

Article

Impact Sound Reduction Performances of Additional Floor Mats for the Retrofitting of an Existing Apartment Building in Accordance with Test-Bed Conditions

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Abstract: Floor mats are commonly used to improve the impact sound performance of existing homes, but actual impact sound reductions do not consistently appear, as they depend on the test-bed conditions used to determine impact sound performance. Therefore, this study evaluated the effects of the environmental conditions of the test bed on the impact sound reduction performances of different floor mats. The Korean industrial standard KS F 2865 specifies the measurement method in the test room and sets the thickness range of the available target floor structure to bare slabs with thicknesses ranging from 120 mm to 210 mm. The evaluation method is ΔL , which is the difference in standardized impact sound levels before and after the installation of the floor finishing material. In this study, a total of eight types of floor mats were tested in four different test beds according to KS F 2865. The impact sources used were tapping, bang machines, and a rubber ball, and we used these sources to consider both light-weight and heavy-weight impact sounds. The results were derived as the impact sound reduction performance for each frequency band and a single-number quantity. The results showed that light impact sound had a similar minimum reduction characteristic of at least 38 dB, regardless of the floor structure on which the mat was installed. However, the heavy-weight impact sound showed different tendencies depending on the floor mat and the characteristics of the floor structure of the test bed when a bang machine and a rubber ball were used. In particular, the reduction achieved by the bang machine showed less than half the tendency of the reduction by the rubber ball, and the tendency of the heavy-weight impact sound was shown to be reducible depending on how the floor mat was maintained, but the reductions differed depending on the test bed. The reductions were larger in the box-type test room than in the real-life-type test room, and among the box-type test rooms, the one with a thicker bare slab showed a relatively larger reduction. In addition, the reliability of the measurement results was evaluated through a correlation analysis between the single-number quantities depending on the thicknesses of the bare slabs of the test beds.

Keywords: floor mats; floor impact sound; apartment buildings; heavy-weight impact sound; light-weight impact sound; bare slab; measurement method



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1. Introduction

In South Korea, the most common complaint from residents in multi-unit housing is floor impact noise from units upstairs and downstairs [1,2]. To address this acoustic problem, various stakeholders, including the government, construction companies, research institutions, and universities, are developing a range of technologies [3–6]. The products and solutions resulting from these research and development efforts are being applied to newly constructed multi-unit housing [7–9]. Furthermore, construction companies use these technological developments as a promotional tool [10–12]. The most active technology developed to solve the problem of floor impact noise is the development of floor structures [13,14]. Currently, developments include hollow slabs and techniques to

increase the thickness and rigidity of the slab beyond the 210 mm bare slab [15–17]. The main development is the installation of resilient structures on top of the bare slab [18]. This involves installing a bare slab, resilient material, light-weight concrete, and a finishing mortar structure. However, there have been recent technological advancements that allow for the thickness and strength of the finishing mortar to be increased, resulting in a single structure of finishing mortar [12]. This type of floor structure is currently being used in multi-unit housing. The materials used for the resilient layer of the floating floor structure have evolved from single structures, such as EPS (Expandable Polystyrene) and EVA (ethylene-vinyl acetate), to composite structures that combine EPS, EVA, and other materials [7,12,19,20]. Additionally, cushioning materials are being developed using a wider range of materials beyond EPS and EVA, and various structures, not just flat types, are being applied for their development [12].

The progress of developing ceiling structures in receiving rooms to reduce noise from floor impacts is also underway [21–26]. This involves using internal acoustic materials to minimize the amplification of impact noises to the room below due to the influence of the air layer within the ceiling and a ceiling-less design to minimize the transmission of impact noises through the ceiling. Furthermore, there have been notable design alterations aimed at minimizing floor impact noises, such as changes in the placement of load-bearing walls and advancements in floor design to manage sound patterns [25]. However, the application of such research and technology appears to be passive and insufficient from the perspective of apartment dwellers [27,28]. Residents of apartments, especially those with young children, are particularly sensitive to the problem of floor impact noise. To address this issue, the most effective solution is to install floor mats of a specific thickness [29–32]. It has been shown that floor mats are typically installed in living rooms and playrooms, and they usually have a minimum thickness of 10 mm and a maximum thickness of 50 mm [33]. Furthermore, the primary outcomes of some studies consist of the outcomes of a survey that asked apartment residents about the measures they take to prevent floor impact noise and the preemptive actions they take [34]. The most frequent response was ‘educating children’, followed by ‘using floor mats or carpets’, and thirdly ‘wearing slippers’. In addition, the government has declared its intention to support apartment residents in purchasing floor mats to reduce floor impact noise by making such purchases interest-free [35]. Thus, apartment residents invest in floor mats to reduce inter-floor noise. However, there is an issue characterized by residents not receiving the expected impact sound reduction performance from the floor mats despite their financial investments.

The Korean standard KS F 2865 provides a method for measuring and evaluating the impact sound reduction performance of floor surface finishing materials and floor mats in South Korea [36]. This standard defines a method for measuring the level of reduction in light-weight and heavy impact sounds achieved by floor surface finishing materials, excluding floating floor layers constructed on a concrete slab in a laboratory. The method is applicable to both single-layer and multi-layer floor finishing materials installed on a standard concrete floor. The scope of the test floor is defined as ‘a reinforced concrete flat plate with a rectangular planform and a thickness of 120 mm to 210 mm’. Some floor mat manufacturers and developers only present the impact sound reduction performance of light-weight impact sound, which is generally high, through the Korean standard code. The evaluation does not include the impact sound reduction performances of a bang machine and rubber ball, which are heavy-weight impact sounds with relatively low impact sound reduction performance. Heavy-weight impact sound is created by simulating the behavior of children in apartment houses, which differs from the purpose of applying floor mats in apartment houses. The impact sound mentioned in the current Korean standard code is different from the impact source generated by children’s behavior. Therefore, even if floor mats are applied, the impact sound reduction performance caused by banging machines and rubber balls is insignificant. Additionally, the impact sound reduction performance of floor mats varies depending on the accuracy of information such as the thickness of the floor structure, as mentioned in the Korean standard code.

On the other hand, the basic application guidelines for evaluating the performance of floor covering products are provided in Annex H of the International Standard ISO 10140-1 [37]. The improvement of impact sound insulation by a floor covering is calculated as the difference between the impact sound pressure levels before and after the installation of the floor covering. The ISO 10140-3 standard specifies the details of the measurement of the impact sound pressure level, and the ISO 10140-5 Annex C specifies the reference floors on which the floor covering is installed [38,39]. ISO 10140-5 Annex C defines one heavy-weight reference floor and three types of light-weight reference floors. The heavy-weight reference floor is a reinforced concrete slab with a thickness ranging from 100 mm to 160 mm. This contrasts with the heavy-weight reference floor in KS F 2865, which requires a minimum thickness of 120 mm to 210 mm and is intended for slabs with a thinner thickness range. The reason for this difference is that floor impact noise has become a significant social issue in South Korea, and the law mandates heavier and more rigid structures to address it. Although reinforced concrete slabs as thin as 100 mm are structurally safe, South Korea currently mandates a minimum slab thickness of 210 mm or more to reduce heavy impact noise caused by children walking around barefoot. A statistical trend toward a reduction in heavy-weight impact sound was observed after the enforcement of legal regulations requiring increased slab thicknesses [3,40]. Additionally, the introduction of high-tight windows has reduced background noise. Furthermore, an increase in complaints about inter-floor noise suggests a need for further enhancements in the performances of floor coverings [32,41,42].

This study evaluated the reductions in light-weight and heavy-weight impact sound achieved by various flooring mat materials at four different test-beds with a thickness range of 150 mm to 210 mm, as specified in KS F 2865. The evaluation method used was like the impact sound generated by children's activities in previous studies. The reduction performance was evaluated by frequency bands and as a single-number quantity. Furthermore, a correlation analysis was carried out on floor structures of various bare slab thicknesses to provide fundamental data on the reliability of the evaluation method, focusing on the sound reduction performance of the same floor mat.

2. Materials and Methods

2.1. Impact Sound Sources and Measurement Method

The impact sources used in this study are shown in Figure 1. The heavy-weight impact sound source we used was a bang machine with a standard-weight impact force characteristic 1 and a rubber ball with a standard heavy-weight impact force characteristic 2, as mentioned in KS F 2865, KS F 2810-1 and KS F 2810-2 [36,43,44]. A tapping machine was used as the standard light-weight impact source. The purpose of using a floor mat is to reduce the impact sound generated by children's behavior in apartment houses. Therefore, an impact source with a force similar to that of children's behavior was selected. For the standard weight impact simulating children's behavior, a rubber ball drop height of 0.4 m with a standard weight impact force characteristic 2 was selected based on existing papers. The drop height of the standard-weight impact force characteristic 2 mentioned in ISO 16283-2 and KS F 2810-2 is 1 m [44,45]. In this case, the impact force is about 1800 N, and the impact force generated by the children's behavior is about 1100 N, which is similar to a rubber ball drop height of 0.4 m [46,47]. The experimental floor mat specimen was placed at the center of the living room of the sound source room. Then, a total of five exciting positions were considered. As shown in Figure 2, a total of five microphones, including one in a central position, were installed in the downstairs sound-receiving room. The floor impact sound insulation performance test was conducted according to KS F 2810-1 and KS F 2810-2 [43,44]. During the experiment, the test beds were closed to everyone except the experimenters to control any possible noise from outside that might have affected the results.

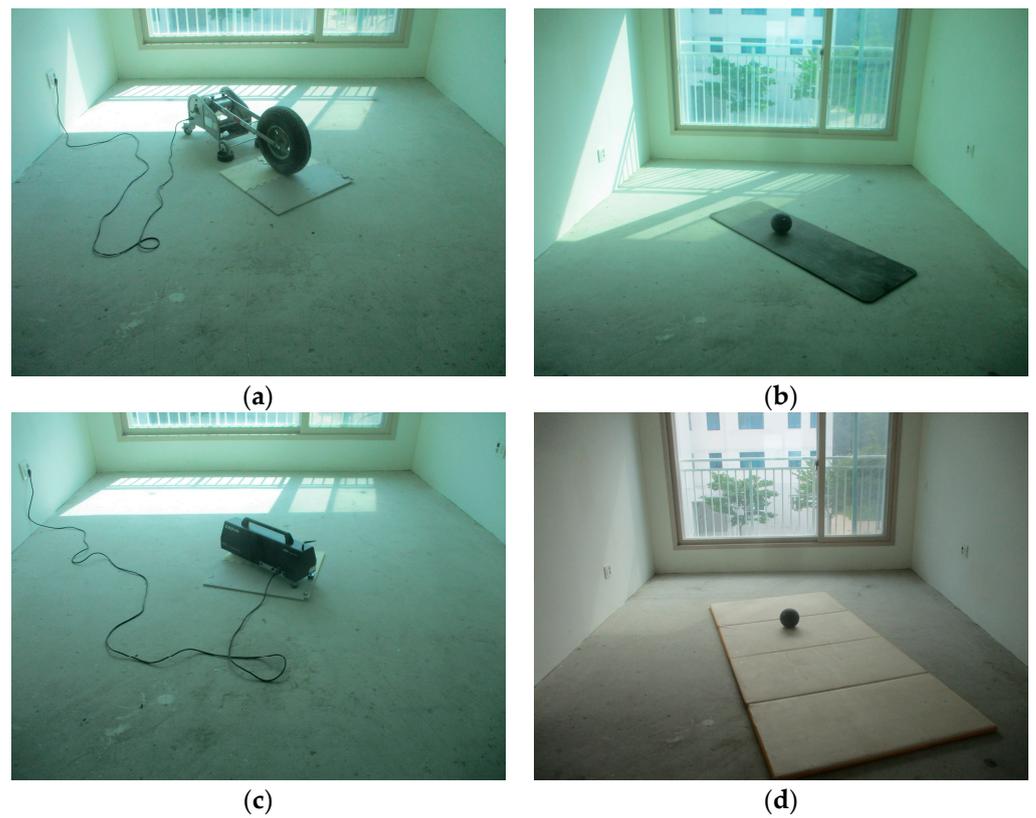


Figure 1. The employed impact sound sources in the sound source room. (a) Bang machine; (b) rubber ball (drop height of 1 m); (c) tapping machine; (d) rubber ball (drop height of 0.4 m).



