



# Article Hydrogen-Rich Gas Production from Two-Stage Catalytic Pyrolysis of Pine Sawdust with Calcined Dolomite

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Abstract: The potential of catalytic pyrolysis of biomass for hydrogen and bio-oil production has drawn great attention due to the concern of clean energy utilization and decarbonization. In this paper, the catalytic pyrolysis of pine sawdust with calcined dolomite was carried out in a novel moving bed reactor with a two-stage screw feeder. The effects of pyrolysis temperature (700–900 °C) and catalytic temperature (500–800 °C) on pyrolysis performance were investigated in product distribution, gas composition, and gas properties. The results showed that with the temperature increased, pyrolysis gas yield increased, but the yield of solid and liquid products decreased. With the increase in temperature, the CO and H<sub>2</sub> content increased significantly, while the CO<sub>2</sub> and CH<sub>4</sub> decreased correspondingly. The calcined dolomite can remove the tar by 44% and increased syngas yield by 52.9%. With the increasing catalytic temperature, the catalytic effect of calcined dolomite was also enhanced.

Keywords: catalytic pyrolysis; biomass; hydrogen; two-stage; dolomite; temperature; catalytic temperature



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# 1. Introduction

Biomass is a carbon-neutral renewable fuel with significant potential to reduce greenhouse gas emissions. China has abundant biomass reserves, with an annual production of about 3.494 billion tons, including available straw resources (694 million tons) and forestry residues (350 million tons). All of this showed great potential for energy utilization [1]. Biomass can be converted into a variety of high-value products, including chemicals, biofuels and advanced materials by thermochemical and biochemical pathways. Among different technologies of biomass utilization, thermochemical conversion is the most efficient method with the shortest time scale of the process [2]. Thermochemical conversion includes pyrolysis, hydrothermal liquefaction and gasification [3–5]. Pyrolysis is a promising technology for biofuels and chemicals and is considered a revolutionary and straightforward energy production method [6,7].

Pyrolysis is an efficient thermochemical conversion technology, which can accomplish the poly-generation of solid, liquid and gas products [8]. Pyrolysis is a process in which carbon-based raw materials such as biomass are heated and converted into char, tar, CO, H<sub>2</sub>, CH<sub>4</sub> and other hydrocarbons under anoxic conditions. The pyrolysis of biomass is able to produce liquid fuels, hydrogen and high-value chemicals [9–11]. Pyrolysis can process all kinds of organic waste and efficiently transform them into energy, with significant economic and environmental benefits. Therefore, utilizing biomass pyrolysis for hydrogen-rich gas can not only reduce the pressure of energy and the environment but also accomplish resource utilization of agricultural and forestry wastes.

Some research on biomass pyrolysis has been carried out in the literature. Cho et al. evaluated the value of sesame waste pyrolysis for syngas, found that the increase in syngas yield was proportional to temperature (500 °C, 600 °C, 700 °C) [12]. Kazimierski et al. prepared biochar by pyrolysis of orchard pruning residue between 25 °C and 600 °C and

measured the pyrolysis products yield. The results showed that the high heating value of the pyrolysis products increased from 29.52 MJ/kg (400 °C) to 30.53 MJ/kg (600 °C) [13]. Parket al. conducted pyrolysis of bark and studied the effect of temperature on the three-phase pyrolysis products. The results showed that with the increase in temperature from 300 °C to 700 °C, the non-condensable gas increased from 6.3 wt% to 17.5 wt%, while char yield decreased from 63.6 wt% to 30.6 wt% [14]. Gao et al. and Desisto et al. investigated the influence of temperature on the pyrolysis of pine sawdust [15,16]. They found that the maximum liquid yield was achieved at 500 °C and gas yield increased with temperature. However, most studies on pyrolysis were limited to low or medium temperatures for liquid fuels, the high-temperature pyrolysis of biomass for hydrogen and syngas has been rarely studied.

