

# Monitoring of curing and cyclic thermoresistive response using monofilament carbon nanotube yarn/silicone composites

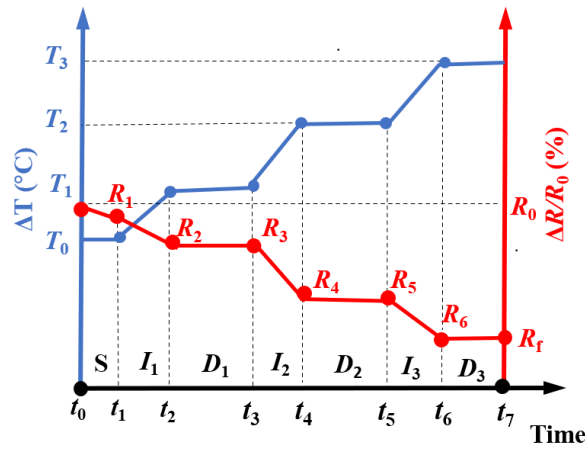
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## Supplementary Information

### S1. Heating-dwell temperature program

A heating-dwell temperature program was used for two CNTY monofilament composites (CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>) in this section. Figure S1 shows the schematic of this temperature program, which is divided into seven zones.



**Figure S1.** Heating-dwell temperature program for CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>.

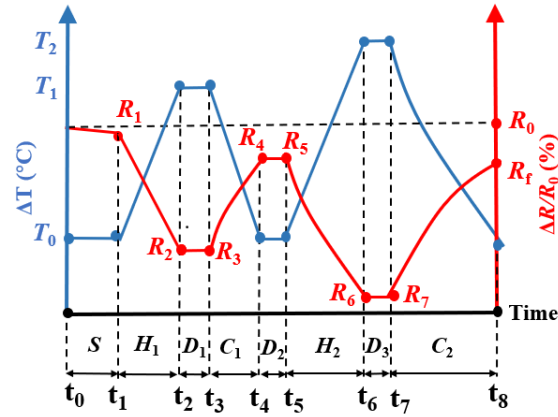
Zone	Time Interval	Electrical Resistance	Fractional Change in the Electrical Resistance		Description of Zones	Parameter
			CNTY/SR <sub>1</sub>	CNTY/SR <sub>2</sub>		
<i>S</i>	$t_0-t_1$	$R_0-R_1$	-0.21%	-0.06%	Stabilization zone	<i>SNR</i>
<i>H</i> <sub>1</sub>	$t_1-t_2$	$R_1-R_2$	-0.44%	-0.30%	Heating from $T_0$ to $T_1$	$\beta_H$
<i>D</i> <sub>1</sub>	$t_2-t_3$	$R_2-R_3$	-1.14%	-0.83%	Dwell at $T_1$	<i>SNR</i>
<i>H</i> <sub>2</sub>	$t_3-t_4$	$R_3-R_4$	-1.85%	-1.57%	Heating from $T_1$ to $T_2$	$\beta_H$
<i>D</i> <sub>2</sub>	$t_4-t_5$	$R_4-R_5$	-4.57%	-3.20%	Dwell at $T_2$	<i>SNR</i>
<i>H</i> <sub>3</sub>	$t_5-t_6$	$R_5-R_6$	-5.38%	-3.90%	Heating from $T_2$ to $T_3$	$\beta_H$
<i>D</i> <sub>3</sub>	$t_6-t_7$	$R_6-R_f$	-6.87%	-5.63%	Dwell at $T_3$	<i>SNR</i>

Table S1 shows the description of zones and the parameters characterized for the specimens in each section. The signal to noise ratio of the fractional change in electrical resistance and the thermoresistive sensitivity (temperature coefficient of resistance) were calculated according to Equations (1), (2) and (3).