Figure 2. View of the sound-receiving room with five microphones.

2.2. Test Beds with Different Floor Plans and Slab Thickness

A total of four test beds were employed, as shown in Figure 3. As shown in Figure 3a, test bed A is a box-type experimental building with a wall-type concrete structure. It was divided into two rectangular rooms, and the impact sound reduction performance was measured for each floor structure due to the different slab thicknesses. The sound source room of test bed A was exposed to the outside. The floors structures were a bare slab with a thickness of 150 mm and a bare slab with a thickness of 180 mm for left and right rooms, respectively. Figure 3b shows test bed B, which was originally designed as an up-and-downside coupled reverberation chamber. In test bed B, an acoustic chamber was designed at the downside, and the floor was composed of a bare slab of 150 mm. Test beds C and D, as shown in Figures 3c and 3d, respectively, were constructed as standard apartment buildings to reflect real-life style floor plans and evaluate floor impact sound performances [3]. The floor structure of test bed C had a bare slab with a thickness of 210 mm as a wall-type concrete structure, as shown in Figure 3c. However, the floor structure of test bed D had a bare slab with a thickness of 150 mm as a Rahmen-type beam–column concrete structure, as shown in Figure 3d. All four test beds are test facilities that meet the requirements of KS F 2865 [36].

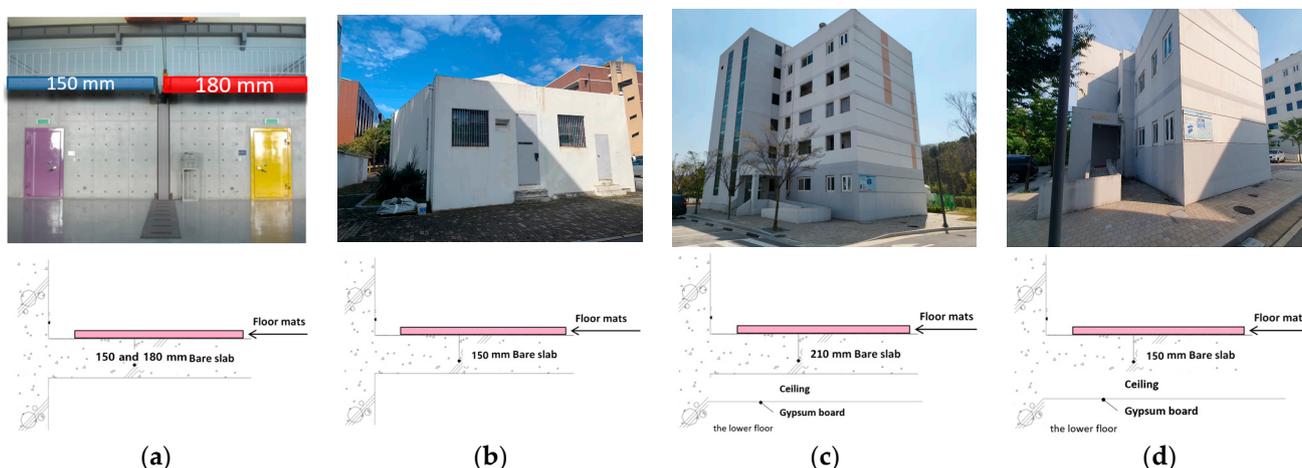


Figure 3. Picture and sectional plan of the bare slab structure with floor mat sample installed. (a) Test bed A—a box-type building with two rooms of bare slab thickness of 150 and 180 mm; (b) Test bed B—an up-and-downside coupled reverberation room with a bare slab thickness of 150 mm; (c) Test bed C—a wall-type concrete apartment building with a real-life floor plan and bare slab thickness of 210 mm; (d) Test bed D—a Rahmen-type beam–column concrete apartment building with a real-life floor plan and bare slab thickness of 150 mm.

2.3. Floor Mat Samples

Table 1 shows the eight types of floor mat samples used in this study. The floor mat samples were selected based on their current availability on the market and frequency of use by residents. Floor mat sample #1 is the thinnest among the eight types; it is made of polyurethane and has a thickness of 8 mm. Floor mat sample #2 is made of polyethylene and has a thickness of 13 mm, while floor mat sample #3 is made of polyurethane and has a thickness of approximately 12 mm. Floor mat sample #4 is characterized by a covering thin film of polyethylene on the inside and PVC on the outside. It is divided into three parts, making it foldable. It is the thickest of the eight types of floor mats, having a thickness of 36 mm. Floor mat sample #5 is a ‘fuzz mat’ made of ethylene-vinyl acetate copolymer. It can be assembled like a puzzle to achieve a desired size. It is 300 mm wide and 300 mm long and is approximately 11 mm thick. Floor mat samples #6 and #7 are both made of polyethylene and have similar thicknesses of 13 mm and 14 mm, respectively. Floor mat sample #8, which is 16 mm thick, is designed for physical exercise and yoga activities at home or in the gym. In this experiment, the impact sound reduction performance of

the eight floor mat samples, placed on the five floor structures of the four test beds, was investigated.

Table 1. Details of the floor mat samples.

Sample No.	Sample #1	Sample #2	Sample #3	Sample #4	Sample #5	Sample #6	Sample #7	Sample #8
Picture								
Thickness	8 mm	13 mm	12 mm	36 mm	11 mm	13 mm	14 mm	16 mm
Material type	Polyurethane	Polyurethane	Polyurethane	Polyurethane	Ethylene-vinyl acetate copolymer	Polyethylene	Polyethylene	Polyurethane

2.4. Evaluation Method including Single-Number Quantity

As shown in Equation (1), the impact sound reduction performance evaluation method was based on the difference in sound pressure level (ΔL) measured with and without the sample covering the bare slab, expressed in decibels (dB), as specified in KS F 2865 and ISO 10140-1 Annex H [36,37]. Firstly, measurements were taken for both light-weight and heavy-weight impact sounds before the mat was installed on the bare slab, and then the same light-weight and heavy-weight impact sounds were evaluated after the mat was installed. The reduction level was calculated by subtracting the pre-installation value from the post-installation value. Additionally, the SNQ (single-number quantity) value was derived for each frequency band simultaneously with the reduction amount. The measurements were taken in 1/3 octave bands ranging from 50 Hz to 630 Hz for heavy-weight impact sound and from 100 Hz to 3150 Hz for light-weight impact sound.

$$\Delta L = L_{\text{without floor covering}} - L_{\text{with floor covering}} \quad (1)$$

3. Results

3.1. Test Bed A (Bare Slab Thickness of 150 mm)

Figure 4 shows the impact sound reduction performance results for the bare slab with a thickness of 150 mm in test bed A (shown in Figure 3a). The test room consisted of two floor structures with a total of eight floor mat samples. It was found that sufficient impact sound reduction was achieved for light-weight impact sound, regardless of the type of floor mat used. We found that the reduction amount by frequency band increased as the reduction amount went to the high frequency band. For a single-number quantity, a reduction amount of up to 38 dB and a reduction amount of up to 47 dB or more was secured. The impact sound reduction was similar to a certain frequency band for the bang machine, but the impact sound reduction performance increased somewhat from 315 Hz and above. In the case of a single-number quantity, the impact sound reduction performance ranged from 1 dB to 3 dB and from 4 dB to 10 dB, respectively. Figure 4c shows the reduction performance of the floor mat samples for a rubber ball drop height of 1 m. The reduction amount by frequency band indicates that the impact sound is amplified from the 50 Hz band to the 100 Hz band when some floor mats are installed. However, the impact sound reduction performance increased as the frequency band increased from 125 Hz and above. Figure 4d shows the impact sound reduction performance of the floor mat for a rubber ball drop height of 0.4 m, simulating a child's behavior. The impact sound reduction performance across frequency bands exhibited a similar reduction pattern to that of the rubber ball drop height of 1 m. A single-number quantity can achieve a minimum of 3 dB and a maximum of 9 dB of impact sound reduction.

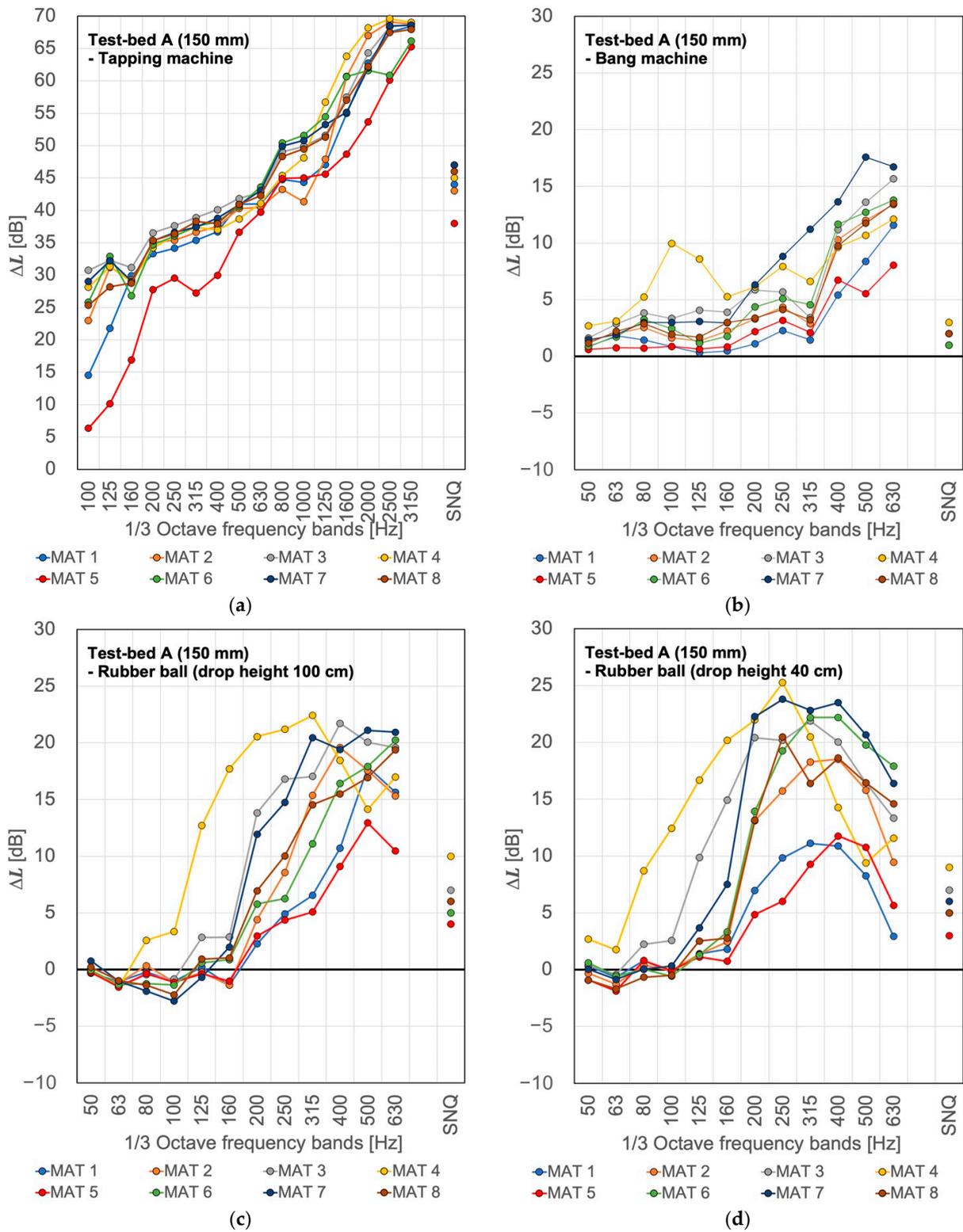


Figure 4. Frequency characteristics of floor impact sound reduction levels for each mat sample in the 150 mm thick room of test bed A. (a) Tapping machine; (b) bang machine; (c) rubber ball (drop height of 1 m); (d) rubber ball (drop height of 0.4 m).