Catalyst can significantly influence the biomass pyrolysis process, improving the product quality and reaction efficiency. The catalysts for biomass catalytic pyrolysis can be divided into synthetic metal catalysts and natural ore catalysts. Metal catalysts include alkali metal catalysts, iron-based catalysts, nickel-based catalysts and mixed metal catalysts. Xie et al. investigated the effect of pyrolysis temperature on gas production of pine sawdust using different nickel-based catalysts [17]. Their results indicated that more syngas and high-quality char could be obtained at 750 °C. Qu et al. used Ni/Fe bimetal ZSM-5 as a catalyst to study the catalytic pyrolysis kinetics and product properties of waste tires. The results showed that ZSM-5loaded with 7 wt% Ni and 3 wt% Fe had the best catalytic effect, and the catalytic activation energy decreased by 13% [18]. Galiwango et al. used transition metal phosphatizing catalysts of nickel, cobalt and iron to catalyze the pyrolysis of jujube palm. The study found that the product yield of C7–C8 compounds was 3.6% without catalyst and increased to 68.0% with a catalyst [19]. Kim et al. used soil-rich catalysts (Co/SiO<sub>2</sub> and Ni/SiO<sub>2</sub>) to pyrolyze two kinds of biomass (barn grass and echinococcus). Under the catalyst of Ni and Co, the syngas yield was 2–3 times greater than that of catalyst-free pyrolysis [20]. Laura et al. and Gao et al. have recently reported the state-ofthe-art of metal catalysts, particularly in Ni-based catalysts, for biomass pyrolysis [21,22]. Although Ni-based catalysts such as Ni/Al<sub>2</sub>O<sub>3</sub> have been widely used and studied for reforming biomass tar, current studies are limited to bench scale. Further knowledge of the catalyst is required to scale up for industrial application, especially in catalyst deactivation and regeneration.

Compared with synthetic mental catalysts, natural ore catalysts are of low cost, including dolomite, magnesite, olivine, limestone and calcite. Aljeradat et al. studied the catalytic effect of different minerals on the jujube kernel pyrolysis. They found that the catalytic oil productions rate of oil shale ash was the highest (44%), and the catalytic gas productions rate of zeolite tuff was the highest (138.1 mL/g-feed) [23]. Khan et al. studied acid pretreatment and subsequent pyrolysis of rice straw in the presence of natural zeolite and HZSM-5 catalysts. The results showed that both catalysts significantly promoted the conversion of oxygen compounds to hydrocarbons [24]. Kawi et al. reviewed the research progress of biomass tar reforming catalyzed by natural minerals and waste. Dolomite had effective tar conversion performance, and olivine behaved similarly to dolomite. Both dolomite and calcite showed higher phenol conversion and selectivity at a higher temperature [25]. However, there are few studies on the catalytic pyrolysis of woody biomass using low-cost natural ore catalysts at high temperatures.

This study aims to study the high-temperature catalytic pyrolysis performance of pine sawdust for hydrogen-rich gas using calcined dolomite as a catalyst in a two-stage moving bed. The pyrolysis performance was examined in terms of pyrolysis products' distribution, gas composition, and gas properties. Firstly, the effects of pyrolysis temperature on pyrolysis performance were studied without catalysts. Moreover, the effect of catalytic temperature on pyrolysis performance was studied with calcined dolomite.

The majority of the catalytic pyrolysis studies in the literature are conducted using highcost metal catalysts, which resulted in difficulty for the large-scale application. However, this study used a low-cost modified natural ore catalyst, calcined dolomite, for the pyrolysis experiments. The influence of the high temperature (700–900  $^{\circ}$ C) and catalytic temperature (500–800  $^{\circ}$ C) was investigated by monitoring product distribution, gas composition, and gas properties.

## 2. Results and Discussion

## 2.1. Effect of Temperature on Pyrolysis

The pyrolysis experiments of pine sawdust were conducted at 700–900  $^{\circ}$ C in the pyrolysis bed without using catalysts in order to investigate the effect of temperature on pyrolysis performance. In the experiments, the velocity of the primary and secondary screw feeder was 171 r/h and 300 r/h, respectively, and the feeding rate of the biomass was 36 g/min. The mass balance of the pyrolysis experiments was in the range of 92–96%.