Zone *S* represents the initial stabilization zone where the temperature of the oven was kept constant at RT ( $T_0$ ) for 15 minutes. The fractional change in the electrical resistance at the beginning of zone *S* is denoted as  $R_0$ . In zone  $H_1$ , the temperature ramped from  $T_0$  to  $T_1$  (~38 °C) at a constant rate of 1.0 °C /min. In this zone, the electrical resistance decreases from  $R_1$  (−0.21% for CNTY/SR<sub>1</sub> and −0.06% for CNTY/SR<sub>2</sub>) to  $R_2$  (−0.44% for CNTY/SR<sub>1</sub> and −0.30% for CNTY/SR<sub>2</sub>).  $D_1$  represents the dwell zone in which the temperature was held constant at 37.5 °C for 60 minutes.  $\Delta R/R_0$  decreased from  $R_2$  to  $R_3$  (−1.14% for CNTY/SR<sub>1</sub> and −0.83% for CNTY/SR<sub>2</sub>). In zone  $H_2$ , the temperature increased from  $T_1$  (38 °C) to  $T_2$  (60 °C), while  $\Delta R/R_0$  decreased from  $R_3$  to  $R_4$  (−1.84% for CNTY/SR<sub>1</sub> and −1.57% for CNTY/SR<sub>2</sub>).  $D_2$  represents the dwell zone at 60°C for 60 minutes in which the resistance changes from  $R_4$  to  $R_5$  (−4.57% for CNTY/SR<sub>1</sub> and −3.20% for CNTY/SR<sub>2</sub>). The temperature ramped from  $T_1$  (60 °C) to  $T_2$  (80 °C) in zone  $H_3$ , while  $\Delta R/R_0$  decreased from  $R_5$  to  $R_6$  (−5.38% for CNTY/SR<sub>1</sub> and −3.90% for CNTY/SR<sub>2</sub>).  $D_3$  represents the dwell zone at 80 °C for 60 minutes in which  $\Delta R/R_0$  changes from  $R_6$  to  $R_f$  (−6.87% for CNTY/SR<sub>1</sub> and −5.63% CNTY/SR<sub>2</sub>, respectively).

## **S2. Heating-dwell-cooling temperature program**

In this section, a heating-dwell-cooling temperature program was used (Figure S2) to investigate the thermoresistive behavior of the CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub> specimens. SNR values were calculated at stabilization/dwell zones according to Equation (1).



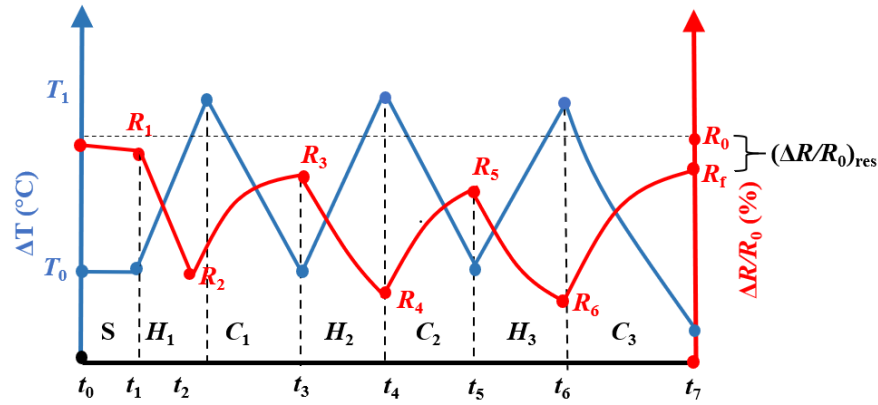
**Figure S2.** Heating-dwell-cooling temperature program for CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>.

After the stabilization zone (S) for 15 minutes, two heating-dwell-cooling cycles were repeated for both specimens. Table S2 shows the summary of zones and parameters characterized in each section. The program was divided into two heating-dwell-cooling cycles. In the first cycle, the oven was heated from  $T_0$  (RT) to  $T_1$  ( $\sim 35^\circ\text{C}$ ) at the rate of  $0.4^\circ\text{C}/\text{min}$  ( $H_1$ ).  $\Delta R/R_0$  decreased from  $R_1$  to  $R_2$  ( $-0.12\%$  to  $-1.16\%$  for CNTY/SR<sub>1</sub> and from  $-0.03\%$  to  $-0.83\%$  for CNTY/SR<sub>2</sub>). The temperature of the oven remained constant at  $T_1$  for 10 minutes (zone  $D_1$ ) while  $\Delta R/R_0$  had a subtle change ( $R_3$  was  $-1.21\%$  for CNTY/SR<sub>1</sub> and  $-0.93\%$  for CNTY/SR<sub>2</sub>). In zone  $C_1$ , the oven cooled down to  $T_0$  at the rate of  $0.05^\circ\text{C}/\text{min}$ . In this zone,  $\Delta R/R_0$  varied from  $R_3$  to  $R_4$  ( $-1.41\%$  and  $-0.73\%$  for CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>, respectively).  $D_2$  represents the dwell zone at  $T_0$  for 10 minutes.  $\Delta R/R_0$  changed from  $R_4$  to  $R_5$  ( $-1.47\%$  for CNTY/SR<sub>1</sub> and  $-0.75\%$  for CNTY/SR<sub>2</sub>). In the second cycle, the temperature raised from  $T_0$  to  $T_2$  ( $50^\circ\text{C}$ ) at the rate of  $0.4^\circ\text{C}/\text{min}$  in zone  $H_2$  while the  $\Delta R/R_0$  decreased from  $R_5$  to  $R_6$  ( $-3.16\%$  and  $-2.29\%$  in CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>, respectively). The temperature of the oven was kept constant at  $T_2$  for 10 minutes in zone  $D_3$ .  $\Delta R/R_0$  had small fluctuations in this section ( $R_7$  was  $-3.30\%$  for CNTY/SR<sub>1</sub> and  $-3.30\%$  for CNTY/SR<sub>2</sub>). In zone  $C_2$ , the temperature was cooled down to  $T_0$  at the rate of  $0.05^\circ\text{C}/\text{min}$ .  $\Delta R/R_0$  increased from  $R_7$  to  $R_f$  ( $-2.24\%$  and  $-1.34\%$  for CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>, respectively). Table S2 represents the details of the temperature program along with their corresponding fractional change in the electrical resistance measurements in each zone. Equations (2) and (3) were used to calculate the thermoresistive sensitivity of the specimens during heating/cooling sections.