3.2. Test Bed A (Bare Slab Thickness of 180 mm)

Figure 5 presents the results regarding the evaluation of the impact sound reduction performance of the floor mat samples for a bare slab with a thickness of 180 mm in test

bed A (shown in Figure 3a). The impact sound reduction performance in the frequency band of light-weight impact sound increased from 100 Hz to 3150 Hz. Our single-number quantity analysis showed that a reduction performance of at least 35 dB and up to 42 dB was achieved. Regarding the measurement results for the bare slab with a thickness of 150 mm, floor mat sample #5 exhibited the lowest impact sound reduction performance. This is because the light-weight impact sound was directly transmitted to the bottom due to the high density of floor mat sample #5. The bang machine demonstrated that it could provide adequate impact sound reduction performance throughout the frequency band. However, the analysis revealed that some floor mats slightly amplified the frequency band of 125 Hz. The single-number quantity analysis confirmed a minimum impact sound reduction performance of 1 dB and a maximum of 5 dB. A 1 dB improvement in impact sound reduction performance was observed for floor mat sample #5. The impact sound reduction of a rubber ball being dropped from a height of 1 m was enhanced when most of the floor mats were installed in the frequency band below 100 Hz. However, it was determined that the impact sound reduction performance was adequate, as it extended to the band above 125 Hz to 630 Hz. For single-number quantities, our analysis showed that the impact sound reduction performance was secured at a minimum of 1 dB and up to 13 dB. Figure 5d shows the impact sound reduction performance of a rubber ball dropped at 0.4 m, which mimics the impact force generated by children’s actions. The reduction performance was amplified in each frequency band from 50 Hz to 100 Hz. However, the impact sound reduction performance increased as the frequency band increased from 125 Hz to the 630 Hz high-frequency band. The single-number quantity analysis indicates a secured impact sound reduction performance of at least 2 dB and up to 13 dB. For the bare slabs of 150 mm and 180 mm, as well as rubber ball drop heights of 1 m and 0.4 m, the performance increased at certain frequency bands. The installation of a floor mat is believed to increase the impact force of each impact source due to the matching of the impact sound of the rubber ball and the resonant frequency band of the floor structure.