### 2.1.1. Effect of Temperature on Pyrolysis Products' Distribution

In flash pyrolysis, biomass generated three kinds of products in gas, liquid and solid. The gas and solid products were pyrolysis gas and the solid residue of biomass (char), respectively. The liquid product was tar generated during pyrolysis. The influence of temperature on the distribution of pine sawdust pyrolysis products is shown in Figure 1. With the pyrolysis temperature increasing, the gas yield increased, while the solid and liquid yield gradually decreased. Specifically, the gas yield increased from 50.67 wt% at 700 °C to 74.19 wt% at 900 °C. However, solid and liquid yield fell by 12.98 wt% and 10.54 wt%, respectively. In general, the high temperature was favorable to the formation of gaseous products, while the medium and low temperature was beneficial to the formation of liquid and solid products. The increase in gas products was because the growth of reaction temperature accelerated the primary pyrolysis of pine sawdust, and then promoted the secondary thermal cracking of the volatiles and char. The results were consistent with the research results of Li et al. [26] and Xu et al. [27]. Li et al. found that tar yield increased when the temperature rose, but it decreased after reaching a peak point (about 600 °C) because of the secondary cracking reactions [26]. In particular, the increase in gas products at a high temperature of 800-900 °C was due to the tar cracking and thermal cracking of char, which also led to a reduction in liquid and solid yield.

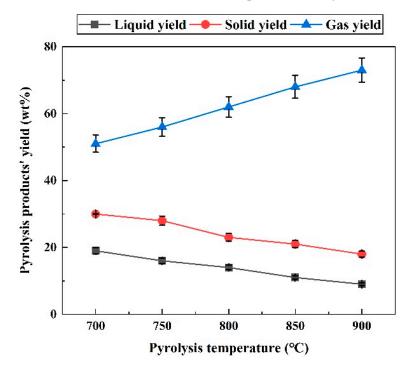


Figure 1. Effect of temperature on the distribution of pyrolysis products of pine sawdust.

#### 2.1.2. Effect of Temperature on Gas Composition

Figure 2 shows the influence of pyrolysis temperature on the composition of gas products from pine sawdust pyrolysis. The generated pyrolysis gas above 700 °C was mainly composed of CO, H<sub>2</sub>, CO<sub>2</sub> and CH<sub>4</sub>, which accounts for more than 94% of gas components. As shown in Figure 2, the CO content decreased as the temperature decreased during pyrolysis at 700–750 °C. However, the CO content increased slightly during pyrolysis at 750–850 °C and then decreased rapidly from 40% to 33% between 850 and 900 °C. At the same time, the CO<sub>2</sub> content decreased by 15% at 700–900 °C. This decrease in CO<sub>2</sub> could be because of the improved Boudouard reaction (Equation (1)) between char and CO<sub>2</sub> at high temperatures [28]. At 900 °C, the CO<sub>2</sub> and CH<sub>4</sub> decreased, whereas the H<sub>2</sub> increased, indicating the occurrence of the dry methane reforming reaction (Equation (3)). The decrease in CO at 900 °C may be a result of the reverse Boudouard reaction (Equation (2)) [29].

$$C + CO_2 \rightarrow 2CO$$
  $\Delta H_{298K} = +159 \text{ kJ/mol} \quad \Delta G_{1100K} = -21.8 \text{ kJ/mol}$  (1)

$$2CO \rightarrow C + CO_2$$
  $\Delta H_{298K} = -172 \text{ kJ/mol} \quad \Delta G_{1173K} = -162 \text{ kJ/mol}$  (2)

$$CH_4 + CO_2 \rightarrow 2CO + 2H_2 \quad \Delta H_{298K} = +247 \text{ kJ/mol} \quad \Delta G_{1173K} = -17 \text{ kJ/mol} \quad (3)$$

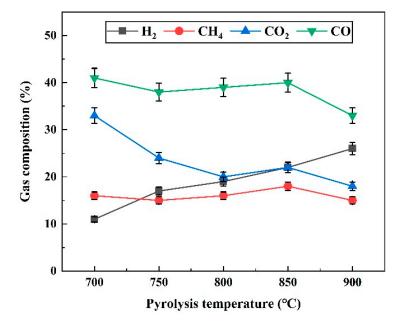
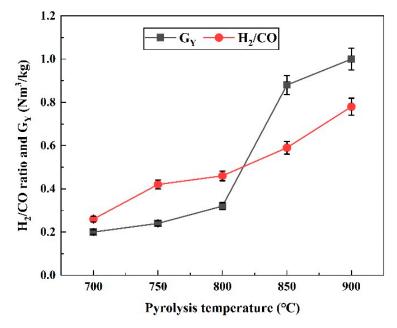


Figure 2. Effect of temperature on pyrolysis gas composition of pine sawdust.

