of fuel consumption at landfilling (L/ton).

The amount of diesel consumed at an unsanitary landfilling is $0.35 \mathrm{~L} /$ ton, based on official data, whereas a sanitary landfill uses $3 \mathrm{~L} /$ ton. Emissions of these fuels, used at landfills both for waste as well as residues, have been included also as landfill emissions. After generating these inventory data, we calculated the GWP impact category based IPCC model 2006 for a 100-year time horizon. Data of emission factors were obtained from the IDEA database of MILCA software. The following tables show detailed explanations of calculations for $\mathrm{CH}_{4}$ emission in different scenarios.

Table S31. Model designed for calculation of $\mathrm{CH}_{4}$ for the open dumping baseline scenario (S-0)

| Parameter | Amount | Unit | Source |
| :--- | :---: | :---: | :---: |
| Waste amount deposited, HWDS | $=0.43 \times 2527 \times 10^{\wedge}-3$ | Gg | calculation |
| Waste amount deposited, HWDS | 1.08661 | Gg | calculation |
| * Degradable organic carbon, DOC | $=0.74 \times 0.15+0.05 \times$ <br> 0.4 | $\mathrm{Gg} \mathrm{C/Gg}$ | IPCC |
| * Degradable organic carbon, DOC | 0.131 | $\mathrm{Gg} \mathrm{C/Gg}$ | IPCC |
| Methane correction factor, MCF | 0.4 | - | IPCC |
| Fraction of DOC under anerobic <br> condition, DOC | 0.77 | IPCC |  |
| Methane generation in Landfill by <br> volume, F | $16 / 12$ | IPCC |  |
| Molecular weight ratio of CH4/C, used <br> as conversions factor to change C to CH4 | 0 | Gg | Assumed |
| Recovered methane, R | 0 | IPCC |  |
| Oxidation factor, OX | 0.02922836 | Gg | calculation |
| CH $_{4}$ emissions | 29.23 | ton | calculation |
| CH $_{4}$ emissions |  |  |  |

* DOC $=\%$ of food waste $\times 0.15+\%$ of paper waste $\times$ paper

Table S32. Model designed for calculation of $\mathrm{CH}_{4}$ for unsanitary landfill of baseline scenario (S-0)

| Parameter | Amount | Unit | Source |
| :--- | :---: | :---: | :---: |
| Waste amount deposited, HWDS | $=0.525 \times 2527 \times 10^{\wedge}-3$ | Gg | calculation |
| Waste amount deposited, HWDS | 1.326675 | Gg | calculation |
| Degradable organic carbon, DOC | 0.131 | $\mathrm{Gg} \mathrm{C} / \mathrm{Gg}$ | IPCC |
| Methane correction factor, MCF | 0.6 | - | IPCC |
| Fraction of DOC under anerobic <br> condition, DOC $_{F}$ | 0.77 | - | IPCC |


| Methane generation in Landfill by <br> volume, F | 0.5 |  | IPCC |
| :--- | :---: | :---: | :---: |
| Molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$, used <br> as conversions factor to change C to <br> $\mathrm{CH}_{4}$ | $16 / 12$ |  | IPCC |
| Recovered methane, R | 0 | Gg | Assumed |
| Oxidation factor, OX | 0 | Gg | calculation |
| $\mathrm{CH}_{4}$ emissions | 0.0535 | ton | calculation |
| CH $_{4}$ emissions | 53.53 | L 隹 |  |
| Fuel consumption at unsanitary <br> landfilling | 0.35 | L | calculation |
| Total fuel consumption at unsanitary <br> landfilling | $=1.326675 \times 0.35 \times$ |  |  |
| Total fuel consumption at unsanitary <br> landfilling | 459 | L | calculation |
| * Change into energy | $=36.9 \times 459$ | MJ | calculation |
| Change into energy | 16,946 | MJ | calculation |
| Fuel consumption for treatment of <br> residues after recycling process | $=5.5 \times 0.35$ | L | calculation |
| Fuel consumption for treatment of <br> residues after recycling process | 1.9 | L | calculation |
| Change into energy | 69.7 | MJ | calculation |
| ** Total energy | 17,015 | MJ | calculation |

* Colorific Value ( CV) of diesel = 36.9 MJ/L . ** Total energy means the summation of fuel energy used for dumping the waste and the residues after recycling left and go to landfill site.

Note: Tables A31 and 32 have given a bit more detail to make the calculations of the following table understandable.