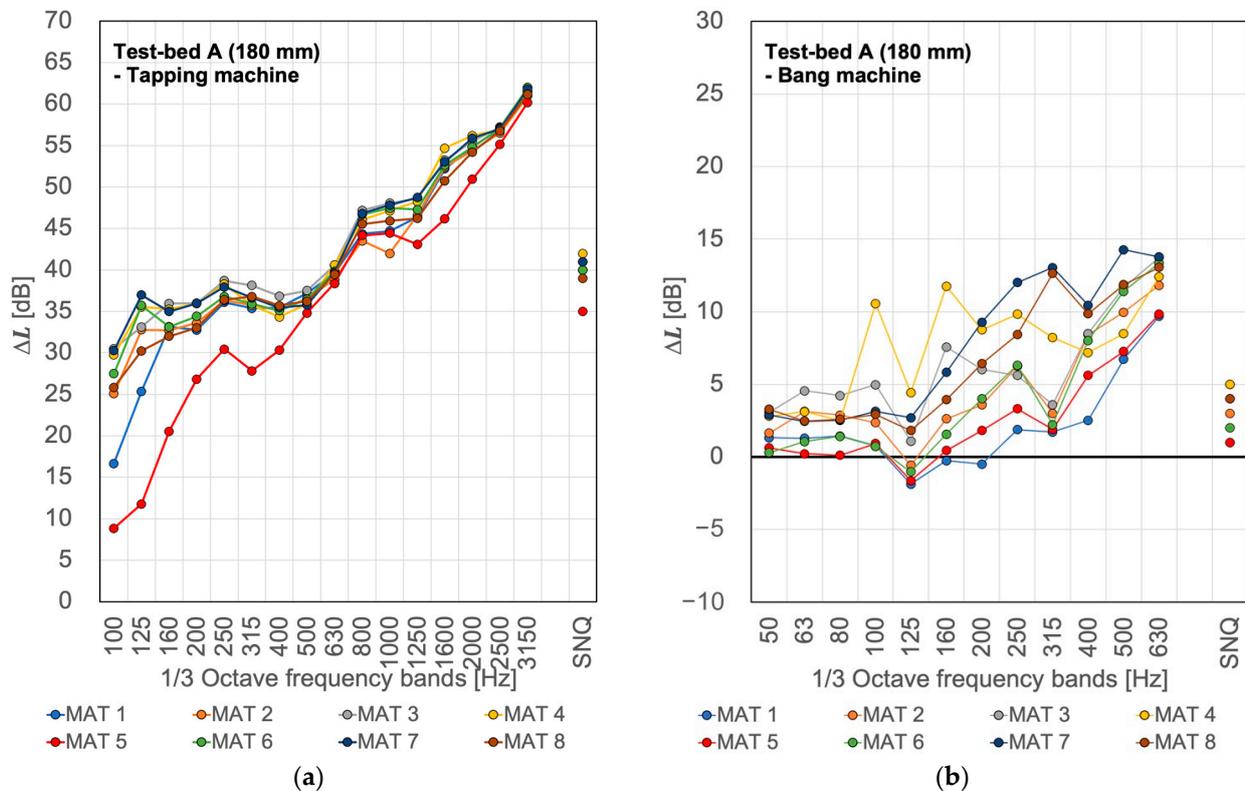


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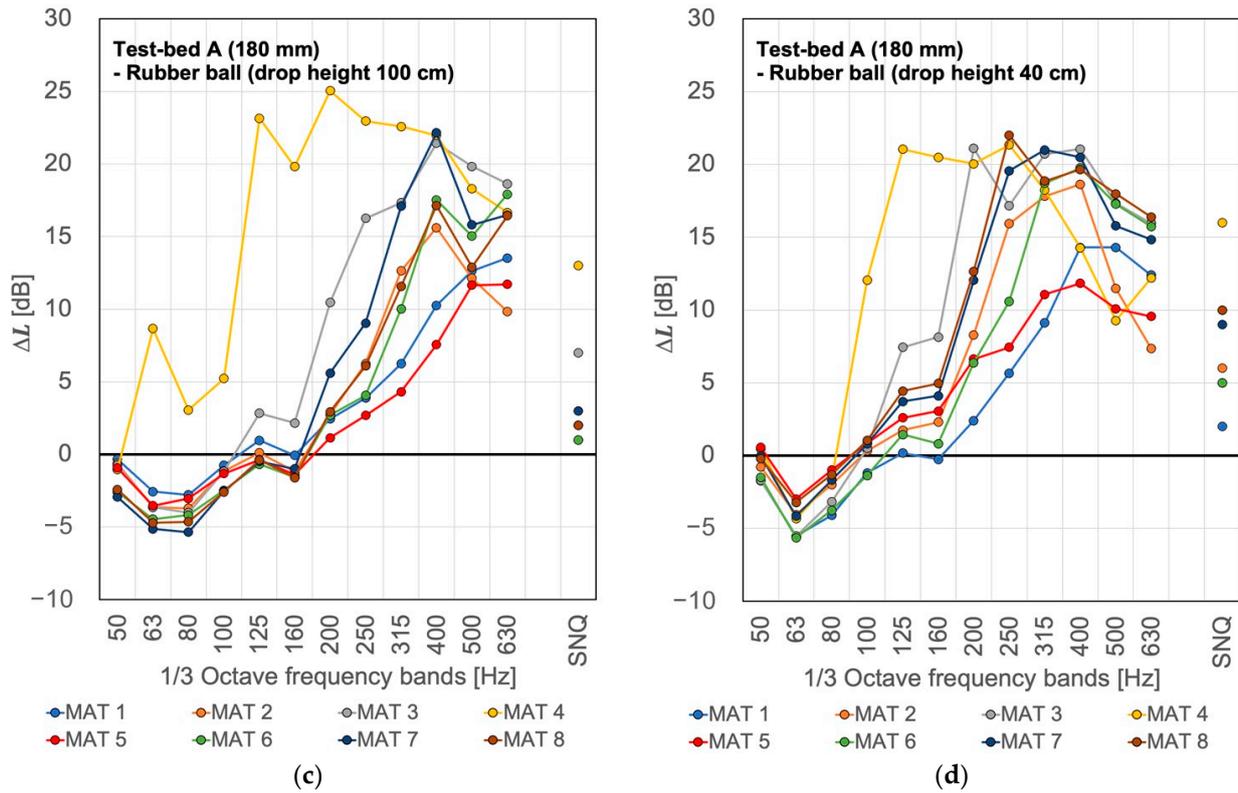
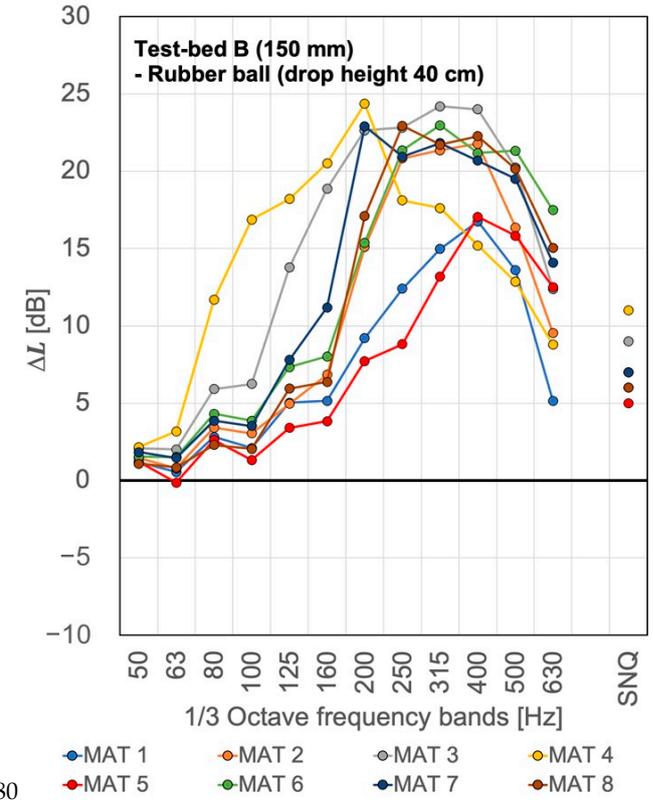
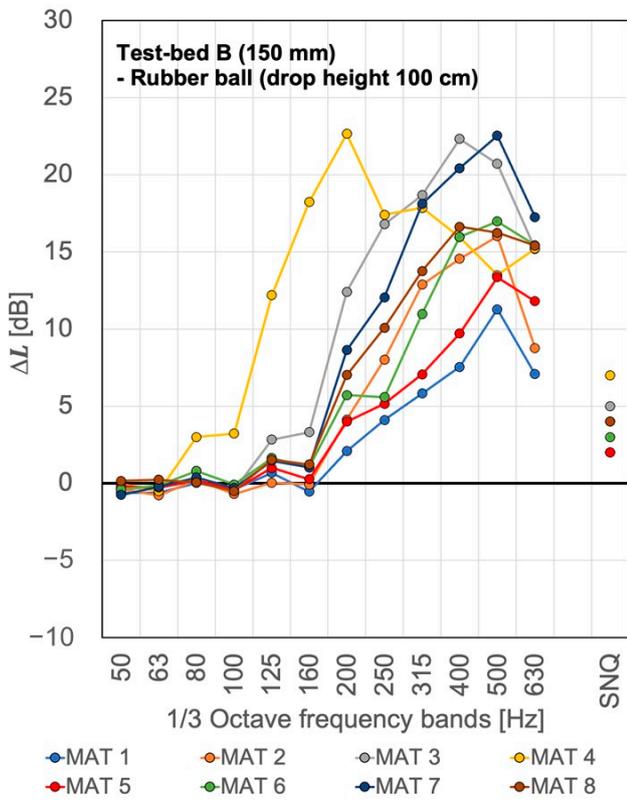
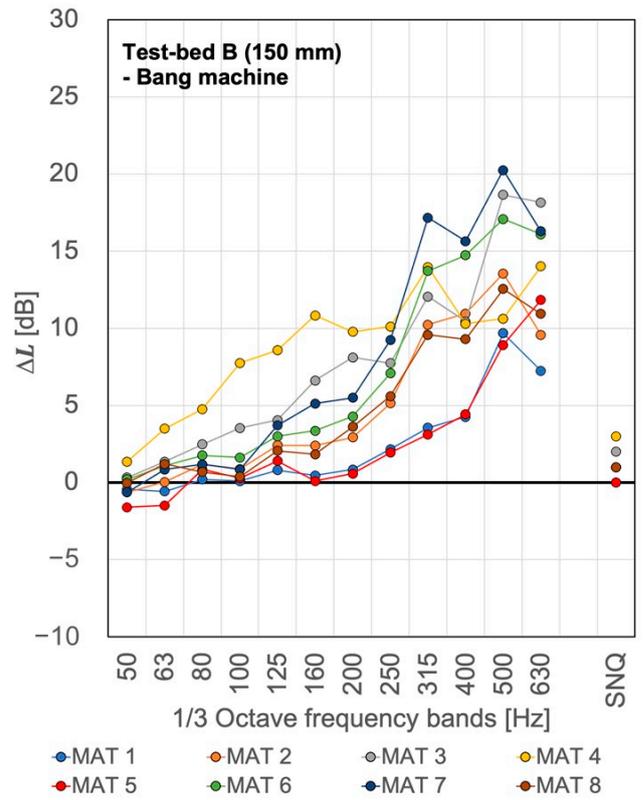
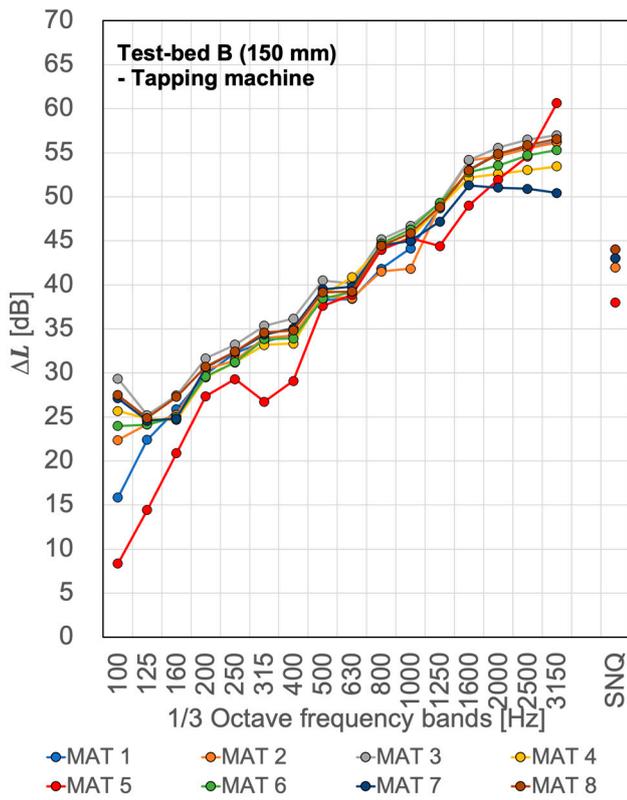


Figure 5. Frequency characteristics of floor impact sound reduction levels for each mat sample in the 180 mm thick room of test bed A. (a) Tapping machine; (b) bang machine; (c) rubber ball (drop height of 1 m); (d) rubber ball (drop height of 0.4 m).

3.3. Test Bed B (Bare Slab Thickness of 150 mm)

Figure 6 shows the results derived from evaluating the impact sound reduction performance of eight floor mat samples in test bed B (shown in Figure 3b). The impact sound reduction performance increased from the 100 Hz band to the 3150 Hz band for all types of floor mat samples, regardless of their weight differences. We found that the single-number quantity resulted in a minimum reduction of 38 dB and a maximum reduction of 44 dB. All samples, except for floor mat sample #5, achieved a reduction performance of over 40 dB. Figure 6b illustrates the impact sound reduction performance after being hit by a bang machine. It was found that the installation of certain floor mats led to a slight amplification of impact sound in the 50 Hz and 63 Hz bands. However, there was an increase in the impact sound reduction performance from 100 Hz to 630 Hz. Upon further analysis of the numerical values, it was observed that floor mat samples #1 and #5 did not provide any impact sound reduction when placed on the floor. However, the floor mats that remained showed a minimum reduction of 1 dB and a maximum reduction of 3 dB. Figure 6c shows the impact sound reduction performance of a rubber ball dropped from a height of 1 m. The reduction performance is insignificant from the 50 Hz band to the 100 Hz band. However, our analysis showed that the impact sound reduction performance from 125 Hz to 630 Hz was sufficiently secured. Furthermore, based on the single-number quantity of impact sound reduction, the performance ranged from a minimum of 2 dB to a maximum of 7 dB. Additionally, the impact sound reduction performance was analyzed in relation to a rubber ball dropping from a height of 0.4 m, which simulates the impact force generated by a child, as shown in Figure 6d. The impact sound reduction performance increased from the 50 Hz band to the 400 Hz band as the frequency band increased. However, from 500 Hz to 630 Hz, the attenuation decreased somewhat. The analysis aimed to achieve a minimum of 5 dB and a maximum of 11 dB of impact sound reduction, based on a single-number quantity.



(a)

(b)

(c)

(d)

Figure 6. Frequency characteristics of floor impact sound reduction levels for each mat sample in the 150 mm thick room of test bed B. (a) Tapping machine; (b) bang machine; (c) rubber ball (drop height of 1 m); (d) rubber ball (drop height of 0.4 m).

3.4. Test Bed C (Bare Slab Thickness of 210 mm)

Figure 7 shows the impact sound reduction performance results of eight types of floor mat samples in the 210 mm bare slab living room of the wall-type test bed C (shown in Figure 3c). The impact sound reduction performance for light-weight impact sound increased from the 100 Hz band to the 3150 Hz band when all floor mat samples were installed. For a single-number quantity, it was found that the impact sound reduction performance ensures a minimum of 35 dB and a maximum of 40 dB. Figure 7b shows the reduction performance of the bang machine by frequency band. Reductions was achieved in all frequency bands, although regarding the impact sound reduction performance of specific floor mat samples, only two floor mat samples (#5 and #6) did not reduce impact sound in the single-number quantity. However, regarding floor mat sample #4, it was analyzed to achieve a maximum reduction performance of 3 dB. The results regarding the impact sound reduction performances of the floor mats for when a rubber ball was dropped from a height of 1 m are presented in Figure 7c. The impact sound reduction performance was insignificant from the 50 Hz to the 100 Hz band. However, it was secure from the 125 Hz band and above. Furthermore, in the case of a single-number quantity, the impact sound reduction performance ranged from 1 dB to 2 dB. These single-number quantities differed slightly from the results obtained in test beds A and B. Figure 7d displays the impact sound reduction performance when a rubber ball was dropped from a height of 0.4 m. Furthermore, the impact sound reduction performance improved in the 50 Hz band to 250 Hz band range but decreased in the 315 Hz band to 630 Hz band range. The single-number quantity indicates a minimum reduction of 1 dB and a maximum reduction of 5 dB.