The CH<sub>4</sub> content was relatively stable and finally reduced by 1% with the increase in temperature. This was because the pine sawdust firstly happened gasification reaction with  $O_2$ . When the  $O_2$  was exhausted, the remaining char gasified with  $CO_2$  and gas products continued the homogeneous reactions, as shown in Equations (1) and (2). Li et al. found that CO and  $CO_2$  were mainly from the O-containing functional groups, including carboxyl and carbonyl. When pyrolysis temperature was higher than 200 °C, carboxyl was broken to form  $CO_2$ . When the temperature was higher than 400 °C, carbonyl was split to form CO [26]. The concentration of H<sub>2</sub> consistently increased with an increase in temperature, mainly due to the decomposition of tar and the secondary gas reaction. Similar results were observed in the study of Laura et al. [30] and Lin et al.'s [31], which also showed that the H<sub>2</sub> content increased with an increase in pyrolysis temperature. The thermal decomposition of lignin and heavy hydrocarbons promoted H<sub>2</sub> formation. Besides, the secondary reactions of bio-oil and self-gasification of pine sawdust also contributed to H<sub>2</sub> formation as pyrolysis temperature increased [31].

#### 2.1.3. Effect of Temperature on Gas Products' Properties

The influence of pyrolysis temperature on  $H_2/CO$  and dry gas yield ( $G_Y$ ) is shown in Figure 3. As seen,  $H_2/CO$  ratio increased with the increase in pyrolysis temperature. In particular, the  $H_2/CO$  ratio was 0.25 at 700 °C, but at 900 °C, it jumped to 0.77, mainly because of the constant increase in  $H_2$  content. The rise of  $H_2$  was caused by the growth of pyrolysis temperature, which resulted in more  $H_2$  released from pine sawdust primary pyrolysis, tar cracking and gas conversion reactions. Similarly, the dry gas yield increased with an increase in pyrolysis temperature, but the increase rate of its value varied greatly over different temperature ranges. The growth rate of dry gas yield 700–800 °C was lower than that in the high-temperature range (800–900 °C). At 900 °C,  $H_2/CO$  and the dry gas yield reached maximum values (0.77 and 1.00 Nm<sup>3</sup>/kg). The increase in  $H_2/CO$  was due to more  $H_2$  released from tar cracking and the secondary gas reaction compared to CO. The increase in dry gas yield was because of the decomposition of semi-cellulose and cellulose with the temperature rise. Moreover, the lignin began to decompose at a higher temperature above 800 °C. In addition, with the temperature increasing, the secondary gas reaction also occurred, which reduced tar and char yield and increased dry gas yield.



**Figure 3.** Effect of pyrolysis temperature on  $H_2/CO$  and dry gas yield ( $G_Y$ ) of pine sawdust.

#### 2.2. Catalytic Effect of Calcined Dolomite

In this section, a pyrolysis bed was performed at 800 °C, and calcined dolomite was used as the catalyst for the catalytic bed. The catalytic bed was conducted at 500–800 °C under  $0.4 \text{ h}^{-1}$  weight hourly space velocity to study the catalytic effect of calcined dolomite. The mass balance of the catalytic pyrolysis experiments was in the range of 91–97%.

#### 2.2.1. Effect of Catalyst on Pyrolysis Products Yield

Figure 4 shows the catalytic effect of calcined dolomite on pyrolysis products of pine sawdust at different temperatures. The change in char yield was small with or without catalyst, ranging from 11.49 to 11.67 wt%. This was because the catalytic reforming bed only affected pyrolysis gas and tar, and it had no direct impact on char in the two-stage catalytic pyrolysis reactor. In the absence of the catalyst, the pyrolysis at yield was 10.35 wt% at 800 °C, but it decreased to 9.38 wt% after catalytic pyrolysis at 500 °C. With the catalytic temperature increased to 800 °C, the tar yield rapidly decreased to 3.83 wt%. The experimental results showed that the tar yield decreased with the increasing catalytic temperature, and the removal rate of tar reached more than 60% under the catalysis of calcined dolomite at 800 °C.

