



Article Unravelling the Impacts of Climate Variability on Surface Runoff in the Mouhoun River Catchment (West Africa)

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Abstract: This study assesses the impacts of climate variability on surface runoff generation in the Mouhoun River Catchment (MRC) in Burkina Faso, in the West African Sahel. The study uses a combination of observed and reanalysis data over the period 1983–2018 to develop a SWAT model (KGE = 0.77/0.89 in calibration/validation) further used to reconstitute the complete time series for surface runoff. Results show that annual rainfall and surface runoff follow a significant upward trend (rainfall: 4.98 mm·year⁻¹, *p*-value = 0.029; runoff: 0.45 m³·s⁻¹·year⁻¹, *p*-value = 0.013). Also, rainfall appears to be the dominant driver of surface runoff (Spearman's $\rho = 0.732$, *p*-value < 0.0001), leading surface runoff at all timescales. Surface runoff is further modulated by potential evapotranspiration with quasi-decadal timescales fluctuations, although being less correlated to surface runoff (Spearman's $\rho = -0.148$, *p*-value = 0.386). The study highlights the added value of the coupling of hydrological modeling and reanalysis datasets to analyze the rainfall–runoff relationship in data-scarce and poorly gauged environments and therefore raises pathways to improve knowledge and understanding of the impacts of climate variability in Sahelian hydrosystems.

Keywords: climate variability; hydrological response; Mouhoun River Catchment; surface runoff; SWAT model; West African Sahel

1. Introduction

Water is generally regarded as a fundamental natural resource underpinning economic and social development trajectories. This is particularly underscored by its inclusion in the Sustainable Development Goals (SDGs), which envision the universal access and the sustainable management of water resources by the year 2030. Yet, over the past few decades, numerous countries worldwide, notably those in semi-arid and arid regions, have grappled with an escalating series of water shortage issues, further heightened by the recent global climate crisis [1–5].

Extensive investigations in previous studies [2,6] have unveiled a disquieting portrait of climate change, characterized by substantial and significant changes in precipitation, increasing temperatures and water losses through evapotranspiration in West Africa. Moreover, the increase in hydrometeorological extremes, ranging from inundating floods to severe droughts and so-called compound risks, is consistently being reported [7–9]. In the Sahelian context, where rivers are the predominant water supply source while being primarily driven by rainfall, the impacts of climate change are alarming and therefore call for urgent assessment of appropriate management strategies [3,10–15].



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Burkina Faso, like many other Sahelian countries, is peculiarly exposed to the repercussions of climate change. This vulnerability arises from the heavy reliance on water resources to sustain vital sectors such as agriculture and livestock husbandry and the indispensable provision of potable water to local populations [2,3,16,17]. Within the Mouhoun River Catchment (MRC), located in the south-western region of the country, 14,900 km² in size, the situation is further compounded by the escalating impact of climate change on water resources [18,19]. The MRC is of specific importance in Burkina Faso for several reasons: in terms of water supply, the Mouhoun River is the largest in Burkina Faso, and the catchment provides drinking water (to over 10 million people), irrigation (over 200,000 ha), and livestock. It is used to generate hydropower, which provides almost 20% of the country's electricity needs. The MRC is also a major agricultural region, home to over 50% of the agricultural lands in the country and producing crops such as cotton, rice, and sorghum. Additionally, it is home to a variety of plant and animal life estimated at 1000 species, including some endangered species [18]. In addition to its importance to Burkina Faso, the MRC is also transboundary to neighbouring countries, such as Mali and Niger, therefore providing water and associated ecosystem services to their populations [18,20–24].

The MRC is already grappling with pronounced climatic fluctuations, including drought spells and episodes of extreme rainfall, affecting water provision to local populations [21–24]. Yet, the context is also depicted by the lack of long-term and consistent climate and hydrology data records, rarely gap-free, since gauging equipment is seldom and poorly maintained [15,19,23,25]. This further hinders the understanding of the rainfall–runoff relationship, the assessment of the available water resource, and the development of well-informed and adapted water management policies.

In this study, we aim to contribute to understanding the impacts of climate variability as a driver of surface runoff generation mechanisms in the MRC in Burkina Faso. In this regard, the study makes use of the agro-eco-hydrological Soil and Water Assessment Tool (SWAT) model [26,27], which has been extensively used in previous studies in various contexts in the study area, mostly because of its relative ability to accommodate data-scarce environments and its robustness in simulating the hydrological cycle [14,15,28–31]. The study focuses on the previous 1983–2018 period, upon which observation records for hydrometeorological variables are relatively abundant and of quality, therefore leveraging the opportunity for hydrological modeling. The objectives of the study are three-fold: (i) to characterize climate variability over the 1983–2018 period in the MRC; (ii) to reconstitute a complete time series for surface runoff in the MRC over the period 1983–2018 through hydrological modeling; and (iii), to analyze the temporal dynamics of surface runoff as affected by climate variables at various timescales.

The study not only proposes valuable insights into the specific challenges faced by the MRC but also offers a methodological contribution that has relevance and applicability in addressing global gaps in understanding climate-driven surface runoff in data-scarce environments globally.

2. Materials and Methods

2.1. Study Area

The MRC is located in the Upper Mouhoun, in the extreme south-western region of the country. The catchment lies within latitudes 10°46′ and 12°32′ North and longitudes 5°21′ and 3°24′ West (Figure 1). The catchment outlet is located at the gauging station of Nowkuy (12°31′ North and 3°33′ West), which drains a total area of 14,900 km², covering the Hauts-Bassins and Boucle du Mouhoun regions. The MRC is highly anthropized and the dominant land use/land cover (LULC) type consists of hydro-agricultural developments [18].



Figure 1. Location of the Mouhoun River Catchment (MRC) in Burkina Faso, West Africa. Elevation data are provided by FABDEM [32].