<b>Table S2.</b> Description of zones and parameters in heating-dwell-cooling temperature cycles.						
Zone	Time Interval	Electrical Resistance	Fractional Change in the Electrical Resistance		Description of Zone	Parameter
			CNTY/SR <sub>1</sub>	CNTY/SR <sub>2</sub>		
<i>S</i>	$t_0-t_1$	$R_0-R_1$	-0.12%	-0.03%	Stabilization zone	$SNR$
<i>H</i> <sub>1</sub>	$t_1-t_2$	$R_1-R_2$	-1.16%	-0.83%	Heating from $T_0$ to $T_1$	$\beta_H$
<i>D</i> <sub>1</sub>	$t_2-t_3$	$R_2-R_3$	-1.21%	-0.93%	Dwell at $T_1$	$SNR$
<i>C</i> <sub>1</sub>	$t_3-t_4$	$R_3-R_4$	-1.41%	-0.73%	Cooling from $T_1$ to $T_0$	$\beta_C$
<i>D</i> <sub>2</sub>	$t_4-t_5$	$R_4-R_5$	-1.47%	-0.75%	Dwell at $T_0$	$SNR$
<i>H</i> <sub>2</sub>	$t_5-t_6$	$R_5-R_6$	-3.16%	-2.29%	Heating from $T_0$ to $T_2$	$\beta_H$
<i>D</i> <sub>3</sub>	$t_6-t_7$	$R_6-R_7$	-3.30%	-2.42%	Dwell at $T_2$	$SNR$
<i>C</i> <sub>2</sub>	$t_7-t_8$	$R_7-R_8$	-2.24%	-1.34%	Cooling from $T_2$ to $T_0$	$\beta_C$

### S3. Heating-cooling cyclic program

Figure S3 represents a thermal cyclic program used to calculate the thermoresistive sensitivity and hysteresis of CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub> specimens. After the stabilization zone (*S*), the samples were heated from RT to 100°C and cooled back to RT for four continuous cycles at the rate of 1.0 °C/min for both heating/cooling paths.  $SNR$  was calculated in the stabilization zone according to Equation (1).



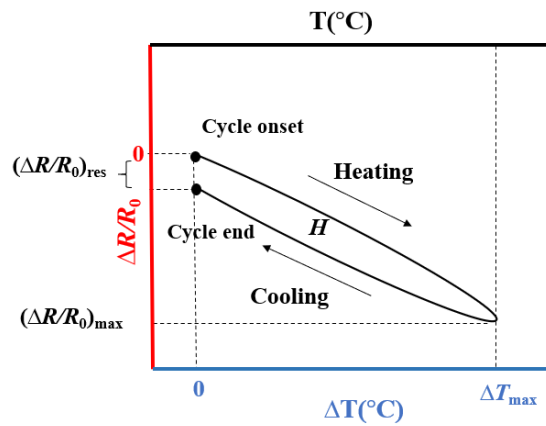
**Figure S3.** Cyclic temperature program for CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>.