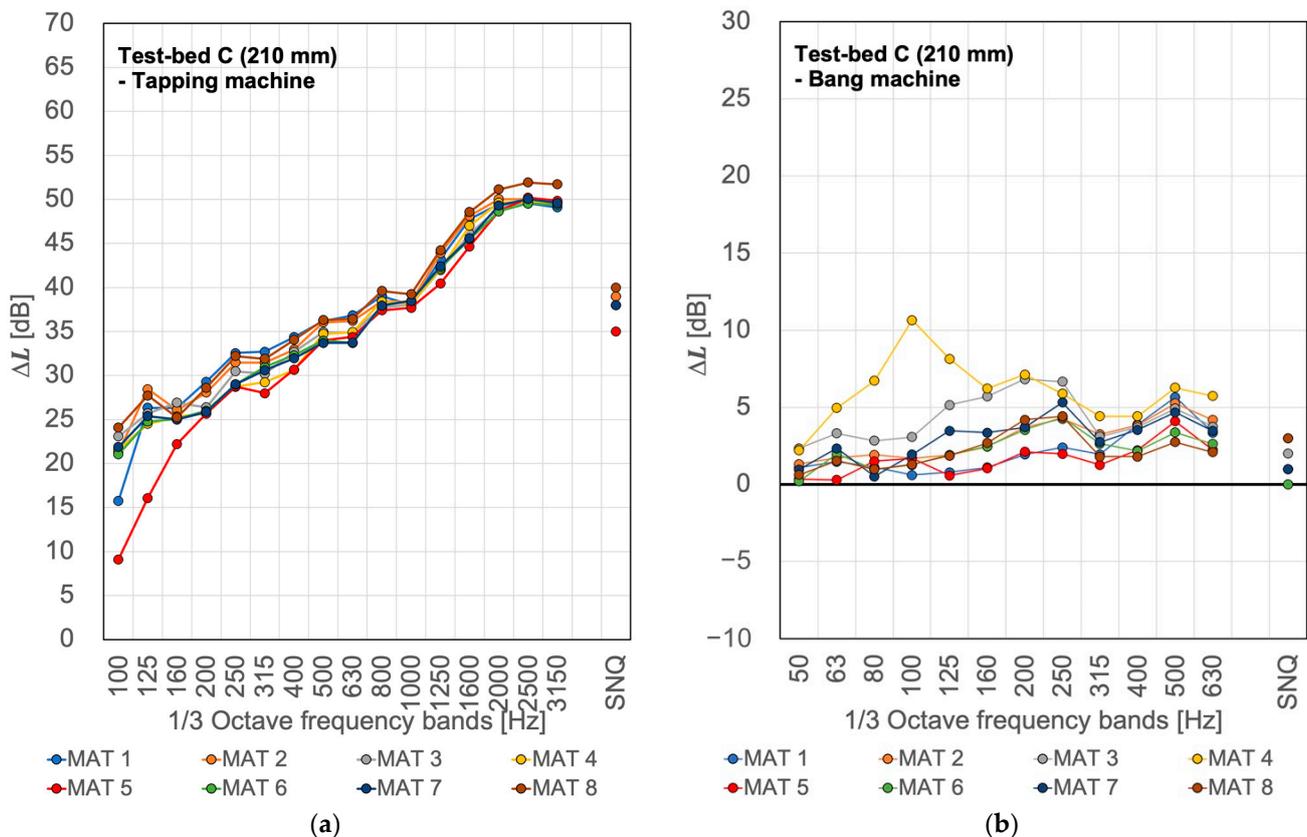


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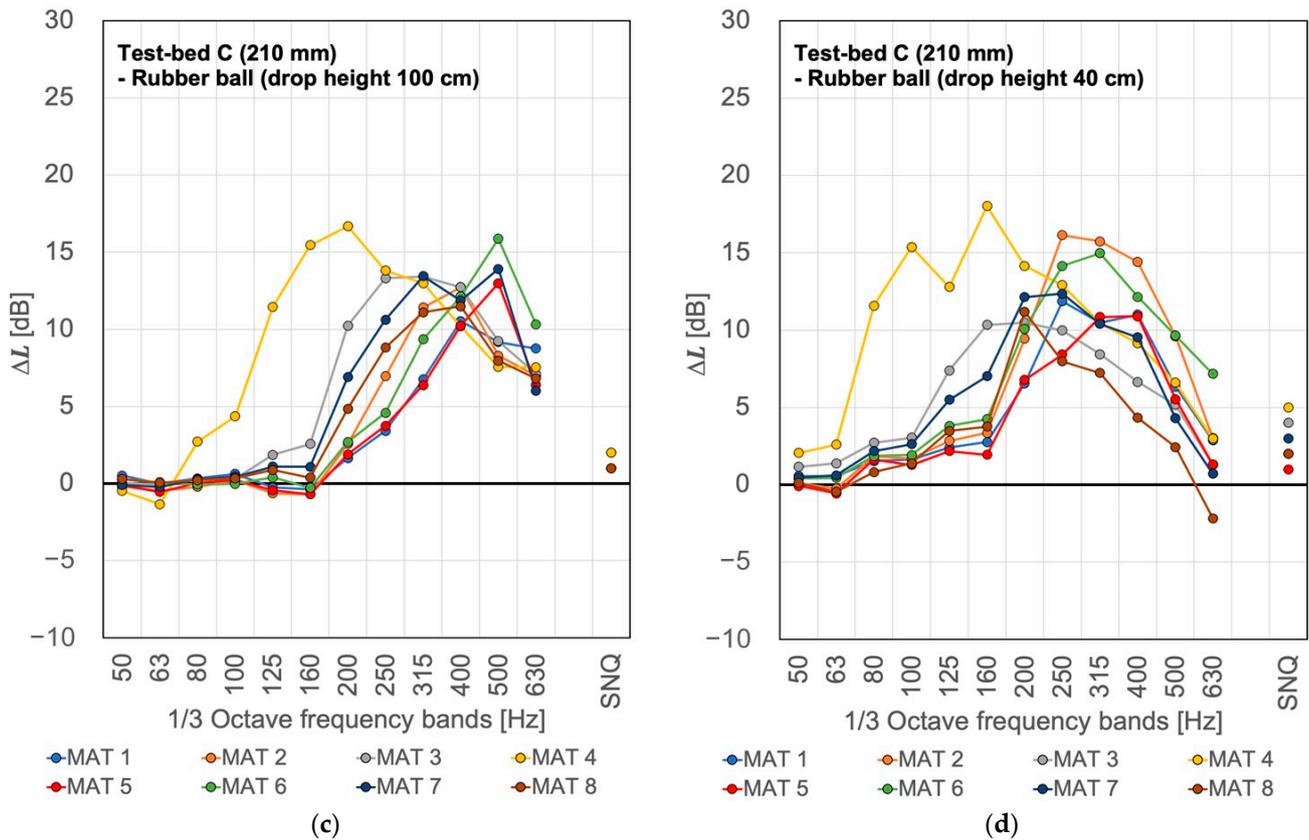


Figure 7. Frequency characteristics of floor impact sound reduction levels for each mat sample in the 210 mm thick room of test bed C. (a) Tapping machine; (b) bang machine; (c) rubber ball (drop height of 1 m); (d) rubber ball (drop height of 0.4 m).

3.5. Test Bed D (Bare Slab Thickness of 150 mm)

Figure 8 shows the impact sound reduction performance results of eight floor mat samples in the 150 mm bare slab living room of the Rahmen-type test bed (test bed D; shown in Figure 3d). For light-weight impact sound, the reduction performance increased from the 100 Hz band to the 3150 Hz band for all floor mat samples. In a single-number quantity, the analysis showed a minimum of 34 dB and a maximum of 44 dB of reduction performance. Figure 8b shows the reduction performance of the bang machine by frequency band. Reductions were achieved in all frequency bands, with varying reduction performances for each floor mat sample. Only two floor mat samples (#5 and #7) showed no reduction performance in a single-number quantity. However, floor mat sample #4 was found to have a maximum reduction performance of 3 dB. Figure 8c displays the results corresponding to when a rubber ball was dropped from a height of 1 m. The reduction performance was insignificant from the 50 Hz band to the 125 Hz band. However, it was secure from the 160 Hz band and above. Additionally, a minimum reduction performance of 1 dB and a maximum reduction performance of 6 dB were observed in terms of single-number quantity. The single-number quantity evaluation results differed from those of test beds A and B but were similar to the impact sound reduction performance pattern of test bed C. Figure 8d shows the reduction performance results corresponding to when a rubber ball was dropped from 0.4 m. Furthermore, the impact sound reduction performance improved in the 50 Hz band to 250 Hz band range but decreased in the 315 Hz band to 630 Hz band range. The single-number quantity indicates a minimum reduction of 2 dB and a maximum reduction of 8 dB.

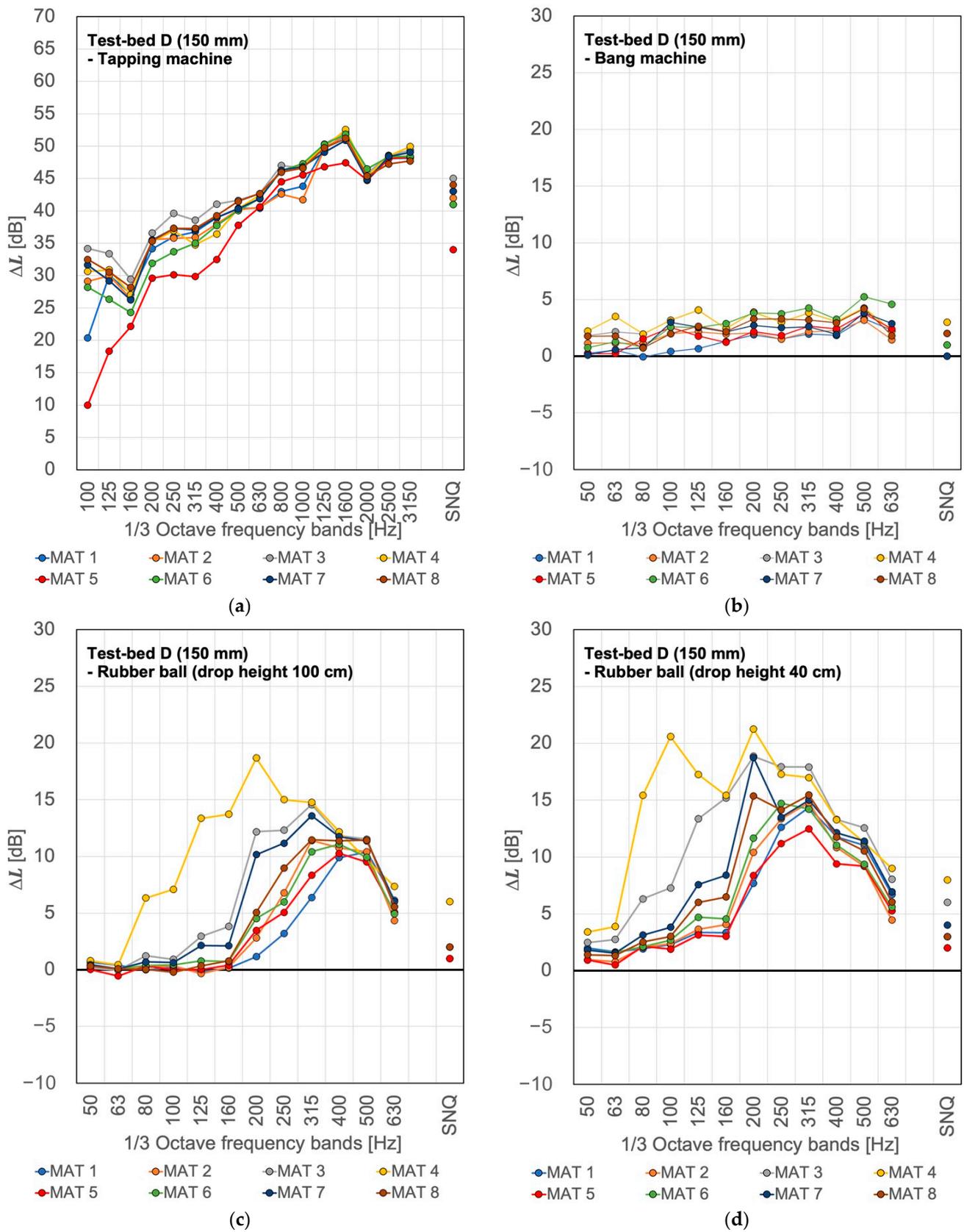


Figure 8. Frequency characteristics of floor impact sound reduction levels for each mat sample in the 150 mm thick room of test bed D. (a) Tapping machine; (b) bang machine; (c) rubber ball (drop height of 1 m); (d) rubber ball (drop height of 0.4 m).

4. Discussion

4.1. Correlation Analysis of Impact Sound Reduction Performance According to Bare Slab Thickness

A correlation analysis was conducted on the reduction performance of the same floor mat with the same floor structure. To examine the reliability of the measurement and evaluation methods specified in KS F 2865, a correlation analysis was conducted on the impact sound reduction performance and single-number quantity evaluation. The Korea standard code of KS F 2865 specifies a requirement for bare slab thicknesses to be in the range of 120 mm to 210 mm for measuring and evaluating floor covering materials [36]. An analysis was conducted to determine the correlation between impact sound reduction performance and slab thickness. The evaluation was based on the single-number quantities derived at slab thicknesses of 150 mm, 180 mm, and 210 mm. The impact sources analyzed were a tapping machine, bang machine, and rubber ball.