The increasing north–south rainfall gradient divides the catchment into three climatic zones: the Sudanian zone (over 900 mm of annual rainfall), the Sudano-Sahelian zone (600–900 mm of annual rainfall), and the Sahelian zone (less than 600 mm of annual rainfall). Rainfall is concentrated in June to September (i.e., four months) with an average cumulative rainfall of 960 mm per year, while the rest of the year (the months of October to May, i.e., 8 months) is characterized by a long dry period. The temperatures are increasing from south to north. On average, the daily temperatures range from 15 °C in December to 40 °C in April [18,25].

From a geological perspective, two geological units are found within the catchment, which are the basement and the sedimentary. The basement is made up of a wide range of rocks, from very acidic (granites) to very basic (amphibolites, greenstone, dolerites). The sedimentary catchment is mainly made of primary and infracambrian formations and clay alluvium of fluvial-lacustrine origin from the terminal continental period. The nature of the topsoil follows closely the geology, geomorphology, and climate patterns, resulting in six major types of soil in the catchment: arenosols, leptosols, lixisols, nitisols, plinthosols, and regosols [33–35]. The catchment is mainly dominated by lixisols, with arenosols representing only a tiny fraction of the catchment [36,37], as shown in Figure 2a.

The vegetation formations in the catchment are essentially composed of wooded savannahs, open forests, and deciduous forest galleries (Figure 2b) mainly concentrating along the Mouhoun River [36]. The dominant slope gradients fall within the 0–2% range, while a smaller portion of the catchment has a terrain slope above 2% (Figure 2c).



Figure 2. Physical characterization of the Mouhoun River Catchment (MRC). (**a**) Soil types. (**b**) Land use/land cover (LULC) types. (**c**) Slope classes, calculated from the FABDEM dataset [32] used in this study.

2.2. Hydroclimatic Data Pre-Processing

2.2.1. Presentation of Data Used in This Study

The following data have been collected for use in this study:

- **Daily discharge data at the Nowkuy station**, obtained from the Water Information Division (DEIE) for the period 1983–2018;
- Meteorological observation data, including daily rainfall, daily maximum and minimum temperature data at the synoptic stations at Bobo-Dioulasso (WMO Code: 1200004000, Latitude: 11.1667° North, Longitude: 4.3167° West) and Dédougou (WMO Code: 1200007900, Latitude: 12.4667° North, Longitude: 3.4667° West). The data cover the period 1983–2018 and are provided by the National Meteorology Agency in Burkina Faso (ANAM-BF);
- Meteorological reanalysis data, which includes daily rainfall and daily maximum and minimum temperature data for the period 1983–2018. The data are provided by the *Modern-Era Retrospective Analysis for Research and Applications, Version 2* (MERRA-2 [38]), provided at a spatial resolution of nearly 50 km. The data were downloaded from the NASA Power platform through the *nasapower* R package [39]. The data were extracted at eight (08) locations within the catchment considered as dummy or fictitious stations;
- **Digital elevation data**, collected from the global *Forest And Buildings removed Copernicus Digital Elevation Model* (FABDEM), providing 30 by 30 m resolution elevation data [32,40];
- Soil map, collected from the Food and Agriculture Organization (FAO) soil database, commonly referred to as the Harmonized World Soil Database (HWSD) version 1.2 [37]. The map was resampled to 30 by 30 m through bilinear interpolation.
- Land use/land cover (LULC) map, taken from the national land use/land cover database inventory in 2012 [36], derived from remote sensing analysis and aerial maps and validated with field surveys at the national scale. The map was also resampled to 30 by 30 m through bilinear interpolation.

2.2.2. Gap-Filling of Observations, Spatial Interpolation, and Bias Correction of Reanalysis Data

The synoptic stations closest to the MRC are the stations of Bobo-Dioulasso and Dédougou. However, relying only on these single locations limits the consideration of the spatial variability of climate variables. Therefore, to increase the density of observation stations within the MRC, we created 8 fictitious (or dummy) stations, evenly spaced in the catchment area, at which daily MERRA-2 reanalysis data were collected over the study

period 1983–2018. The location of these fictitious stations is given in Figure 1. MERRA-2 is a global gridded assimilation model, consistently providing daily estimates for most of the meteorological variables since 1980, with a spatial resolution of nearly 50 km [38]. In Burkina Faso, MERRA-2 has been used in many previous impact studies [15,31,41,42].

However, despite the relatively good accuracy shown by MERRA-2 in reproducing observation data, there are still biases which could be further treated. In this study, we used the daily observation data at the Bobo-Dioulasso and Dédougou synoptic stations to develop bias-correction transfer functions and further adjust MERRA-2 data in the same locations. Then, MERRA-2 data extracted at fictitious stations are bias-adjusted by referring to the bias-correction function of the nearest synoptic station.

The bias-correction approach used in this study is the univariate Cumulative Distribution Function transform (CDFt), which is an extension of the popular quantile mapping method [43,44]. The CDFt method accounts for the changes in CDF from reference to simulated (here, reanalysis) data through the construction of a transfer function, expressed as in Equation (1).

$$F_{D_f}(x) = F_{O_h} \Big(F_{M_h}^{-1} \Big(F_{M_f}(x) \Big) \Big)$$
(1)

where F_{D_f} is the downscaled CDF for bias correction of the univariate distribution of the variable x, F_{O_h} is the CDF of the observed data over the reference period, $F_{M_h}^{-1}$ is the inverse CDF of the simulated (reanalysis) data over the reference period, and F_{M_f} is the CDF of the simulated data over a projection period, which in this case refers to the same historical period. The bias-correction procedure was carried out with the R package *CDFt* [45].