Table (S3) shows the description of each zone and the parameters calculated in each section. The thermoresistive sensitivity was calculated in each heating/cooling section according to Equations (1) and (2). The first cycle was not included in the calculations. In zone *H*<sub>1</sub>, the temperature was raised from  $T_0$  (RT) to  $T_1$  (100 °C) while  $\Delta R/R_0$  decreased from  $R_0$  to  $R_1$  (0 to -5.93% for CNTY/SR<sub>1</sub> and 0 to -4.96% for CNTY/SR<sub>2</sub>). In zone *C*<sub>1</sub>, the temperature cooled back to  $T_0$ , and the resistance increased from  $R_1$  to  $R_2$  (-0.31% for

CNTY/SR<sub>1</sub> and  $-0.47\%$  for CNTY/SR<sub>2</sub>). During the second cycle, the temperature increased from  $T_0$  to  $T_1$  in zone  $H_2$  and  $\Delta R/R_0$  decreased from  $R_2$  to  $R_3$  ( $-5.95\%$  for CNTY/SR<sub>1</sub> and  $-4.90\%$  for CNTY/SR<sub>2</sub>). In zone  $C_2$ , the oven was cooled back to  $T_0$  while  $\Delta R/R_0$  decreased from  $R_3$  to  $R_4$  ( $-0.47\%$  for CNTY/SR<sub>1</sub> and  $-0.28\%$  for CNTY/SR<sub>2</sub>).  $H_3$  represents the last heating zone in which  $\Delta R/R_0$  decreased from  $R_4$  to  $R_5$  ( $-6.09\%$  for CNTY/SR<sub>1</sub> and  $-5.07\%$  for CNTY/SR<sub>2</sub>).  $\Delta R/R_0$  increased from  $R_5$  to  $R_f$  ( $-0.74\%$  for CNTY/SR<sub>1</sub> and  $-0.36\%$  for CNTY/SR<sub>2</sub>) by cooling down the temperature to  $T_0$ . TCR values were calculated in heating/cooling sections and average TCR were reported according to Equations (2) and (3).

<b>Table S3.</b> Description of zones and parameters characterized for CNTY/SR1 and CNTY/SR2.						
Zone	Time Interval	Electrical Resistance	Fractional Change in the Electrical Resistance		Description of Zone	Parameter
			CNTY/SR <sub>1</sub>	CNTY/SR <sub>2</sub>		
$H_1$	$t_0-t_1$	$R_0-R_1$	$-5.93\%$	$-4.96\%$	Heating from $T_0$ to $T_1$	$\beta_H$
$C_1$	$t_1-t_2$	$R_1-R_2$	$-0.31\%$	$-0.47\%$	Cooling from $T_1$ to $T_0$	$\beta_C$
$H_2$	$t_2-t_3$	$R_2-R_3$	$-5.95\%$	$-4.90\%$	Heating from $T_0$ to $T_1$	$\beta_H$
$C_2$	$t_3-t_4$	$R_3-R_4$	$-0.47\%$	$-0.28\%$	Cooling from $T_1$ to $T_0$	$\beta_C$
$H_3$	$t_4-t_5$	$R_4-R_5$	$-6.09\%$	$-5.07\%$	Heating from $T_0$ to $T_1$	$\beta_H$
$C_3$	$t_5-t_6$	$R_5-R_f$	$-0.74\%$	$-0.36\%$	Cooling from $T_1$ to $T_0$	$\beta_C$

#### S4. Calculation of hysteresis in heating-cooling cycles



**Figure S4.** Parameters used for characterization of hysteresis of CNTY/SR<sub>1</sub> and CNTY/SR<sub>2</sub>.

The cyclic thermoresistive behavior of each heating-cooling cycle was quantified using three experimental parameters: the residual fractional change in electrical resistance  $(\Delta R/R_0)_{\text{res}}$ , the maximum fractional change in electrical resistance  $(\Delta R/R_0)_{\text{max}}$ , and the normalized hysteresis ( $H_N$ ). Figure S4 shows a schematic of a cycle and the parameters. The cycles described in section S3 were used for data analysis of each specimen. Two independent parameters were used to evaluate the normalized hysteresis: the maximum normalized change in electrical resistance  $(\Delta R/R_0)_{\text{max}}$  and a dependent metric ( $H$ ), which is obtained by subtracting the absolute value of area under the heating curve of each cycle from that of cooling curve. Then the normalized hysteresis ( $H_N$ ) was quantified for each cycle (Equation 6) by dividing the area of the hysteresis loop ( $H$ ) over the product of the maximum temperature change  $(\Delta T)_{\text{max}}$  and the maximum fractional change in electrical resistance,  $(\Delta R/R_0)_{\text{max}}$ .

## References

References list in the Supplementary Information correspond to the list of References in the main manuscript.