4.1.1. Correlation Analysis between the Test Beds with a Bare Slab Thickness of 150 mm

This study utilized four test beds and tested two structures in test bed A, resulting in a total of five floor structures. Three test beds had a bare slab thickness of 150 mm. A correlation analysis was conducted on a single-number quantity (SNQ) of the reduction performance of eight floor mat samples for the same impact source measured on a 150 mm bare slab in three test beds.

First, the correlation between test bed A (pictured in Figure 3a) and test bed B (pictured in Figure 3b) for a 150 mm bare slab was analyzed, as shown in Figure 9. The correlation analysis of SNQ for light-weight impact sound reduction performance is shown in Figure 9a, and the correlation $R^2 = 0.90$ ($y = 1.51x - 19.45$) was observed to be very high. The coefficient of determination of the data obtained from the two floor structures of the bang machine is $R^2 = 0.75$ ($y = 0.62x + 1.05$), as shown in Figure 9b, and the coefficient of determination of the rubber ball is $R^2 = 0.95$ ($y = 1.08x + 1.96$), as shown in Figure 9c. Based on the results of the analysis, the evaluated values of light-weight impact sound reduction performance and heavy-weight impact sound reduction performance in test beds A and B, consisting of a bare slab with a thickness of 150 mm, are at a reliable level for impact sound reduction. In addition, when measuring and evaluating the reduction performances of the floor mats in these two test beds, it was judged that the values can support the validity of the bare slab thickness range of 150 mm mentioned in KS F 2865.

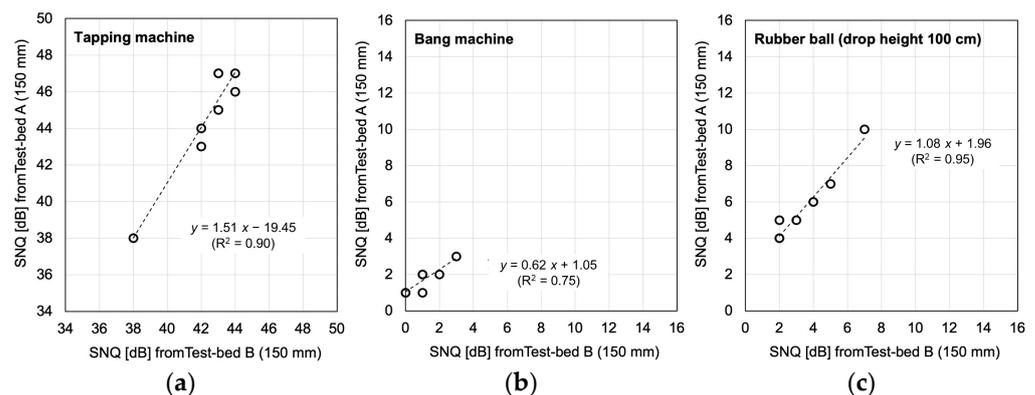


Figure 9. Correlation analysis between test beds A and B (both with a slab thickness of 150 mm). (a) Tapping machine; (b) bang machine; (c) rubber ball dropping at 1 m height.

Second, the correlation analysis of the test bed with a bare slab thickness of 150 mm shown in Figure 3a and the Rahmen-type test bed (test bed D) shown in Figure 3d is shown in Figure 10. The correlation analysis of SNQ for light-weight impact sound reduction performance showed that the coefficient of determination was very high, with $R^2 = 0.78$ ($y = 0.80x + 11.34$), as shown in Figure 10a. The coefficient of determination of the data obtained from the two test beds when using a bang machine is $R^2 = 0.58$ ($y = 0.48x + 1.21$),

as shown in Figure 10b, and the coefficient of determination for the data obtained when using the rubber ball is $R^2 = 0.88$ ($y = 1.12x + 3.50$), as shown in Figure 10c. Therefore, the evaluation values of the rubber ball reduction performance among light-weight impact sound and heavy-weight impact sound in test beds A and D (both consisting of a bare slab with a thickness of 150 mm) are reliable in terms of the amount of impact sound reduction. However, the correlation analysis results for the bang machine are somewhat lower than the correlation analysis results derived from test beds A and B. This is because the correlation analysis results are somewhat lower. The reason for the lower correlation is that the floor impact sound test bed is a Rahmen-type structure rather than a wall structure, so when a large impact force such as the bang machine is applied, the behavioral characteristics of the floor structure are different, and the impact sound transmitted to the lower part is different.

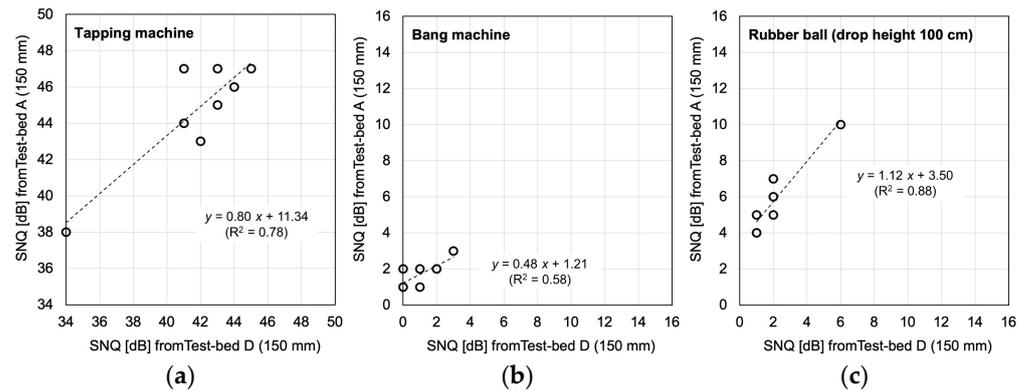


Figure 10. Correlation analysis between test beds A and D (both with a slab thickness of 150 mm). (a) Tapping machine; (b) bang machine; (c) rubber ball dropping at 1 m height.

Third, a correlation analysis of test bed B (shown in Figure 3b), which is a 150 mm bare slab, and test bed D (shown in Figure 3d), which has a Rahmen-type structure, was conducted, and the results are shown in Figure 11. The correlation analysis of SNQ for light-weight impact sound reduction performance showed that the coefficient of determination was very high, with $R^2 = 0.94$ ($y = 1.71x - 30.64$), as shown in Figure 11a. The coefficient of determination of the data obtained from the two test beds when using the bang machine is $R^2 = 0.77$ ($y = x$), as shown in Figure 11b, and the coefficient of determination of the data obtained when using the rubber ball is $R^2 = 0.82$ ($y = 0.84x - 0.92$), as shown in Figure 11c. Therefore, the evaluation values of light-weight impact sound and heavy-weight impact sound reduction performance in test beds B and D (both consisting of a bare slab with a thickness of 150 mm) are reliable in terms of impact sound reduction. In addition, when measuring and evaluating the reduction performance of floor mats in the two test beds, it was judged that it is possible to secure the validity of the slab thickness range of 150 mm mentioned in KS F 2865.

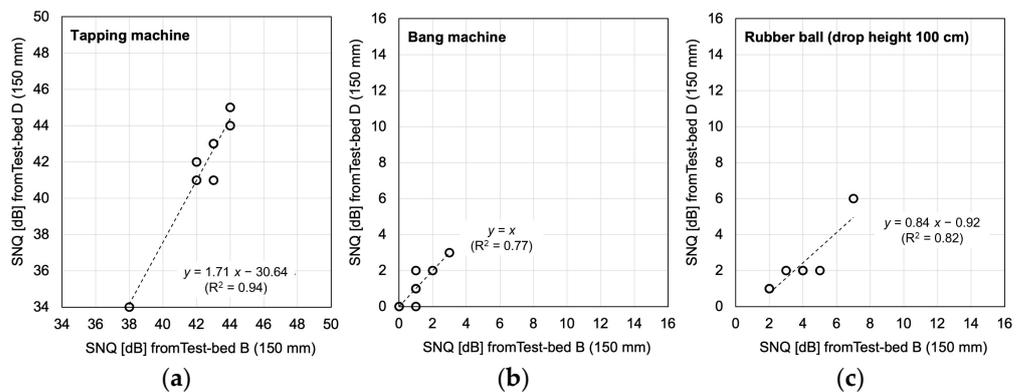


Figure 11. Correlation analysis between test beds B and D (both with a slab thickness of 150 mm). (a) Tapping machine; (b) bang machine; (c) rubber ball dropping at 1 m height.

4.1.2. Correlation Analysis between the Bare Slab Thicknesses of 150 mm and 180 mm in Test Bed A

A correlation analysis was conducted on the SNQs of the impact sound reduction performances evaluated on bare slabs with thicknesses of 150 mm and 180 mm in test bed A. The correlation analysis was conducted on the reduction performance. The results of the correlation analysis are shown in Figure 12. As shown in Figure 12a, the correlation analysis of SNQs with light-weight impact sound reduction performance was high, with a correlation of $R^2 = 0.67$ ($y = 0.57x - 14.52$) being recorded. The correlation of the data obtained from the two test beds when using the bang machine was $R^2 = 0.80$ ($y = 2.07x - 0.50$), as shown in Figure 12b, and the correlation of the data obtained when using the rubber ball was $R^2 = 0.89$ ($y = 2.00x - 7.90$), as shown in Figure 12c. Based on the results of the analysis, the evaluated values of light-weight impact sound and heavy-weight impact sound reduction performance in test bed A when bare slab thicknesses of 150 mm and 180 mm were used are reliable in terms of impact sound reduction.

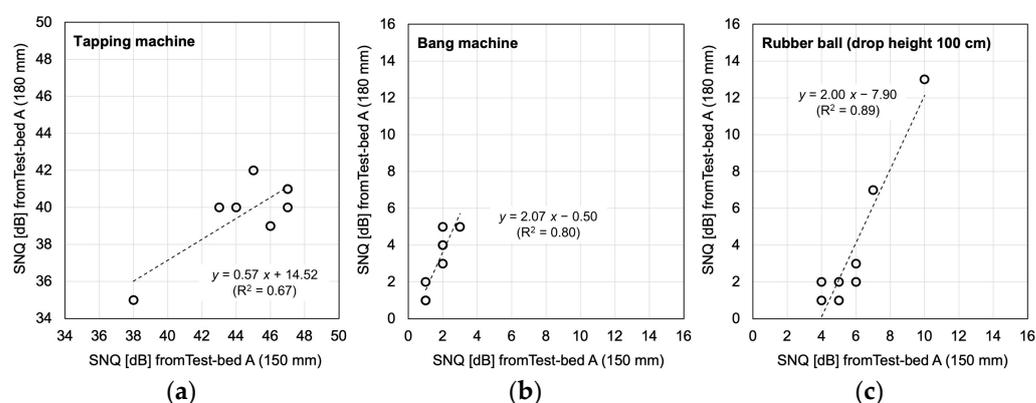


Figure 12. Correlation analysis between slab thicknesses of 150 mm and 180 mm in test bed A. (a) Tapping machine; (b) bang machine; (c) rubber ball dropping at 1 m height.