2.2.3. Estimation of Potential Evapotranspiration (PET)

Potential evapotranspiration (PET) is a major component of the water balance, which represents the evaporative water demand in the hydrological system and therefore controls the surface runoff and the water availability [25]. This study estimates daily PET using the Hargreaves and Samani (HS) method [46,47]. The HS method is an empirical approach commonly used to estimate daily PET only from temperature data while accounting for extraterrestrial radiation, hence explaining its popular use in data-scarce environments. Previous studies reported the reliability of the HS equation for PET estimation in Burkina Faso [6,14,15,25,48]. The mathematical expression of the HS method is given in Equation (2):

$$PET = 0.0135 \times k_{RS} \times (Ra/\lambda) \times (T_{max} - T_{min})^n \times (T_m + b)$$
⁽²⁾

where *Ra* is the extraterrestrial radiation (MJ·m⁻²·d⁻¹), λ the latent heat of vaporization (= 2.45 MJ·kg⁻¹), *T_{max}*, *T_{min}*, and *T_m* are the daily maximum and minimum and average temperatures (°C), respectively, and *k_{RS}*, *n*, and *b* are coefficients originally defined as 0.17 (for interior locations), 0.5, and 17.8, respectively [47].

2.3. Hydrological Modeling

2.3.1. Definition of Warm-Up, Calibration, and Validation Periods

For the hydrological modeling step, a warm-up period of two years (1983–1984) is defined. The remaining years are further divided into a calibration and validation period following the standard single split-sampling procedure, with the period 1985–2008 (i.e., 26 years) for model calibration and the period 2009–2018 for validation (i.e., 10 years). Figure 3 shows the distribution of gaps in the daily discharge data, with three years of completely missing observed data: 1989, 1995 (in the calibration period), and 2012 (in the validation period).



Figure 3. Distribution of gaps in the observed dataset of daily discharge at Nowkuy gauging station. The years 1989, 1995, and 2012 are completely missing observed data. The dashed blue lines indicate the limits of the warm-up (1983–1984), calibration (1985–2008), and validation (2009–2018) periods.

2.3.2. The SWAT Model

The Soil and Water Assessment Tool (SWAT) is an agro-eco-hydrological model developed in 1999 by the United States Department of Agriculture (USDA). It is a widely adopted modeling tool for hydrological modeling and the assessment of external stressors on water resources at the watershed scale [26,27]. The SWAT model is physically based and semi-distributed. It operates through the discretization of the watershed into spatially connected sub-catchments through a hydrographic drainage network. The sub-catchments are further sub-divided into hydrologic response units (HRUs), which correspond to lumped homogeneous units in terms of land use, soil type, and slope class. Hydrological processes are evaluated at the scale of HRUs and summed up at the sub-catchment level. The surface runoff is then routed to the watershed global outlet through the channel network. The hydrological balance at the scale of HRUs in the SWAT model is calculated based on Equation (3) [27]:

$$SW_t = SW_0 + \sum_{i=0}^{t} (P_i + Q_{s,i} + ET_i + w_i + Q_{gw,i})$$
(3)

where SW_t and SW_0 are the soil water content and the initial soil water content at the beginning of day *i*, *t* is the elapsed time (in days), P_i is the daily rainfall, $Q_{s,i}$ is the daily surface runoff, ET_i is the daily actual evapotranspiration, w_i is the daily seepage loss entering the vadose zone under the soil profile, and $Q_{gw,i}$ is the return flow from the aquifer. All these quantities are expressed in millimeters (mm). Surface runoff is estimated in this study through the Soil Conservation Service Curve Number (SCS-CN) method [26,27,49], given by Equation (4):

$$Q_{s,i} = (P_i - I_a)^2 / (P_i - I_a + S), \quad S = 245 \times (100/CN - 1)$$
(4)

where I_a (in mm) is the initial abstraction defined as the amount of rainfall interception by plant canopy or to fill in soil surface depression storage, occurring at the onset of a rainfall event, *S* is the soil water retention parameter (in mm), defined as a function of soil, slope, and LULC type, and the *CN* parameter relates to *S*.

The surface runoff obtained at the sub-basin level is transmitted to the watershed outlet using the variable travel time method [26,27,50] and converted to discharge.

2.3.3. Selection of Model Parameters

In this study, based on a screening of previous SWAT model applications in the West African Sahel [14,15,28–31,51], a set of 28 model parameters are selected for sensitivity analysis. Table 1 provides the definition, update mode, and range for the different parameters. Overall, 1 parameter affects the surface runoff generation mechanism, 14 parameters control runoff routing, 10 parameters control infiltration and groundwater recharge, and 3 parameters control soil surface hydraulic properties [27].