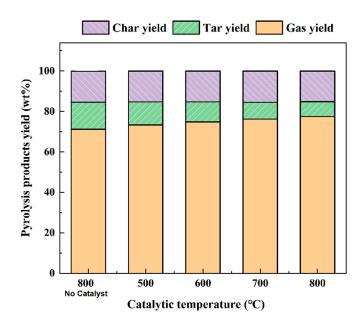


Figure 4. Effect of catalytic temperature on the distribution of pyrolysis products of pine sawdust.

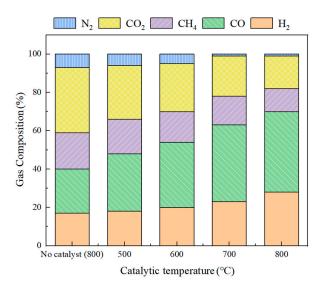
The trend of gas yield was just the opposite. With the increase in tar yield, gas yield increased significantly. The gas yield of pine sawdust was 61.23 wt% under catalyst-free pyrolysis at 800 °C. However, when the pyrolysis gas entered the catalytic reforming bed, the gas yield increased significantly. With the increase in catalytic temperature from 500 °C to 800 °C, the catalytic pyrolysis gas yield increased from 68.34 wt% to 78.12 wt%. The increase in gas yield was mainly attributed to the catalyst, which promoted the cracking of tar and organic volatiles. Since the pyrolysis of pine sawdust was mainly carried out in the pyrolysis bed, the role of catalyst in the catalytic reforming bed was to catalyze the pyrolysis of tar, thus increasing the yield of gas products.

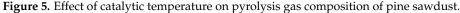
#### 2.2.2. Effect of Catalyst on Gas Composition

The composition of pyrolysis gas of pine sawdust at different catalytic temperatures is shown in Figure 5. The main gas components were H<sub>2</sub>, CO, CH<sub>4</sub> and CO<sub>2</sub>, while N<sub>2</sub> and O<sub>2</sub> were absent. Without the catalyst, CO and CO<sub>2</sub> were the main gas components. However, in the presence of the catalyst, the H<sub>2</sub> and CO contents increased significantly. With the increase in catalytic temperature from 500 °C to 800 °C, the H<sub>2</sub> and CO contents rose by 9.43 vol% and 11.45 vol%. The increase in H<sub>2</sub> and CO contents was attributed to the release of H<sub>2</sub> and CO from the tar cracking. The catalyst also promoted secondary gas reactions such as water–gas reactions (Equation (4)) and methane reforming reactions (Equation (3)). At the same time, the whole process was endothermic, so the increasing temperature was conducive to the catalytic cracking of tar. The research results of Zhao et al. showed that the increasing temperature promoted the dry methane reforming reaction between CO<sub>2</sub> and CH<sub>4</sub> (Equation (4)), leading to an increase in the H<sub>2</sub> and CO content [32].

$$CO + H_2O \rightarrow CO_2 + H_2 \qquad \Delta H_{298K} = -40 \text{ kJ/mol} \quad \Delta G_{1173K} = -11 \text{ kJ/mol} \quad (4)$$

On the contrary, the CO<sub>2</sub> content decreased significantly in the presence of the catalyst. The CO<sub>2</sub> content decreased from 34.33% to 27.88% at 500 °C, and the CO<sub>2</sub> content continued to decline with the increase in catalytic temperature. When it reached 800 °C, the content was only 17.53%. This was because the active components of calcined dolomite were MgO and CaO, which absorbed CO<sub>2</sub> in the reaction. Similarly, the CH<sub>4</sub> content decreased considerably with the increase in catalytic temperature. This was because calcined dolomite catalyzed the tar cracking and secondary gas reaction. The experimental results showed that calcined dolomite could effectively promote the cracking of tar and secondary gas reaction, so the H<sub>2</sub> and CO contents significantly increased.





2.2.3. Effect of Catalyst on Gas Products' Properties

The effect of catalytic temperature on the properties of pyrolysis gas products is presented in Table 1. As can be seen from Table 1, the syngas (H<sub>2</sub> + CO) content increased significantly after catalytic pyrolysis, from 45.48% (catalyst-free pyrolysis) to 48.71% (catalytic pyrolysis at 500 °C). The syngas content increased steadily to 69.55% when the catalytic temperature increased to 800 °C. This was due to the increasing trend of CO and H<sub>2</sub> content at higher catalytic temperatures. Similarly, the H<sub>2</sub>/CO ratio was only 0.47 before the catalytic pyrolysis. After catalysis at 500 °C, the H<sub>2</sub>/CO ratio rose to 0.58 and constantly increased with the increase in catalytic temperature, reaching a maximum of 0.65 at 800 °C. This was due to the fact that the tar cracking and secondary gas reaction released more H<sub>2</sub> than CO with the increasing temperature.