Table S33. Model designed for calculation of $\mathrm{CH}_{4}$ emissions for unsanitary landfill of S-1

| Parameter | Amount | Unit | Source |
| :--- | :---: | :---: | :---: |
| Waste amount deposited, HWDS | 2.527 | Gg | calculation |
| Degradable organic carbon, DOC | 0.131 | $\mathrm{Gg} \mathrm{C/Gg}$ | IPCC report |
| Methane correction factor, MCF | 0.6 | - | IPCC report |
| Fraction of DOC under anerobic <br> condition, DOC | 0.77 | - | IPCC report |
| Methane generation in landfill by <br> volume, F | 0.5 |  | IPCC |
| Molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$, used <br> as conversion factor to change C to <br> $\mathrm{CH}_{4}$ | $16 / 12$ |  | Assumed |
| Recovered methane, R $^{\text {Oxidation factor, OX }}$ | 0 | Gg | IPCC |


| $\mathrm{CH}_{4}$ emissions | 0.101959396 | Gg | calculation |
| :--- | :---: | :---: | :---: |
| $\mathrm{CH}_{4}$ emissions | 101.96 | ton | calculation |
| Fuel consumption at unsanitary <br> landfilling | 0.35 | L | DoS |
| Total fuel consumption at unsanitary <br> landfilling | 884 | calculation |  |
| Change into energy | 32,636 | MJ | calculation |

Table S34. Model designed for calculating $\mathrm{CH}_{4}$ emissions for unsanitary landfill of S-2

| Parameter | Amount | Unit | Source |
| :---: | :---: | :---: | :---: |
| Waste amount deposited, HWDS | 2.208598 | Gg | calculation |
| Degradable organic carbon, DOC | 0.111 | Gg C/Gg | IPCC report |
| Methane correction factor, MCF | 0.6 |  | IPCC report |
| Fraction of DOC under anerobic condition, DOC ${ }_{F}$ | 0.77 |  | IPCC report |
| Methane generation in Landfill by volume, F | 0.5 |  | IPCC report |
| Molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$, used as conversions factor to change C to $\mathrm{CH}_{4}$ | 12/44 |  | IPCC report |
| Recovered methane, R | 0 | Gg | assumed |
| Oxidation factor, OX | 0 |  | IPCC |
| $\mathrm{CH}_{4}$ emissions | 0.076 | Gg | literature |
| $\mathrm{CH}_{4}$ emissions | 76 | ton | calculation |
| Fuel consumption at unsanitary landfilling | 0.35 | L/ton | DoS |
| Total fuel consumption at unsanitary landfilling | 773 | L | calculation |
| Change into energy | 28524 | MJ | calculation |
| Fuel consumption for treatment of residues after recycling process | $=95.5 \times 0.35$ | L | calculation |
| Fuel consumption for treatment of residues after recycling process | 33.4 | L | calculation |
| Fuel consumption for treatment of residues after recycling process | 1,232.5 | MJ | calculation |
| Total energy | 29,756.46 | MJ | calculation |

Table S35. Model designed for calculating $\mathrm{CH}_{4}$ emissions for unsanitary landfill of S-3

| Parameter | Amount | Unit | Source |
| :--- | :---: | :---: | :---: |
| Waste amount deposited, HWDS | 2.29957 | Gg | calculation |


| Degradable organic carbon, DOC | 0.121 | Gg C/Gg | IPCC report |
| :---: | :---: | :---: | :---: |
| Methane correction factor, MCF | 0.6 |  | IPCC report |
| Fraction of DOC under anerobic condition, DOC ${ }_{F}$ | 0.77 |  | IPCC report |
| Methane generation in Landfill by volume, F | 0.5 |  | IPCC report |
| Molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$, used as conversions factor to change C to $\mathrm{CH}_{4}$ | 12/44 |  | IPCC report |
| Recovered methane, R | 0 | Gg | assumed |
| Oxidation factor, OX | 0 |  | IPCC |
| $\mathrm{CH}_{4}$ emissions | 0.085700375 | Gg | calculation |
| $\mathrm{CH}_{4}$ emissions | 85.7 | ton | calculation |
| Fuel consumption at unsanitary landfilling | 0.35 | L/ton | Dos |
| Total fuel consumption at unsanitary landfilling | 804.85 | L | calculation |
| Change into energy | 29,698.95 | MJ | calculation |
| Fuel consumption for residues treatment after recycling process | 51.67 | ton | calculation |
| Fuel consumption for residues treatment after recycling process | 18.09 | L | calculation |
| Change into energy | 667.36 | MJ | calculation |
| Total energy | 30,366.29 | MJ | calculation |

Table S36. Model designed for calculating $\mathrm{CH}_{4}$ emissions for unsanitary landfill of S-4

| Parameter | Amount | Unit | Source |
| :---: | :---: | :---: | :---: |
| Waste amount deposited, HWDS | 2.29957 | Gg | calculation |
| Degradable organic carbon, DOC | 0.121 | Gg C/Gg | IPCC report |
| Methane correction factor, MCF | 1 | - | IPCC report |
| Fraction of DOC under anerobic condition, DOC $_{F}$ | 0.77 | - | IPCC report |
| Methane generation in Landfill by volume, F | 0.5 |  | IPCC report |
| Molecular weight ratio of $\mathrm{CH}_{4} / \mathrm{C}$, used as conversions factor to change C to CH 4 | 12/44 |  | IPCC report |
| Recovered methane, R | 0 | Gg | assumed |
| Oxidation factor, OX | 0 |  | IPCC |
| $\mathrm{CH}_{4}$ emissions | 0.142833958 | Gg | calculation |
| $\mathrm{CH}_{4}$ emissions | 142.8 | ton | calculation |


| Fuel consumption at sanitary <br> landfilling | 3.00 | L/ton | literature |
| :--- | :---: | :---: | :---: |
| Total fuel consumption at <br> sanitary landfilling | $6,898.71$ | L | calculation |
| Change into energy | $254,562.39$ | MJ | calculation |
| Fuel consumption for <br> residues treatment after <br> recycling process | 155.02 | L | calculation |
| Energy | $5,720.10$ | MJ | calculation |
| Total energy | $260,282.5$ | MJ | calculation |