| Parameter Name | Description | Initial Range | Unit | | | |
|---|--|---------------|-----------------------------------|--|--|--|
| Soil management, runoff generation parameters (1) | | | | | | |
| CN2 | SCS runoff curve number | 35–98 | - | | | |
| Groundwater control parameters (10) | | | | | | |
| ALPHA_BF | Baseflow alpha factor | 0–1 | $\rm days^{-1}$ | | | |
| GW_DELAY | Groundwater delay | 0-500 | days | | | |
| SHALLST | Initial depth of water in the shallow aquifer | 0–50,000 | mm | | | |
| DEEPST | Initial depth of water in the deep aquifer | 0–50,000 | mm | | | |
| GWQMN | Depth of water (in the shallow aquifer) triggering return flow | 0-5000 | mm | | | |
| GW_REVAP | Groundwater re-evaporation coefficient | 0.02-0.20 | - | | | |
| REVAPMN | Water depth (in the shallow aquifer) triggering re-evaporation | 0-500 | mm | | | |
| RCHRG_DP | Deep aquifer percolation fraction | 0–1 | - | | | |
| GWHT | Initial groundwater height | 0–25 | m | | | |
| GW_SPYLD | Specific yield of the shallow aquifer | 0.0-0.4 | $\mathrm{m}^3~\mathrm{m}^{-3}$ | | | |
| Soil parameters (3) | | | | | | |
| SOL_Z | Depth from the soil surface to the bottom of the layer | 0-3500 | mm | | | |
| SOL_AWC | Available water capacity of the soil layer | 0–1 | ${ m mm}{ m \cdot m}^{-1}$ | | | |
| SOL_K | Saturated hydraulic conductivity | 0-2000 | ${ m mm}~{ m h}^{-1}$ | | | |
| Channel and flow routing parameters (14) | | | | | | |
| CH_N2 | Manning's roughness for the main channel | 0.01–0.3 | $s \cdot m^{-1/3}$ | | | |
| CH_K2 | Effective hydraulic conductivity in main channel alluvium | 0.01-500 | $\mathrm{mm}\cdot\mathrm{h}^{-1}$ | | | |
| ALPHA_BNK | Baseflow alpha factor for bank storage | 0–1 | days | | | |
| CH_N1 | Manning's roughness for tributary channels | 0.01-30 | $s \cdot m^{-1/3}$ | | | |
| CH_K1 | Effective hydraulic conductivity in tributary channel alluvium | 0-300 | $\mathrm{mm}\cdot\mathrm{h}^{-1}$ | | | |
| OV_N | Manning's roughness for overland flow | 0.01-30 | $s \cdot m^{-1/3}$ | | | |
| LAT_TTIME | Lateral flow travel time | 0-180 | days | | | |
| CANMX | Maximum canopy storage | 0-100 | mm | | | |
| ESCO | Soil evaporation compensation factor | 0–1 | - | | | |
| EPCO | Plant uptake compensation factor | 0–1 | - | | | |
| MSK_CO1 | Storage time constant for normal flow | 0-10 | - | | | |
| MSK_CO2 | Storage time constant for low flow | 0–10 | - | | | |
| MSK_X | Inflow/outflow rate in reach segment control weighting | 0-0.3 | - | | | |
| TRNSRCH | Loss fraction from the main channel entering the deep aquifer | 0–1 | - | | | |

Table 1. SWAT Model parameters were selected for global sensitivity analysis in this study.

The model parameter description is provided by [27,52].

2.3.4. Sensitivity Analysis

The global sensitivity analysis (GSA) procedure is used to assess the sensitivity of surface runoff to each of the considered model parameters while accounting for the possible interaction with the others [52]. The parameter sensitivities are determined through multiple regression of Latin hypercube sampling of parameters against an objective function, followed by a Student *t*-test to identify the relative significance of each parameter. In this study, the level of significance of 5% was initially applied and 500 simulations were run. The GSA procedure was carried out using the SWAT-CUP (Calibration Uncertainty Program) software, version 5.1.6.2 [52]. However, some parameters above the 5% signifi-

cance level were later found to be useful since they were critical for the proper adjustment of specific processes, such as groundwater flow or surface channel routing. Therefore, these parameters were included in the calibration step which, definitively, used a total of 15 parameters.

2.3.5. Calibration, Validation, and Evaluation of Model Performance

The model calibration over the period 1985–2008 is carried out under the SWAT-CUP calibration software using the Sequential Uncertainty Fitting (SUFI-2) algorithm, with Latin Hypercube sampling for the generation of random sets of parameters at each simulation [52]. The objective function used in this study is the Kling–Gupta Efficiency (KGE) metric [53], defined as in Equation (5):

$$KGE = 1 - \sqrt{(r-1)^2 + (\mu_s/\mu_0 - 1)^2 + (CV_s/CV_0 - 1)^2}$$
(5)

where *r* is the product-moment Pearson's correlation coefficient between observed and simulated values, μ_s/μ_0 is the ratio of the averages of simulated and observed values, and CV_s/CV_0 is the ratio of coefficients of variations of simulated and observed values. The KGE is bounded and ranges between $-\infty$ (poor performance) and 1 (perfect model). The KGE as an objective function is advantageous in that it simultaneously optimizes correlation, bias, and variability. The performance of a hydrological model operating at the daily timestep is considered poor if $0.00 \le \text{KGE} \le 0.50$, satisfactory when $0.50 \le \text{KGE} \le 0.75$, good when $0.75 \le \text{KGE} \le 0.90$, and excellent when $0.90 \le \text{KGE} \le 1.00$ [14,53,54].

Additionally, we used some other criteria to assess the model performance, namely the coefficient of determination (R², Equation (6)), the Nash–Sutcliffe Efficiency (NSE, Equation (7)), the percentage of bias (PBIAS, Equation (8)), the *r_factor* (Equation (9)), and *p_factor*. R² refers to the amount of variation in observations explained by the model and is bounded within 0 (poor model) and 1 (perfect model). The NSE is a popular predictive skill measure, bounded between $-\infty$ (poor model) and 1 (perfect model), which determines the relative magnitude of the residual of simulated variance as compared to the observed data variance. PBIAS shows the average tendency of the model to underestimate (PBIAS > 0) or overestimate (PBIAS < 0) observations, the optimal value being 0. The *r_factor* measures the thickness of the 95% uncertainty prediction band (95PPU) around the simulated value, while the *p_factor* represents the percentage of observations which fall within the 95PPU envelope. Guidelines suggest satisfactory watershed-scale model performance at the daily timestep when R² > 0.60, NSE > 0.50, PBIAS $\leq \pm 15\%$ (Moriasi et al., 2015) and *r_factor* < 1.50, *p_factor* > 0.70 [55–57].