<b>Catalytic Temperature (°C)</b>	No Catalyst (800)	500	600	700	800
H <sub>2</sub> /CO (-)	0.47	0.58	0.59	0.60	0.65
Syngas (H <sub>2</sub> + CO) (%)	45.48	48.71	55.09	67.04	69.55
Dry gas yield (Nm <sup>3</sup> /kg)	0.36	0.41	0.47	0.48	0.74
Carbon conversion (wt%)	34.23	36.72	41.11	44.62	61.43
LHV (MJ/Nm <sup>3</sup> )	12.4	12.13	12.50	13.75	12.72

Table 1. Effect of catalytic temperature on properties of gas products.

The dry gas yield also increased significantly with a catalyst. Under the condition of no catalyst, the dry gas yield was only  $0.36 \text{ Nm}^3/\text{kg}$ . After catalysis at 500 °C, the dry gas yield increased from  $0.41 \text{ Nm}^3/\text{kg}$  to  $0.74 \text{ Nm}^3/\text{kg}$ . The increase in dry gas yield can be attributed to the catalytic cracking of the tar. In addition, the value of carbon conversion increased with the increase in catalytic temperature. The experimental results showed that calcined dolomite could effectively increase the syngas yield and improve the quality of syngas by increasing the ratio of H<sub>2</sub> and CO.

#### 3. Experimental Section

#### 3.1. Sample Preparation

The feedstock used in the experiment was pine sawdust, which came from the furniture processing factory of Wuhan in China. It was mainly sawdust, including shavings and wood residues from the wood processing. The sawdust was air-dried and screened by a vibrating material screener, and it was sieved to the particle sizes of more than 100 mesh (less than 177  $\mu$ m). In addition, the raw materials were dried at 105 °C for four hours in an oven before the experiments. The proximate analysis of the pine sawdust was measured

according to the Chinese standard-GB/T 28731-2012. Ultimate analysis of the sample was carried out by an elemental analyzer (Vario Micro Cube, Elementar, Langenselbold, Germany). The results of proximate analysis and ultimate analysis of pine sawdust are shown in Table 2.

Table 2. The	properties of	pine sawdust	(air-dry	basis).
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Sample	Proximate Analysis (wt%)			Ultimate Analysis (wt%)					
	Moisture	Volatile	Fixed Carbon	Ash	С	Н	Ν	S	0 *
Pine Sawdust	9.18	62.23	15.77	11.82	46.36	5.75	2.26	0.35	47.28

\*: by difference.

## 3.2. Catalyst Preparation

In this study, the low-cost natural ore was used as the catalyst. The main composition of the dolomite is  $CaCO_3$  and  $MgCO_3$ , and it also contains a small amount of Si, Fe and Al, as well as some trace mineral impurity. The dolomite was calcined at 900 °C for 4 h in a muffle furnace and then crushed and sieved to a particle size of 3–10 mm was selected as the catalyst. Their XRD patterns are shown in Figure 6, and their surface characteristics are listed in Table 3. As shown in Figure 6, at 900 °C, more CaO and MgO were generated by the decomposition of  $CaMg(CO_3)_2$  in dolomite, and the catalytic components increased significantly after high-temperature calcination. As seen in Table 3, the specific surface area of calcined dolomite increased more than 30 times, compared to the original dolomite. Therefore, the catalytic properties of calcined dolomite were improved compared with the original dolomite. The chemical analysis of calcined dolomite is shown in Table 4. As seen, the CaO and MgO were the major components in calcined dolomite.