4.1.3. Correlation Analysis between Test Bed A (Bare Slab Thickness of 180 mm) and Test Bed C (Bare Slab Thickness of 210 mm)

A correlation analysis was conducted on the impact sound reduction performance SNQs evaluated on bare slabs with thicknesses of 180 mm and 210 mm. The thickness of the two floor structures differs by about 30 mm, but it is included in the floor thickness range specified in KS F 2865. The results of the correlation analysis of the impact sound reduction performance of the two floor structures are shown in Figure 13. The correlation of the SNQ for light-weight impact sound reduction performance was somewhat lower, with a correlation of $R^2 = 0.37$ ($y = 0.89x + 5.79$), as shown in Figure 13a. The correlation of the data obtained from the two floor structures when using the bang machine is $R^2 = 0.61$ ($y = 1.08x + 1.65$), as shown in Figure 13b, and the correlation of the data obtained when using the rubber ball is as high as $R^2 = 0.83$ ($y = 8.17x - 6.33$), as shown in Figure 13c. Based on the results of the analysis, the correlation between light-weight impact sound and the SNQ of impact sound reduction performance was low. The factors that were analyzed for low correlation were the different structures of the two test beds and the fact that the floor impact sound test bed with a bare slab thickness of 210 mm had a ceiling structure, which had a higher reduction performance in the high frequency band when evaluating light-weight impact sound. In the case of the bang machine, the correlation value of impact sound reduction performance was also somewhat lower than the correlation analysis results according to other floor thicknesses. However, the correlation value of the impact sound reduction performance of the rubber ball is at a level that can be trusted as the amount of impact sound reduction. Looking towards the future, it is necessary to change the conditions, such as the acoustic chamber, in the floor impact test room with a bare slab thickness of 210 mm. In addition, it is necessary to conduct additional floor mat tests in the changed test room to evaluate the impact sound reduction and to correlate the results

with other bare slab thicknesses and conditions. Based on the results, it is judged that it is necessary to consider whether the slab thickness range mentioned in KS F 2865 can be met.

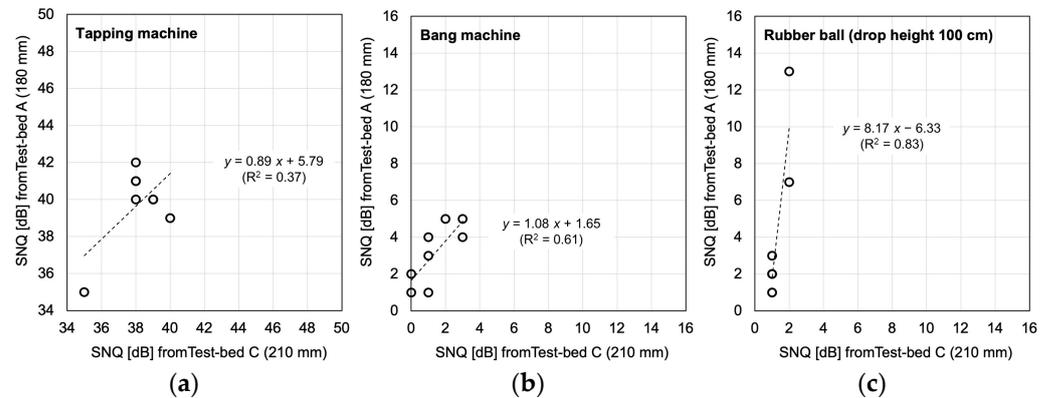


Figure 13. Correlation analysis between test bed A with a slab thickness of 180 mm and test bed C with a bare slab thickness of 210 mm. (a) Tapping machine; (b) bang machine; (c) rubber ball dropping at 1 m height.

4.2. Comparison of Single-Number Quantities for the Same Impact Sound Sources

Tables 2–4 show the SNQ results of the eight floor mat samples from the different test-beds for the same impact source. Table 2 shows the results for the tapping machine, Table 3 shows the results for the bang machine, and Table 4 shows the results for the rubber ball. Regardless of the type of floor mat, it was found that the light-weight impact sound blocking performance can be sufficiently reduced due to the consistent results recorded after each floor mat was installed in the apartment houses. In addition, the discriminating power of impact sound reduction performance by type of floor mat samples was analyzed. On the other hand, in the case of the bang machine, even if floor mats were installed, there were conditions where there was no impact sound reduction performance depending on the floor structure. However, an impact sound reduction performance of up to 5 dB could be achieved depending on the type of floor mat. The impact sound reduction performance of the rubber ball was found to be at least 1 dB and up to 10 dB or more. However, the impact sound reduction performance was analyzed to be somewhat different depending on the test facility condition and bare slab thickness. Except for test bed D, with a bare slab thickness of 150 mm and 180 mm, the impact sound reduction performance corresponding to the use of the rubber ball was analyzed to be similar. In addition, in test beds C and D, which were designed similarly to actual apartment houses, the bare slab thicknesses were 210 mm and 150 mm, respectively, and the impact sound reduction performance was analyzed to be somewhat lower than in test beds A and B, which were laboratory test beds.

Table 2. The SNQs measured for the floor mat samples using a tapping machine in different test-beds. The unit is dB.

Test Bed with Bare Slab Thickness	Sample No.							
	Sample #1	Sample #2	Sample #3	Sample #4	Sample #5	Sample #6	Sample #7	Sample #8
Test bed A (150 mm)	44	43	47	45	38	47	47	46
Test bed A (180 mm)	40	40	41	42	35	40	41	39
Test bed B (150 mm)	42	42	44	43	38	43	43	44
Test bed C (210 mm)	39	39	38	38	35	38	38	40
Test bed D (150 mm)	41	42	45	43	34	41	43	44
Average	41.2	41.2	43	42.2	36	41.8	42.4	42.6
Standard deviation	1.9	1.6	3.5	2.6	1.9	3.4	3.3	3.0

Table 3. The SNQs measured for the floor mat samples using a bang machine in different test beds. The unit is dB.

Test-Bed with Bare Slab Thickness	Sample No.							
	Sample #1	Sample #2	Sample #3	Sample #4	Sample #5	Sample #6	Sample #7	Sample #8
Test-bed A (150 mm)	1	2	2	3	1	1	2	2
Test-bed A (180 mm)	1	3	5	5	1	2	4	4
Test-bed B (150 mm)	0	1	2	3	0	1	1	1
Test-bed C (210 mm)	1	1	2	3	0	0	1	3
Test-bed D (150 mm)	0	1	2	3	0	1	0	2
Average	0.6	1.6	2.6	3.4	0.4	1.0	1.6	2.4
Standard deviation	0.5	0.9	1.3	0.9	0.5	0.7	1.5	1.1

Table 4. The SNQs measured for the floor mat samples using a rubber ball dropping at 1 m height in different test beds. The unit is dB.

Test Bed with Bare Slab Thickness	Sample No.							
	Sample #1	Sample #2	Sample #3	Sample #4	Sample #5	Sample #6	Sample #7	Sample #8
Test bed A (150 mm)	4	5	7	10	4	5	6	6
Test bed A (180 mm)	2	2	7	13	1	1	3	2
Test bed B (150 mm)	2	2	5	7	2	3	4	4
Test bed C (210 mm)	1	1	2	2	1	1	1	1
Test bed D (150 mm)	1	1	2	6	1	2	2	2
Average	2	2.2	4.6	7.6	1.8	2.4	3.2	3.0
Standard deviation	1.2	1.6	2.5	4.2	1.3	1.7	1.9	2.0

There are several reasons for the differences that appeared in the impact sound reduction performance results even when the same floor mat and same slab thickness were used. These reasons are linked to various factors, such as the floor area, the location of bearing walls (both those above and below), and the presence or absence of a sound-absorbing plenum structure. These laboratory conditions may have influenced the amount of reduction due to the differences in floor vibration during impact and the changes in receiving room modes. However, these results are still considered valid since the test was conducted in accordance with KS F 2865. Therefore, the reduction values should be described with their test-bed conditions.

5. Conclusions

This study measured and evaluated the impact sound reduction performances of floor mats used in apartment buildings. The evaluation method we used followed the guidelines outlined in KS F 2865, which specifies a bare slab thickness range of 120 mm to 210 mm. Thus, the impact sound reduction performance of floor mats applied in actual apartment houses was evaluated using various test facilities with different bare slab thicknesses. The standard impact sources included a tapping machine, a bang machine, a rubber ball, and a rubber ball falling from a height of 0.4 m, simulating the impact force generated by children's behavior.

The experimental results indicate that the tapping machine, a light-weight impact sound, provided sufficient impact sound reduction performance regardless of the floor mat used and the test room conditions. Furthermore, the impact sound reduction performance increased from the low frequency band to the high frequency band. The bang machine produces heavier impact sounds than other sources, resulting in a lower impact sound reduction performance, even with floor mats installed. In some cases, it may even amplify certain frequency bands. Similar to light-weight impact sounds, the impact sound reduction

performance increases from low to high frequency bands. The results of the SNQ analysis indicate that the installation of floor mats may not always reduce impact sound, with a maximum reduction of 5 dB being observed. However, the effectiveness of floor mats varied depending on their type. Rubber balls amplified the impact sound from the 50 Hz band to the 125 Hz band for heavy-weight impacts, depending on the type of floor mat and the thickness of the bare slab. However, the study found that impact sound reduction performance was achieved from the 160 Hz band and above, with a tendency for the impact sound to decrease from the 315 Hz band to the 630 Hz band. The SNQ evaluation showed a minimum of 1 dB and a maximum of 10 dB or more of impact sound reduction performance. For a rubber ball drop height of 0.4 m, which simulates a child's behavior, it is possible to secure impact sound reduction performance by installing a floor mat, regardless of the bare slab and floor structure. The impact sound reduction performance was somewhat amplified in certain frequency bands with certain floor mats. Similar to the rubber ball drop height of 1 m, the impact sound reduction performance increased up to a certain frequency band. However, above a certain frequency band, the impact sound reduction performance tended to decrease somewhat. In terms of a single numerical evaluation, the impact sound reduction performance ranged from a minimum of 1 dB to a maximum of 16 dB or more, depending on the type of floor mat and floor structure.

Finally, to assess the reliability of each floor mat's impact sound reduction performance, a correlation analysis was conducted for each bare slab thickness to evaluate a SNQ value of impact sound reduction performance. The correlation analysis of light-weight and heavy-weight impact sounds showed a high correlation between test beds A and B, which consisted of bare slabs with a thickness of 150 mm. Since the same floor matting was used to evaluate the impact sound reduction performance in both test beds A and B, the figures can be considered reliable. Additionally, we analyzed the correlation of the 150 mm bare slab with a Rahmen structure, which was designed in the same way as a real apartment building, to ensure sufficient impact sound reduction performance reliability could be achieved without using the bang machine. Furthermore, the correlation analysis between the impact sound SNQ in the laboratory and the 150 mm and 180 mm bare slabs of test bed A indicated that the light-weight impact sound is lower than the heavy-weight impact sound, bang machine, and rubber ball. However, the impact sound reduction performance is still reliable in both test beds. The correlation analysis results for bare slab thicknesses of 180 mm and 210 mm show a weaker correlation. Therefore, further research is required.

It is expected that the results of this study will be used as a basis for improving the existing measurement standards. In the future, additional evaluations using the same floor mat and the same source at bare slab thicknesses of 180 mm and 210 mm will be required. It is also necessary to evaluate the impact sound reduction performance of floor mats according to changes in the conditions of the sound chamber to examine the effects of changes in test facility conditions. In the future, additional listening tests will need to be conducted with human subjects to account for auditory insensitivity at low frequency bands.