$$R^{2} = \frac{\left[\sum_{i} \left(Q_{o,i} - \overline{Q}_{o}\right) \times \left(Q_{s,i} - \overline{Q}_{s}\right)\right]^{2}}{\sum_{i} \left(Q_{o,i} - \overline{Q}_{o}\right)^{2} \times \sum_{i} \left(Q_{s,i} - \overline{Q}_{s}\right)^{2}}$$
(6)

$$NSE = 1 - \frac{\sum_{i} (Q_o - Q_s)_i^2}{\sum_{i} (Q_{o,i} - \overline{Q}_o)^2}$$
(7)

$$PBIAS = \frac{\sum_{i} (Q_o - Q_s)_i}{\sum_{i} Q_{o,i}} \times 100$$
(8)

$$r_{factor} = \frac{1}{n} \times \frac{\sum_{i=1}^{n} \left(Q_{s,i}^{97.5\%} - Q_{s,i}^{2.5\%} \right)}{\sigma_0}$$
(9)

where $Q_{o,i}$ and $Q_{s,i}$ refer to the observed and simulated discharges on day *i*, \overline{Q}_o and \overline{Q}_s are the average of observed and simulated values, $Q_{s,i}^{97.5\%}$ and $Q_{s,i}^{2.5\%}$ are the higher and lower limits (respectively) of the 95PPU band on day i across all simulations. In this study, a total of 5 iterations of 500 simulations each were needed to reach optimal results. The model validation over the period 2009–2018 is carried out through a single

iteration of 500 simulations following the guidelines in [52]. The model performance is also evaluated using the same performance metrics. Also, a graphical evaluation of the simulated discharges is carried out using time series plots and flow duration curve plots.

2.4. Analysis of Hydrological Response to Climate Variability

2.4.1. Annual Trends and Correlation Analyses in P, PET, and Q

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The trends in annual P, PET, and simulated Q values are evaluated using the nonparametric Mann–Kendall (M-K) trend test at a 5% significance level [58,59]. To account for autocorrelation, which is often present in hydrometeorological time series, a modified version of the M-K test including a trend-free serial correlation prewhitening correction [60] is applied using the *tfpwmk* function in the *modifiedmk* R package [61]. The magnitude of trend slopes is evaluated using the non-parametric Theil–Sen slope estimator, as given in Equation (10).

$$\beta = Median\left(\frac{x_j - x_i}{j - i}\right), \ \forall i < j \tag{10}$$

where x_i and x_j are sequential values in a time series at times *i* and *j*, respectively, β is a robust unbiased estimate of the trend slope magnitude [62,63]. To further assess the level of association between P and Q and PET and Q, the non-parametric Spearman's correlation test at a 5% significance level is applied [64].

2.4.2. Sensitivity of Surface Runoff to P, PET, and Environmental Conditions (n)

To further explore how surface runoff is sensitive to P, PET, and environmental conditions (n), we used the concept of elasticity [65], as shown in the total differential Equation (11):

$$dQ = \varepsilon_P^Q \frac{dP}{P} + \varepsilon_{PET}^Q \frac{dPET}{PET} + \varepsilon_n^Q \frac{dn}{n}$$
(11)

where ε_P^Q , ε_{PET}^Q , and ε_n^Q are *P*, *PET*, and *n* elasticities to surface runoff (*Q*), assuming that these variables are independent [66,67]. These elasticities are expressed as in Equation (12):

$$\varepsilon_P^Q = \frac{\partial Q/Q}{\partial P/P}, \ \varepsilon_{PET}^Q = \frac{\partial Q/Q}{\partial PET/PET} \ and \ \varepsilon_n^Q = \frac{\partial Q/Q}{\partial n/n}$$
 (12)

The elastic coefficients were therefore determined in this study from the linear regression between the partial derivatives. For a given variable, the higher the value of its elastic coefficient is, the more sensitive surface runoff is to the variable. In other terms, the elastic coefficient represents the rate of change in surface runoff for a 1% increase in a given causing variable.

Following [31,66,67], the environmental conditions parameter (n), representing the soil surface conditions characteristics, is determined for each year by solving a simplified Budyko–Mezentsev–Choudhury–Yang model [68–70], as given in Equation (13):

$$Q = P - \frac{P \times PET}{\left(P^n + PET^n\right)^{1/n}} \tag{13}$$

2.4.3. Modes of Variability in P, PET, and Q

To investigate the variability in P, PET, and Q at various timescales (annual, decadal, and above) over the analysis period and investigate how short- to longer-term fluctuations in P and PET are further propagated to surface runoff, we use a continuous wavelet transform (CWT). The process entails the use of a non-orthogonal Morlet mother wavelet of order 6 to generate local wavelet spectra. Morlet wavelets are suitable for such transformations as they offer a good balance between time and frequency localization, therefore giving a good definition of the signal in the spectral space [71]. These wavelet spectra, in turn, enable us to discern the prevailing timescales of variability and their temporal progression [5,14,72,73].

The statistical significance of wavelet power can be assessed relative to the null hypotheses that the signal is generated by a stationary process with a given background power spectrum [71]. In this research, we calculated the CWTs for P, PET, and Q time series at a 10% significance level with the *biwavelet* R package [74]. Additionally, wavelet coherence plots were generated using 1000 Monte Carlo randomizations and used to analyze the time-phase correlation between P-Q signals and P-PET signals.

3. Results

3.1. Bias Correction of Meteorological Data over the Study Period 1983–2018

Figure 4 shows the empirical cumulative distribution plots for the meteorological variables analyzed in this study (rainfall, maximum and minimum temperature) over the period 1983–2018 at the synoptic stations of Bobo-Dioulasso and Dédougou between daily observations and MERRA-2 reanalysis estimates. It appears that discrepancies in distribution quantiles occur, especially a severe underestimation of rainfall, because of the so-called drizzle effect [75]. Also, MERRA-2 underestimates the highest values of daily maximum temperatures but underestimates the lowest values of daily minimum temperatures. The mismatch between the observations and reanalysis is adjusted through the CDFt bias-correction method, resulting in similar distributions.



— MERRA-2 (raw) — MERRA-2 (bias corrected) — Observations

Figure 4. Empirical cumulative distribution functions showing bias-correction adjustment through the CDFt method for MERRA-2 reanalysis and observed data. The top panels are for the synoptic station of Bobo-Dioulasso, while the bottom panels are for the station of Dédougou. On each row, panels show, left to right, daily rainfall, maximum temperature (T_{max}), and minimum temperature (T_{min}) over the period 1983–2018.