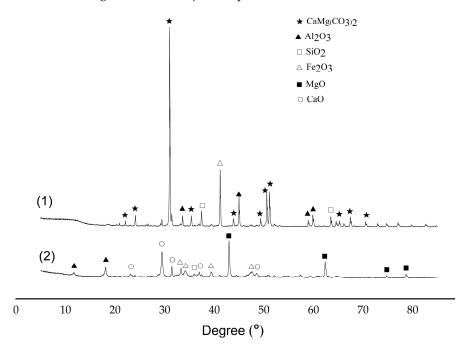


Figure 6. XRD patterns of dolomite (1) and calcined dolomite (2).

Table 3. The surface characterization of dolomite and calcined dolomite.

Samples	BET Surface Area (m <sup>2</sup> /g)	Micropore Surface Area (m <sup>2</sup> /g)	External Surface Area (m <sup>2</sup> /g)	Pore Volume (cm <sup>2</sup> /g)
Dolomite	0.32	0.14	0.31	0.07
Calcined dolomite	9.97	1.75	8.24	2.28

		,	,			
Catalyst	CaO	MgO	SiO <sub>2</sub>	Fe <sub>2</sub> O <sub>3</sub>	$Al_2O_3$	Na <sub>2</sub> O
Calcined dolomite	53.2	38.7	2.97	0.71	0.83	0.76

## Table 4. Chemical analysis of calcined dolomite (wt%).

#### 3.3. Experimental Apparatus and Procedures

A self-designed two-stage catalytic pyrolysis reactor was used for catalytic pyrolysis experiments in our study. It was mainly composed of a two-stage screw feeder, a horizontal electric furnace, a temperature control system, a two-stage catalytic pyrolysis reactor (pyrolysis bed and catalytic reforming bed), and a gas cleaning and tar collecting system. The schematic diagram of the apparatus is shown in Figure 7.

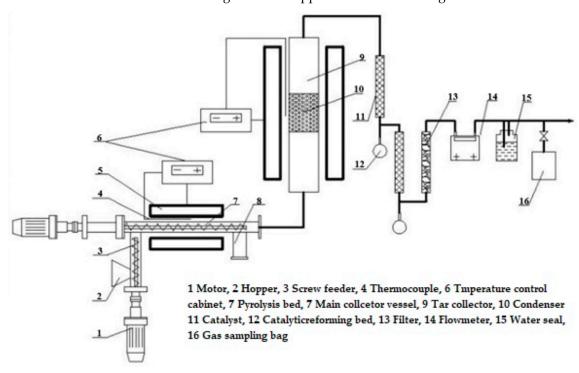


Figure 7. Schematic diagram of the two-stage catalytic pyrolysis reactor.

The two-stage screw feeder system consisted of two screw feeders. The screw feeder mainly included the screw, motor and hopper. The motor drove the rotation of the screw and then pushed the raw material forward. The primary screw feeder contained a hopper, and its end was connected with the pyrolysis reactor. A short distance was maintained between the screw end and the outlet of the feeder, to achieve a good sealing performance by forming a material seal. According to the cold mode tests, the input mass of the feeder was determined by the speed of the primary screw feeder. The secondary screw feeder was located in the pyrolysis reactor, and its rotational speed determined the biomass moving velocity within the reactor. The relationship between biomass moving velocity and the speed of the secondary screw feeder was measured by the cold mode experiment, which is shown in Figure 8.

The electric horizontal pyrolysis bed reactor with electric heating was used in this study. The horizontal pyrolysis bed reactor mainly consisted of a motor, screw feeder and ash hopper. The reactor was made of high-temperature-resistant stainless steel. The highest temperature of the reactor can reach up to 1000 °C, the size of the internal reaction tube was  $\varphi$  80 × 1100 mm. The motor drove the rotation of the screw so that the biomass samples from the primary screw feeder moved forward and reacted in the pyrolysis reactor. Finally, the solid residue generated by the pyrolysis reactions fell into the ash hopper. An electric vertical tube reactor was used as the catalytic reforming bed. The reactor was made of high temperature of

1000 °C, with an internal size of  $\phi$  60 × 1100 mm. It was filled with the catalyst inside and had a gas outlet on the top.

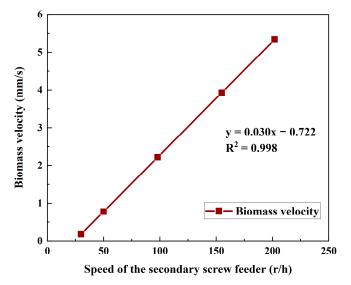


Figure 8. The relationship between biomass velocity and speed of the secondary screw feeder.