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References

1. Jeon, J.Y.; Jeong, J.H.; Ando, Y. Objective and subjective evaluation of floor impact noise. *J. Temp. Des. in Arch. Environ.* **2002**, *2*, 20–28.
2. Kim, J.H.; Kim, S.H.; Lee, S.M.; Song, H.S.; Ryu, J.K. Comparative examination of the relationship between personal and social factors and annoyance on floor impact noise using survey and laboratory methods. *J. Build. Eng.* **2023**, *72*, 106736. [[CrossRef](#)]
3. *Act No. 2023-494*; Accreditation and Inspection Requirements for Floor Sound Insulation in Apartment Buildings. Ministry of Land, Infrastructure and Transport: Sejong, Republic of Korea, 2023.
4. Shin, H.K.; Park, S.H.; Kim, M.J.; Kim, K.W. A study on subjective response to heavy-weight impact sound through representative spectrum analysis: A case study in South Korea. *Appl. Acoust.* **2022**, *188*, 108562. [[CrossRef](#)]
5. Im, J.B.; Chung, J.Y. A study to reduce heavy-weight floor impact noise in apartment building using stiffness reinforcement method on concrete slab. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise07, Istanbul, Turkey, 28–31 August 2007; pp. 5027–5036.
6. Yun, C.Y.; Kim, M.J.; Sohn, M.H. The Evaluation of Heavy-weight Floor Impact Sound Using Noise Reduction. In Proceedings of the KSNVE Annual Autumn Conference, Daegu, Republic of Korea, 27–28 October 2011; pp. 596–597.
7. Lee, S.C.; Ha, S.S.; Kim, T.S. Strengthening Slab Stiffness to Reduce Heavy-weight Impact Noise on the Floor. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise23, Chiba, Japan, 20–23 August 2023; pp. 7455–7458.
8. Kang, M.W.; Oh, Y.K. Research on simple measurement method of floor finishing materials to predict lightweight floor impact noise reduction performance in apartment houses. *J. Acoust. Soc. Kor.* **2023**, *42*, 594–602.
9. Kim, K.W.; Shin, H.K.; Park, S.H.; Lee, J.W. Analysis of Floor Impact Sound Reduction Performance of Floor Structure with Damping Material. *Trans. Korean Soc. Noise Vib. Eng.* **2022**, *32*, 631–637. [[CrossRef](#)]
10. Kim, T.M.; Kim, J.T.; Kim, T.H.; Park, I.S.; Shin, D.M. The Study of Floor Impact Noise for Apartment Complex using Statistical Energy Analysis: Coupling Loss Factor. In Proceedings of the KSNVE Annual Spring Conference, Gyeongju, Republic of Korea, 20–22 April 2016; pp. 116–120.
11. Yoon, C.Y.; Kang, C.G.; Lee, B.H. Influence of Floor Impact sound according to the composition change on the Aerated Concrete containing Lightweight Aggregate. In Proceedings of the KSNVE Annual Autumn Conference, Yeosu, Republic of Korea, 17–20 October 2018; p. 234.
12. Koo, B.S. Construction companies' response to reducing floor impact noise. *Arch. Environ. Facil.* **2022**, *16*, 6–12.
13. Bouttout, A. Experimental study of the impact noise through concrete floor with resilient layers. *J. Acoust. Soc. Am.* **2017**, *142*, 2517. [[CrossRef](#)]
14. *Act No. 2018-585*; Structural Criteria for Floor Impact Sound Insulation between Floors to Prevent Noise. Ministry of Land, Infrastructure and Transport: Sejong, Republic of Korea, 2018.
15. Oliveira, M.D.; Patricio, J.V. Impact noise of non-homogeneous floors: Analysis of different input parameters for computational modeling predictions. *J. Civ. Eng. Arch.* **2017**, *11*, 274–281.
16. Kim, T.M.; Kim, J.T.; Kim, J.S. Effect of structural vibration and room acoustic modes on low frequency impact noise in apartment house with floating floor. *Appl. Acoust.* **2018**, *142*, 59–69. [[CrossRef](#)]
17. Chun, Y.S.; Lee, S.B. The Influence of the Shape of Slab on Heavyweight Impact Sound Reduction for an Apartment Building. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise16, Hamburg, Germany, 21–24 August 2016; pp. 3234–3242.
18. Kim, K.W.; Jeong, G.C.; Sohn, J.Y. Evaluation of the dynamic stiffness and heavy-weight floor impact sound reduction by composition of resilient materials. *Trans. Korean Soc. Noise Vib. Eng.* **2008**, *18*, 247–254.
19. Ryu, J.K.; Jeong, G.H.; Jeon, I.A.; Go, J.C.; Lee, J.I.; Kim, H.B.; Kim, Y.S. Relationship between property of isolator for standardized floor structure and floor impact sound level. In Proceedings of the KSNVE Annual Autumn Conference, Wonju, Republic of Korea, 25–27 October 2012; pp. 278–279.
20. Führ, G.; Masuero, A.B.; Pagnussat, D.T.; Barreto, M.F.F.M. Impact sound attenuation of subfloor mortars made with exfoliated vermiculite and chrome sawdust. *Appl. Acoust.* **2021**, *174*, 107725. [[CrossRef](#)]
21. Kim, K.W.; Kang, J.S.; Lee, S.E.; Yang, K.S. Floor Impact Sound Isolation Performance by Composition of Ceiling and Wall. *Trans. Korean Soc. Noise Vib. Eng.* **2005**, *15*, 465–473.
22. Kim, I.H.; Go, J.C. Effects of Finishing Materials in Wall and Ceiling on Floor Impact Sound. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise16, Hamburg, Germany, 21–24 August 2016; pp. 7512–7517.
23. Ryu, J.K.; Song, H.S.; Kim, Y.H. Effect of the suspended ceiling with low-frequency resonant panel absorber on heavyweight floor impact sound in the building. *Build. Environ.* **2018**, *139*, 1–7. [[CrossRef](#)]
24. Shin, H.K.; Kim, K.W. Floor Impact Sound Insulation Using Perforated Gypsum Board Ceiling. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise19, Madrid, Spain, 16–19 June 2019; pp. 5848–5853.
25. Kim, S.T.; Cho, H.M.; Kim, M.J. Effects of Wall-to-Wall Supported Ceilings on Impact Sound Insulation for Use in Residential Buildings. *Buildings* **2021**, *11*, 587. [[CrossRef](#)]

26. Cho, H.M.; Kim, S.T.; Kim, M.J. Experimental Study on the Reduction Performance of Floor Impact Sound according to Reduction Method of Floor Structure Layers in Aged-Apartment. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise18, Hong Kong, China, 26–29 August 2018; pp. 2753–2758.
27. Jeon, J.Y.; Ryu, J.K. Influence of noise sensitivity on annoyance of indoor and outdoor noises in residential buildings. *Appl. Acoust.* **2011**, *72*, 336–340.
28. Park, S.H.; Lee, P.J. Reaction to floor impact noise in multi-storey residential buildings: The effects of acoustic and non-acoustic factors. *Appl. Acoust.* **2019**, *150*, 268–278. [[CrossRef](#)]
29. Nakamura, S.I. Reduction of Impact Noise in Apartment Houses by Floor Covering Materials. *J. INCE of Jap.* **1980**, *4*, 137–140.
30. Song, G.G.; Lee, C.S.; Choi, E.S. Floor Impact Sound Reduction of Floor Coverings. In Proceedings of the KSNVE Annual Autumn Conference, Gyeongju, Republic of Korea, 23–25 October 2013; pp. 384–385.
31. Mun, D.H.; Song, G.G.; Lee, C.S.; Park, H.G. Reduction of Floor Impact Noise and Impact Force for PVC Floor Covering and Floor Mat. *Trans. Korean Soc. Noise Vib. Eng.* **2014**, *24*, 501–508. [[CrossRef](#)]
32. Pereira, A.; Godinho, L.; Mateus, D.; Ramis, J.; Branco, F.G. Assessment of a simplified experimental procedure to evaluate impact sound reduction of floor coverings. *Appl. Acoust.* **2014**, *79*, 92–103. [[CrossRef](#)]
33. Chung, J.Y.; Song, H.S.; Song, G.G.; Yoon, Y.J. Improvement of evaluation method for impact sound reduction performance of floor coverings. *J. Acoust. Soc. Korean* **2023**, *42*, 161–167.
34. Yeon, J.O.; Kim, K.W.; Kim, M.J. Evaluation of the Effect and the Perception Range on Impact Sound Reduction by Installing Floor Mats. *J. Korean Inst. Arch. Sustain. Environ. Build. Syst.* **2021**, *15*, 600–612.
35. Korea Apartment News. Available online: <https://www.hapt.co.kr/news/articleView.html?idxno=160369> (accessed on 10 January 2023).
36. *KS F 2865*; Laboratory Measurements of the Reduction of Transmitted Impact Sound by Floor Covering Materials Using Standard Light and Heavy Impact Sources. Korean Agency for Technology and Standards: Eumseong, Republic of Korea, 2015.
37. *ISO 10140-1*; Acoustics—Laboratory Measurement of Sound Insulation of Building Elements—Part 1: Application Rules for Specific Products. International Organization for Standardization: Geneva, Switzerland, 2021.
38. *ISO 10140-3*; Acoustics—Laboratory Measurement of Sound Insulation of Building Elements—Part 3: Measurement of Impact sound Insulation. International Organization for Standardization: Geneva, Switzerland, 2021.
39. *ISO 10140-5*; Acoustics—Laboratory Measurement of Sound Insulation of Building Elements—Part 5: Requirements for Test Facilities and Equipment. International Organization for Standardization: Geneva, Switzerland, 2021.
40. Lee, J.W. The Status and Current Situation of Interfloor Noise in Multi-Unit Residential Buildings. *J. KSNVE* **2013**, *23*, 4–8.
41. Hong, S.S.; Koo, B.S.; Lee, B.K. A characteristic of Floor Impact Noise Reduction using Slab Reinforcement of the Existing Apartment. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise18, Hong Kong, China, 26–29 August 2018; pp. 5601–5608.
42. Kim, K.W.; Shin, H.K. Floor Impact Sound Performance Variation in Old Apartment Housing. In Proceedings of the INTER-NOISE and NOISE-CON Congress and Conference Proceedings, InterNoise19, Madrid, Spain, 16–19 June 2019; pp. 5823–5828.
43. *KS F 2810-1*; Field Measurements of Impact Sound Insulation of Floors—Part 1: Method Using Standard Light Impact Source. Korean Agency for Technology and Standards: Eumseong, Republic of Korea, 2015.
44. *KS F 2810-2*; Field Measurements of Floor Impact Sound Insulation of Buildings—Part 2: Method Using Standard Heavy Impact Sources. Korean Agency for Technology and Standards: Eumseong, Republic of Korea, 2012.
45. *ISO 16283-2*; Acoustics—Field Measurement of Sound Insulation in Buildings and of Building Elements—Part 2: Impact Sound Insulation. International Organization for Standardization: Geneva, Switzerland, 2018.
46. Jeon, J.Y.; Lee, P.J.; Sato, S.I. Use of the standard rubber ball as an impact source with heavyweight concrete floors. *J. Acoust. Soc. Am.* **2009**, *126*, 167–178. [[CrossRef](#)]
47. Lee, W.H.; Haan, C.H. Floor Impact Noise Characteristics of Impact Ball Depending on the Drop Heights in the both Wooden and Concrete Structures. In Proceedings of the 20th International Congress on Acoustics, ICA 2010, Sydney, Australia, 23–27 August 2010; pp. 1–5.

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