The bias-correction transfer functions established are further used to adjust MERRA-2 estimates at the fictitious weather stations within the watershed, based on the proximity to the synoptic stations.

3.2. Modeling the Surface Runoff Response

3.2.1. Parameter Sensitivity

The model parameters retained through the GSA analysis procedure screening, their optimal fitted values, and uncertainty ranges are presented in Table 2.

| Sensitivity Rank | Parameter | Fitted Value | Uncertainty Range |
|------------------|----------------|--------------|----------------------|
| 1 | rCN2 | 0.265 | [0.1010.464] |
| 2 | vGW_DELAY | 56.649 | [0.000112.623] |
| 3 | v_GWQMN | 1833.929 | [33.2102110.164] |
| 4 | $v_SHALLST$ | 14,511.832 | [13441.77130983.770] |
| 5 | v_GW_REVAP | 0.195 | [0.1430.196] |
| 6 | vGWHT | 6.017 | [3.2309.695] |
| 7 | v_GW_SPYLD | 0.117 | [0.0870.195] |
| 8 | r_SOL_AWC | -0.841 | [-0.8910.293] |
| 9 | <i>v</i> CH_N2 | 0.173 | [0.0050.218] |
| 10 | <i>v</i> CH_K2 | 374.704 | [289.448452.462] |
| 11 | vALPHA_BNK | 0.799 | [0.5090.846] |
| 12 | <i>v</i> CH_K1 | 154.571 | [100.138162.205] |
| 13 | vEPCO | 0.359 | [0.0360.372] |
| 14 | r_MSK_CO1 | -0.661 | [-0.6900.368] |
| 15 | v_TRNSRCH | 0.550 | [0.4220.597] |

Table 2. Model parameters' sensitivity ranking, fitted values, and uncertainty ranges.

The prefix before each parameter name describes how the parameter is updated during the calibration process in SWAT-CUP: the relative mode (r_{-}), in which the current value of the parameter is multiplied at each simulation by 1 + x, x being the given value; the value mode (v_{-}), in which the current value of the parameter is replaced by a new value taken in a given interval. The uncertainty range around each parameter defines the uncertainty band (95PPU) around the simulated values [52]. The 15 parameters are ranked out in a decreasing order of global sensitivity, ranging from 1 (more sensitive) to 13 (less sensitive).

The most sensitive parameter is CN2, which controls surface runoff generation, highlighting that soil surface conditions are quite deterministic in surface runoff production in the MRC, as picture in the calibrated SWAT model. Following are the GW_DELAY, GWQMN, SHALLST, GW_REVAP, GWHT, and GW_SPYLD parameters which control groundwater processes, further suggesting that according to the model, groundwater/surface water interactions are important in the MRC. This finding seems accurate since the Mouhoun River is permanent throughout the year, with a low-flow period probably sustained by groundwater. Next, soil hydraulic properties (SAL_AWC) and runoff routing parameters (CH_N2, CH_K2, ALPHA_BNK, CH_K1, EPCO, MSK_CO1, and TRNSRCH) appear to be effective for model adjustment, which could be related to the elongated shape of the catchment, suggesting that surface runoff transfer time is important in explaining discharge values at Nowkuy outlet downstream.

3.2.2. Model Calibration and Validation

The model performance on both calibration and validation periods is evaluated according to performance metrics presented in Table 3. The calibrated model shows satisfactory performance in the period 1983–2008, which is further superior during the validation period, probably because this latter period is shorter. Nevertheless, it appears that the model is successful at simulating surface runoff in the MRC. The average value of the observed daily discharge is $31.94 \pm 32.27 \text{ m}^3 \cdot \text{s}^{-1}$ ($45.41 \pm 29.78 \text{ m}^3 \cdot \text{s}^{-1}$), while the simulated value average is $32.59 \pm 29.23 \text{ m}^3 \cdot \text{s}^{-1}$ ($47.43 \pm 28.59 \text{ m}^3 \cdot \text{s}^{-1}$), respectively, on the calibration and validation periods. It should also be noted that the *r_factor* and *p_factor* on both calibration and validation periods are optimal, meaning that the uncertainty 95PPU band around the simulated values is not significantly larger than the variability in observations and that a significant portion of those observations are captured within this envelope [52,55].

| Performance Metric | Calibration (1983–2008) | Validation (2009–2018) |
|--|----------------------------|----------------------------|
| Observed/simulated mean Q ($m^3 \cdot s^{-1}$) Observed/simulated standard deviation Q ($m^3 \cdot s^{-1}$) | 31.94/32.59 32.27/29.23 | 45.41/47.43 29.78/28.59 |
| KGE (objective function) | 0.77 | 0.89 |
| R ² | 0.63 | 0.82 |
| NSE | 0.54 | 0.80 |
| PBIAS | 2.00% | 4.30% |
| r_factor | 1.43 | 1.27 |
| p_factor | 0.83 | 0.89 |

Table 3. Model performance on calibration and validation periods.

Figure 5 shows the time series of daily simulations over the study period 1983–2018, which further highlights the model performance at reproducing observed patterns in streamflow.



Figure 5. Observed and simulated discharge of the calibrated SWAT model in the MRC over the period 1983–2018. (a) Daily time series. (b) Daily average annual observed and simulated discharge over the calibration period. (c) Daily average annual observed and simulated discharge over the validation period. The green band shows the 95PPU envelope around simulated values.

Figure 6 shows the Flow Duration Curve (FDC) for simulated and observed daily discharges, over the period 1983–2018, which shows that the model overall reproduces well the quantile distribution of daily values. However, it could be further noted that the high flows (having the lowest exceedance probabilities, <40%) are overestimated, while low flows (having the highest exceedance probabilities, >60%) are underestimated.



Figure 6. Observed and simulated flow duration curves (FDCs) in the MRC over the period 1983–2018.