In the catalytic pyrolysis experiments, the pyrolysis bed and catalytic reforming bed were preheated, and around 300 g pine sawdust was set in the hopper. When the two reactors were heated to the required temperature, N<sub>2</sub> was introduced for approximately half an hour to drain the oxygen from the system. After that, the two-stage screw feeder started feeding, under the primary feeding speed of 171 r/h and the secondary feeding speed of 300 r/h. The pyrolysis reactions of the pine sawdust took place in the pyrolysis bed at 700–900 °C. Then, the pyrolysis gas was inputted to the catalytic reforming reactor through the pipeline, and further cracked and reformed under the action of the catalyst. In the downstream, when the reformed gas passed the condensers under the ice water (~0 °C), most of the tar was condensed and collected by the collection impingers. The residual tar and impurities were absorbed and removed by the filters with the quartz cotton. The output gas flow rate was recorded by the gas flowmeter. Finally, the gas passed through the water-sealed bottle and was then ignited and exhausted.

After the experiment ran around 15 min under a steady-state, the generated gas was collected by a gas sampling bag and analyzed by gas chromatography (GC 9800 T, Kechuang, Shanghai, China). The gas yield was counted by the gas flowmeter. After the experiment, the collected tar from the collection bottles was weighted. Solid residues were collected from the ash hopper for weighing and analysis. Each experiment was repeated three times, and the results were averaged and presented.

#### 3.4. Data Analysis

1. Dry gas yield,  $G_Y$  (Nm<sup>3</sup>/kg), refers to the volume of gas that can be generated per kilogram of dried biomass, which was calculated by the following equation:

$$G_{\rm Y}$$
 = Produced gas volume (Nm<sup>3</sup>) ÷ Dry biomass weight (kg) (5)

2. Carbon conversion rate,  $\eta_c$  (%), refers to the ratio of carbon content in gas products to the carbon content in biomass, which was calculated by the following equation:

$$\eta_{c} = \frac{CO + CO_{2} + CH_{4} + 2 \times C_{n}H_{m}}{22.4 \times C} \times 12G_{Y} \times 100\%$$
(6)

where C means the mass percentage of carbon in the ultimate analysis of samples,  $G_Y$  is the dry gas yield, CO, CO<sub>2</sub>, CH<sub>4</sub>, C<sub>n</sub>H<sub>m</sub> are the volume ratio of CO, CO<sub>2</sub>, CH<sub>4</sub> and hydrocarbons in gas products.

3. The low heating value of gas products (LHV, kJ/Nm<sup>3</sup>) was calculated by the following equation:

$$LHV = (CO \times 30.0 + H_2 \times 25.7 + CH_4 \times 85.4 + C_n H_m \times 151.3) \times 4.2$$
(7)

where CO,  $H_2$ ,  $CH_4$  and  $C_nH_m$ , respectively, are their corresponding gas composition by volume in gas products.

#### 4. Conclusions

In a two-stage catalytic pyrolysis reactor, the effects of pyrolysis temperature and catalytic temperature on catalytic pyrolysis performance of pine sawdust with calcined dolomite were studied. The main conclusions were summarized as follows:

- 1. High pyrolysis temperature improved gas yield by thermal cracking of solid and liquid products.
- 2. The CO, CH<sub>4</sub> and CO<sub>2</sub> contents in gas decreased with the increase in temperature.  $H_2/CO$ , dry gas yield and carbon conversion rates all increased with the growth in temperature. The heating value of gas products reached a maximum value of 13.43 MJ/Nm<sup>3</sup> at 850 °C.
- 3. Calcined dolomite had good catalytic activity for biomass pyrolysis, which could increase the tar removing capability and syngas yield by 44.64% and by 52.92%, respectively.
- 4. The increasing catalytic temperature could increase  $H_2$  and CO content in pyrolysis gas. In addition, increasing catalytic temperature also significantly improved  $H_2/CO$  ratio, dry gas yield, carbon conversion and heating value.

However, the deactivation of the catalyst during the pyrolysis was not examined in this study, which will be further investigated in future work. Moreover, the number of catalysts used in this study was insufficient. Further investigation should be undertaken using more other natural ores catalysts for the optimum catalytic pyrolysis performance.

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