Table S37. Estimating GHG emissions at a landfill site under different scenarios

| Scenario | Impact category <br> (CO2eq) | Unit | Open dumping | Unsanitary <br> landfilling | Sanitary <br> landfilling |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Baseline <br> scenario | Global Warming | ton CO2 <br> eq/year | $267,910.00$ | $488,947.67$ | - |
| Scenario 1 |  |  | - | $931,316.31$ | - |
| Scenario 2 |  |  | - | $689,842.28$ | - |
| Scenario 3 |  |  | - | $770,534.75$ | - |
| Scenario 4 |  |  | - | - | $1,308,513.88$ |

(2) Cost

## A. Estimating the number of workers

The current WMS has 36 workers working at the landfill site. They are able to landfill $52.71 \%$ ( 1,332 ton/day) of waste, including $52.5 \%$ of that which has been collected plus residues ( $0.21 \%$ ) from reycling treatent. Therefore, a worker, on average, can treat 37 tons of waste per day at an unsanitary landfill of Kabul city. However, for a sanitary landfill, formalized workers have been assumed as fewer than a tenth in number compared with the number at an MRF. Because the number of formalized workers at an MRF has been calculated as 494. The equation of integration of informal workers at a landfill site is

$$
\begin{equation*}
A=x / A, \tag{36}
\end{equation*}
$$

where A represents the number of informal workers to be integrated (number), X represents the amount of waste that is landfilled (ton/day), and $A$ is the amount of waste treated per person per day (ton/person/day).

Table S38. Number of informal workers to be integrated at landfill site in different alternative scenarios (ton/day)

| Scenario 1 | 33 |
| :---: | :---: |
| Scenario 2 | 26 |
| Scenario 3 | 27 |
| Scenario 4 | 13 |

## B. Cost calculation

The equation for calculation the cost at landfill site is

$$
\begin{equation*}
B=X \times C o L, \tag{37}
\end{equation*}
$$

where B represents the total cost (ton/year), X signifies the amount of waste (ton/day), and CoL stands for the cost of landfill per ton of waste(\$/ton).

Table S39. Cost calculation of waste landfilling in different scenarios of WMS (\$/year)

| Scenario | Amount of waste <br> (ton/day), X | Unit cost (\$/ton), CoL | Total cost (ton/year) |
| :---: | :---: | :---: | :---: |
| Baseline scenario | $1,331.73$ | ${ }^{\mathrm{a}} 1.60$ | $777,729.74$ |
| Scenario 1 | $2,527.00$ | 1.60 | $1,475,768.00$ |
| Scenario 2 | $2,304.12$ | 1.60 | $1,345,605.26$ |
| Scenario 3 | $2,351.63$ | 1.60 | $1,373,349.70$ |
| Scenario 4 | $2,351.63$ | ${ }^{\mathrm{b}} 10.00$ | $8,583,435.63$ |

Sources: ${ }^{\text {a }}$ Department of sanitation (2020) ${ }^{\text {b }}$ Global study for purpose of global world bank guidance development solid waste management holistic decision modeling (2008).

## Section 4. Power generation

The electricity mix grid of Kabul city consists of energy produced from domestic resources (40\%), and imported resources from Uzbekistan (60\%), according to Da Afghanistan Breshna Sherkat (DABS). Table A40 presents the electric energy sources and their contributions in Kabul city. In addition, the unit price of electricity in commercial and industrial zones is $\$ 0.16 / \mathrm{kWh}$.

Table S40. Electricity grid mix of Kabul city

| Sources of energy |  |
| :--- | :---: |
| Amount in \% |  |
| ${ }^{\text {B }}$ Imprgy from domestic resources |  |
| Hydroelectric power | 62 |
| Heavy oil | 38 |
|  |  |
| Natural gas | 60 |
| Coal | 86.12 |
| Heavy oil | 6.20 |


| Hydroelectric power | 6.63 |
| :--- | :---: |
| Total |  |
| Natural gas | 51.67 |
| Coal | 3.72 |
| Heavy oil | 15.90 |
| Hydroelectric power | 28.79 |

Source: ${ }^{\text {a }}$ DABS (2020) ${ }^{\text {b }}$ IDEA database
(1) Greenhouse gas emissions

The GHG emissions from electricity consumption have been integrated with diesel fuel emissions at the section of recycling treatment, where we use electric energy. To calculate GHG releases, we applied the IDEA database after generating basic data (see MRF/recycling).

## (2) Cost

Electricity cost calculations were conducted in the section of MRF/recycling, as the price of each kilowatt hour in commercial and industrial zones as \$0.16 [DABS, 2020].