3.3. Hydrological Balance of the MRC

Table 4 shows the average annual values of the main hydrologic processes in the MRC as represented by the calibrated SWAT model. The average annual rainfall and PET are 952.1 \pm 130.4 mm and 1940.4 \pm 51.1 mm (respectively), of which 199.1 \pm 72.2 mm are converted to surface runoff (i.e., a surface runoff coefficient of 20.91%). The actual evapotranspiration ET is estimated at 459.6 \pm 33.6 mm on an annual average (i.e., 48.27% of the annual rainfall). Also, the average annual groundwater recharge (DEEPAQ) reaches 23.3 \pm 5.6 mm, i.e., 2.44% of the annual rainfall.

Table 4. Average annual values of the hydrological processes simulated in the MRC over the period1983–2018.

| Hydrological Process | Average Annual Values (\pm Standard Deviation) | |
|--|---|--|
| Annual rainfall (P, mm) | 952.1 (±130.4) | |
| Potential evapotranspiration (PET, mm) | 1940.4 (±51.1) | |
| Actual evapotranspiration (ET, mm) | 459.6 (±33.6) | |
| Surface runoff (Q, mm) | 199.1 (±72.2) | |
| Soil water content (SW, mm) | 5.2 (±1.0) | |
| Lateral flow (LATQ, mm) | $0.9~(\pm 0.1)$ | |
| Deep aquifer recharge (DEEPAQ, mm) | 23.3 (±5.6) | |

Figure 7 shows the spatial variation of average annual rainfall, actual evapotranspiration ET, and surface runoff within the catchment. An increasing rainfall gradient (north to south) is observed (Figure 7a). ET follows the same gradient (Figure 7b), indicating that ET is mostly conditioned by available water excess in different sub-catchments in the MRC. The highest annual surface runoff amounts (Figure 7c) are generated in the north-western sub-catchments followed by the southernmost sub-catchments, where soil surface conditions are mostly barren or degraded and less natural vegetation is found, indicating that the rainfall–runoff generation is sensitive to soil surface conditions in the MRC.



Figure 7. Spatial variation of average annual values for: (**a**) Rainfall; (**b**) ET; (**c**) Surface runoff in the Mouhoun River Catchment (MRC) over the period 1983–2018.

3.4. Effects of Climate Variability on Surface Runoff

3.4.1. Correlation and Trends

The Spearman rank correlation analysis reveals that at the annual scale, rainfall is significantly and positively correlated with surface runoff ($\rho = 0.732$, *p*-value < 0.0001). On the other hand, PET shows a negative association with surface runoff, although not statistically significant ($\rho = -0.148$, *p*-value = 0.386). This could further be explained by the fact that evapotranspiration is a latent hydrological process, mostly active during dry periods between successive rainfall events, while rainfall is the major process providing entering flux in the hydrological system and responsible for the onset of surface runoff.

The trends in annual rainfall, ET, and surface runoff are presented in Figure 8.

The trend in annual rainfall in the MRC is significant (*p*-value = 0.029), with an increase of 4.98 mm·year⁻¹ over the period 1983–2018. Annual PET, however, appears to be stationary (*p*-value = 0.307, not significant), with a slope of increase of about 1.55 mm·year⁻¹. Annual surface runoff shows a significant increasing trend of 0.45 m³ s⁻¹·year⁻¹ (*p*-value = 0.013), largely caused by the trend observed in rainfall over the study period.

Figure 9 further highlights the patterns of increase in surface runoff over successive decades, from the 1980s to 2010s on both monthly averages (Figure 9a) and flow duration curves (Figure 9b). A decrease is observed from the 1980s to the 1990s, then an increase in average monthly surface runoff and high-to-median quantiles is observed from the 1990s onwards. This also highlights implications for the sizing of future hydraulic infrastructures, especially check dams [8].

3.4.2. Elasticity of P, PET, and Environmental Conditions in the MRC

Figure 10 shows the elasticities of P, PET, and environmental conditions to surface runoff in the MRC.

The analysis shows that surface runoff is highly sensitive to rainfall ($\mathbb{R}^2 = 0.54$), as given by the elastic coefficient ε_P^Q of 2.002, suggesting that an increase of 1% in the annual rainfall results in an increase of 2% in annual surface runoff. Also, surface runoff is less sensitive to PET, with an elasticity ε_{PET}^Q of -1.804, suggesting that an increase in annual PET results in drier catchment conditions, causing a decrease in annual surface runoff. Finally, surface runoff is also less sensitive to environmental conditions, with an elasticity ε_{PET}^n of 0.270, which outlines that the catchment evolution tends towards an increase in annual surface runoff. Also, it should be noted that the sensitivities of surface runoff to PET and environmental conditions are not significant ($\mathbb{R}^2 = 0.022$ and 0.012, respectively).



Figure 8. Annual trend analysis using the modified Mann–Kendall test (at 5% significance level) in the MRC. (a) Annual rainfall. (b) Annual PET. (c) Annual discharge.



Figure 9. Decadal changes in surface runoff over the 1983–2018 period in the MRC. (**a**) Decadal changes in average monthly discharges. (**b**) Decadal changes in interannual Flow Duration Curves (FDCs).



Figure 10. Elastic coefficients of rainfall (in (**a**)), PET (in (**b**)), and environmental conditions (in (**c**)) to surface runoff in the MRC over the period 1983–2018 in the MRC.

3.4.3. Modes of Variability in P, PET, and Surface Runoff

Figure 11 shows the modes of variability in rainfall, PET and surface runoff, as depicted by wavelet power spectra shown in Figure 10d–f. The annual rainfall wavelet power spectrum shows high and significant fluctuations in 2007–2012 in the 2–4-year band (Figure 10d). The annual PET wavelet power spectrum shows a hint of significant fluctuations in 1997–1998 and in 2010 in the 2–4-year band and strong quasi-decadal significant fluctuation in 1997–2008 in the 4–8-year band (Figure 10e). The annual surface runoff wavelet power spectrum shows only significant fluctuations in 2010–2012 in the 2–4-year band (Figure 10f), which appears to be related to rainfall fluctuations at the same timescale, although being further modulated by external factors, probably catchment properties [14,73].



Figure 11. Modes of variability in rainfall, PET, and surface runoff over the period 1983–2018 in the MRC. (**a**–**c**) show the standardized values of rainfall, PET, and runoff, respectively. (**d**–**f**) show the continuous wavelet power spectra of rainfall, PET, and runoff, respectively. The thick black contour lines delimit the cone of influence (COI) outside which edge effects distort the signal and, therefore, are not considered in the analysis. Within the COI, significant fluctuations at a 10% level against red noise are outlined in thick black contour lines [14,72–74].

Figure 12 further investigates the multiscale phase–antiphase relationship between rainfall and surface runoff and between PET and surface runoff through the analysis of

wavelet coherence transform (WCT). The arrows indicate the phase relationship between the two variables: arrows point to the right (left) when the time series are in phase (antiphase) or when they are positively (negatively) correlated. Also, arrows pointing up mean that the first variable leads the second by 90°, whereas arrows pointing down indicate that the second variable leads the first by 90° [5,73,74]. In Figure 11a, continuously over the 1983–2018 period in the 2–16-year band, the phase relationship reveals that rainfall is the primary driver of surface runoff at all timescales, with the two series being in phase (highly correlated). In Figure 11b, it appears that PET is significantly in phase from 2003–2012 with surface runoff, however, being led by 90° in the 2–4-year band. Also, a significant quasi-decadal zero-phase from 1993–2007 is observed, indicating that the two variables move together over this sub-period.



Figure 12. Wavelet coherence over the period 1983–2018 in the MRC for (**a**) rainfall–surface runoff (P-Q) relationship and (**b**) PET–surface runoff (PET-Q) relationship. The thick black contour lines delimit the cone of influence (COI) outside which edge effects distort the signal and, therefore, are not considered in the analysis. Within the COI, significant fluctuations at a 10% level against red noise are outlined in thick black contour lines. Arrow line orientation indicates the phase relationship between the variables: pointing to the right indicates in-phase (0°) relationship, pointing to the left is out of phase (180°) relationship; pointing upward (downward) indicate that Q is led (Q is leading) by 90° the other variable. Overall, it appears that rainfall is the primary driver of surface runoff, at small to quasi-decadal timescales, and is leading surface runoff [76,77]. However, at quasi-decadal timescales, part of the variability in surface runoff is explained by PET. Finally, a significant portion of the variability in surface runoff remains unexplained by rainfall and PET, indicating that external factors, most likely changes in catchment properties (i.e., changes in LULC, [78]), are also affecting surface runoff generation mechanisms in the MRC.

4. Discussion and Conclusions

This study analyzed the impact of climate variability on hydrological processes in the MRC in Burkina Faso, in the West African Sahel, with a focus on surface runoff response. Hydrological modeling is used to reconstitute complete and gap-free records of surface runoff and further analyze the various components of the hydrological balance over the period 1983–2018. Overall, it appears that rainfall is the dominant driver of surface runoff, further modulated to a lesser extent by potential evapotranspiration at a quasi-decadal timescale. Also, the findings suggest that catchment properties may also play a role in the variability of surface runoff remains unexplained by rainfall and PET, and that the evolution in environmental changes tends towards a higher surface runoff potential generation. However, the study did not address the quantification of the isolated contribution of these sources of variation.

The West African Sahel in general is already acknowledged in the literature as one of the regions marked by extreme climate variability, which has profound implications for the regional hydrology [13,18,73,79]. This further explains why populations in the region are particularly vulnerable to climate stress since the water availability is mostly driven by rainfall. Recent climate changes, including erratic rainfall patterns and temperature increases, have created significant challenges for the region's hydrological response. Yet, the hydrology in the region, in terms of quantification, understanding of the processes operating at various timescales and interactions between such processes, and direct and indirect implications on the availability of water resources remain understudied [12]. This further creates severe impediments to the development of well-informed, adapted, and resilient water management policies.

The integration of hydrological modeling, as carried out in this study, coupled with the use of global gridded datasets can help alleviate the knowledge gap [14,31]. These models help researchers and policymakers understand how changes in precipitation and temperature affect water resources and runoff patterns but also soil erosion [80]. In this study, it was shown that the MRC at Nowkuy gauging station is characterized by a significant upward trend in cumulative rainfall and potential evapotranspiration (to a lesser extent), which is further propagated to surface runoff showing an increase over the period 1983–2018. These findings are in line with previous observations [10,11,14,15,81–83], which also highlighted the important role of climate in surface runoff generation, especially in West African environments. In this regard, it should be outlined that the use of the MERRA-2 reanalysis data helped in representing spatial patterns in the rainfall over the catchment, which was certainly critical in attaining optimal model calibration. Therefore, the potential of using reanalysis datasets in hydrological modeling should be further explored as a potential and viable pathway to improve hydrological modeling efforts in data-scarce, poorly gauged, or even ungauged catchments, which are quite common in the West African Sahel [19,42].

Finally, since surface runoff response is acknowledged to be mainly driven by rainfall patterns in the MRC in this study, implications for future water availability should be explored through climate models. Previous studies analyzing the future projections of climate consistently highlight the increase in temperature and, therefore, potential evapotranspiration, but also changes in rainfall patterns, which are likely to result in a decrease in surface water availability [1,2,84]. This has been highlighted in local assessments in the region, especially with the recent launch of the CMIP6 global gridded climate projections [15]. However, in-depth and large-scale studies are essential to bridging the knowledge gap regarding the impacts of climate variability on surface runoff in Burkina Faso and the wider West African Sahel. This will further enable researchers and policymakers to better understand and anticipate the hydrological consequences of climate change, facilitating the development of targeted adaptation strategies to address water resource challenges and enhance resilience in the face of a globally changing climate.

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